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Connecticut Program Savings Document

8th Edition for 2013 Program Year

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Contributors

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INTRODUCTION

1.1 PURPOSE

Purpose

This Program Savings Documentation (PSD) manual provides detailed, comprehensive documentation of resource and non-resource savings corresponding to the Energy Efficiency Fund program and individual Conservation and Load Management (C&LM) program technologies. The PSD manual fulfills the former Connecticut Department of Public Utility Control's (DPUC's) requirement to develop a Technical Reference Manual (Docket NO. 03-11-01PH02, DPUC Review of CL&P and UI Conservation and Load Management Plan for Year 2004 – Phase II, July 28, 2004). Savings calculations detailed in this document are used by The Connecticut Light and Power Company, The United Illuminating Company, Yankee Gas Services Company, Connecticut Natural Gas Corporation and The Southern Connecticut Gas Company, hereinafter referred to as the "Companies."

The Companies have worked together during the past several years to develop common engineering assumptions regarding measured savings for all types of energy-efficient measures. This manual is a compilation of those efforts. In addition, the results of program impact evaluations have been incorporated by the Program Administrators. As a result, all C&LM savings claims will be traceable through cross-references to this manual. The manual is reviewed annually and updated to reflect changes in technology, baselines, measured savings, evaluation work, and impact factors.

The C&LM savings calculations in this manual represent typical measures and the prescriptive calculations used for those measures. In some cases projects are more comprehensive and prescriptive measure calculations are not appropriate. To accurately calculate the savings related to these types of projects, more detailed spreadsheets or computer simulation models must be used. Third-party engineering consultants may be contracted to run simulations and create these spreadsheets; all simulations and spreadsheets are reviewed for reasonableness.

Legislative Imperative

Public Act 05-01, June (2005) Special Session, "An Act Concerning Energy Independence" (the "Act") established a Class III portfolio standard requirement for electric suppliers and electric distribution companies. Following the passage of the Act, the DPUC held a proceeding to develop Class III Renewable Energy Credit standards (Docket NO. 05-07-19, DPUC Proceeding to Develop a New Distributed Resource Portfolio Standard (Class III)). Based on the DPUC Final Decision in that Docket, the Energy Efficiency Fund program and C&LM's technical reference manual must be used as the basis to calculate energy efficiency savings for both C&LM and non-C&LM measures that qualify for Class III credits. As a result, C&LM and non-C&LM measure savings will be determined using the same baseline and parameters. The exception is that non-C&LM funded projects shall not incorporate free-ridership and spillover because these factors are specific to C&LM program savings, however, other impact factors (i.e., other realization rates) that are part of the energy savings calculations and methodologies must be incorporated into non-C&LM savings calculations.

In June 2006, FERC approved a settlement that established a redesigned wholesale electric capacity market in New England intended to encourage the maintenance of current power plants and construction of new generation facilities. The settlement established a Forward Capacity Market ("FCM"). ISO New England, Inc. ("ISO-NE"), operator of the region's bulk power system and wholesale electricity markets, will project the energy needs of the region three years in advance and then hold an annual auction to purchase power resources to satisfy the region's future needs.

In response to ISO-NE solicitation for proposals for the first Forward Capacity Auction, ("FCA1"), CL&P and UI submitted new demand side resource projects, including energy efficiency, that will decrease electric demand and use. Per ISO-NE requirements, detailed Project Qualification Packages that include Measurement and Verification Plans ("M&V") were submitted. The purpose of ISO-NE's required M&V activity is to verify that energy efficiency measures promoted by the programs were actually installed, are still in place and functioning as intended,

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and to validate the reduction in electrical demand compared to some baseline pattern of use. The CL&P and UI PSD, this document, serves as the basis of the demand reduction value calculations that will be submitted in the FCM.

1.2 ORGANIZATION

C&LM measures in this manual are grouped by primary sector and reflect how programs and measures are organized within C&LM. Commercial and industrial measures are also categorized as either "Lost Opportunity" or "Retrofit". The main sections of the manual are as follows:

- Introduction
- Section 2: Commercial & Industrial Lost Opportunity
- Section 3: Commercial & Industrial Retrofit
- Section 4: Residential including Limited Income
- Appendices

Each individual measure is divided into several or all of the following subsections:

- **Description of Measure** describes the scope and basics of the measure
- Savings Methodology lists the methods, reasoning, and tools used to perform calculations
- **Inputs** captures required project or measure data that is used in calculations
- Nomenclature captures variables, constants, and other terminology used in the measure
- **Retrofit Gross Energy Savings Electric** describes the calculations used to determine electric gross Energy savings
- Retrofit Gross Energy Savings Fossil Fuel describes the calculations used to determine fossil fuel gross energy savings
- Retrofit Gross Seasonal Peak Demand Savings Electric (Winter and Summer) describes the calculations used to determine gross peak electric demand savings
- Retrofit Gross Peak Day Savings Natural Gas describes the calculations used to determine gross peak gas demand savings
- Lost Opportunity Gross Energy Savings Electric describes the calculations used to determine gross lost opportunity electric savings
- Lost Opportunity Gross Energy Savings Fossil Fuel describes the calculations used to determine gross lost opportunity fossil fuel savings
- Lost Opportunity Gross Seasonal Peak Demand Savings Electric (Winter and Summer) describes the calculations used to determine gross lost opportunity seasonal peak electric demand savings
- Lost Opportunity Gross Peak Day Savings Natural Gas describes the calculations used to determine gross peak gas lost opportunity savings
- Non Energy Benefits describes any benefits not directly associated with energy savings
- Changes from Last Version if there are any changes from the previous version, they are described in this section
- **References** sources used to construct the measure are listed here
- Notes relevant comments and information is presented in this section

Subsections that do not apply to a particular measure are not included.

Version Date: 10/30/2012 1.3 BACKGROUND

1.3 BACKGROUND

In 1999, the State Legislature created the Energy Conservation Management Board, now called the Energy Efficiency Board ("EEB"), to guide and assist Connecticut's electric and gas distribution companies in the development and implementation of cost-effective energy conservation programs and market transformation initiatives (CGS § 16-245m). The Connecticut Energy Efficiency Fund ("CEEF") created by this legislation provides the financial support for EEB-guided programs and initiatives. The Department of Energy and Environmental Protection ("DEEP") is responsible for final approval of all Energy Efficiency Fund programs. Energy Efficiency Fund programs are administrated by the Conservation and Load Management ("C&LM") divisions of The Connecticut Light and Power Company ("CL&P") and The United Illuminating Company ("UI"). These programs are designed to realize the Energy Efficiency Fund's three primary objectives:

1. Advance the Efficient Use of Energy

Energy Efficiency Fund programs are critical in reducing overall energy consumption and reducing load during periods of high demand. They help mitigate potential electricity shortages and reduce stress on transmission and distribution lines in the State.

2. Reduce Air Pollution and Negative Environmental Impacts

Energy Efficiency Fund programs produce environmental benefits by slowing the electricity demand growth rate, thereby avoiding emissions that would otherwise be produced by increased power generation activities. The Environmental Protection Agency regulates "criteria" air pollutants under the Clean Air Act's National Ambient Air Quality Standards ("NAAQSs"). The EPA calls these pollutants "criteria" air pollutants because it regulates them by developing human health-based and/or environmentally-based criteria (science-based guidelines) for setting permissible levels. Energy Efficiency Fund programs have significantly reduced two NAAQS criteria pollutants emitted in the process of generating electricity: sulfur dioxide and nitrogen oxides. Carbon dioxide and other "greenhouse gases," such as methane, are also emitted during the process. Greenhouse gases have been linked to global warming and climate change. Energy Efficiency Fund programs have helped to reduce carbon dioxide emissions by reducing electrical demand, and consequently the need for additional generation, through energy efficiency and conservation. These programs also produce environmental benefits by reducing the consumption of natural gas and fuel oil. With assistance from the EEB, the Energy Efficiency Fund programs developed by the Companies support the state's environmental initiatives to reduce these air pollutants as well as fine particulate emissions and ozone.

3. Promote Economic Development and Energy Security

Energy Efficiency Fund programs generate considerable benefits for Connecticut customers. These programs are tailored to meet the particular needs of all customers, thereby benefiting all state residents and businesses. Energy efficiency measures assist residential customers in reducing their energy costs. Other groups that benefit from energy efficiency programs include educational institutions, non-profit organizations, municipalities, and businesses. By reducing operating costs and enhancing productivity, Connecticut businesses remain competitive in the dynamic global economy.

Information regarding Energy Efficiency Fund programs is available at:

Connecticut's statewide energy information portal:

The Connecticut Light and Power Company:

Www.cl-p.com

Www.uinet.com

Www.cngcorp.com

Www.cngcorp.com

Southern Connecticut Gas Company:

Yankee Gas Services Company:

www.yankeegas.com

The Energy Efficiency Board: http://www.ctsavesenergy.org/ecmb/

1.4 SAVINGS CALCULATIONS

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The savings results presented in this manual (both electric and non-electric) are assumed to be the savings that would be measured at the point of use. In other words, electric savings, both energy (kWh) and demand (kW), and natural gas savings (Ccf) are savings that would occur at the customer's meter. Line losses are not included in the savings values presented here. Instead, line loss effects are captured within the screening model that the Companies use to evaluate the benefits of energy efficiency programs. (Refer to Chapter 6, *Cost Benefit Analysis*, for detail on C&LM Program screening.) Additionally, the annual electric savings from measures has a specified load shape, i.e., the time of day and seasonal patterns at which savings occur. (See Appendix 2 for load shapes for various end-use savings.) The load shapes are used to assign the proper value of energy savings resulting from the implementation of C&LM measures to the corresponding time of day when those savings are realized.

Types of Savings

Energy efficiency measures are generally limited to two types:

- Replacement or "Retirement" of less efficient measures with a baseline or standard measures
- "Lost Opportunity", where measures are installed that are more efficient than a baseline or standard Many energy efficiency measures consist of both a retirement component and a lost opportunity component. This is illustrated by the chart below:

Existing /Old Energy Usage equipment Retirement Retrofit Savings Baseline Savings equipment Lost Opportunity Savings High Efficiency equipment Remaining Useful Life Measure Program (RUL) Lifetime action Time

Retrofit, Retirement, and Lost Opportunity Savings

Some measures may utilize a two-part lifetime savings calculation. For example, in an "Early Retirement" case, where the existing unit (using lower efficiency, out-of-date technology) would have been operating until failure and early retirement is stimulated by the program measure, savings may be claimed between the existing unit to the standard baseline unit (driven by the level of efficiency most standard units achieve), for the retirement measure life. The residential retirement lifetime refers to how much longer the existing unit would have operated absent the influence of the program. For example, a working heating system may be retired prior the end of its useful life as a result of program intervention.

Lost opportunity lifetimes apply to the portion of savings resulting from choosing a high efficiency product to replace the retired product over a standard efficiency product available on the market. If the retired heating system in the above example were replaced with a high efficiency model (versus a standard baseline model) generating additional savings, it would result in lost opportunity savings.

If the retirement life is much greater than zero, the retirement and lost opportunity savings are combined to generate total Retrofit savings. When the retirement life is approximately zero, savings are reduced to lost opportunity

savings only. Retirement savings are acknowledged to exist but are ignored because they are assumed to be short lived.

Peak Savings

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The values for electric demand savings (both winter and summer) in this manual are given based on the following definition:

- A "Seasonal Peak" reduction is based on the average peak reduction for a measure during the ISO New England definition for a Seasonal Peak Demand Resource when the real-time system hourly load is equal to or greater than 90 percent of the most recent "50/50" system peak load forecast for the applicable summer or winter season.
- The "Summer Season" is defined as non-holiday weekdays during the months of June, July and August.
- The "Winter Season" is defined as non-holiday weekdays during December and January.

Typically, seasonal peaks are weather driven and occur in the mid-afternoon on summer weekdays, or for winter, in the early evening.

Electric peak demand savings can be calculated either on a measure-by-measure basis or on a default basis. Coincidence factors can be used to calculate demand savings based on the annual savings and load shape of the measure. Coincidence factors are multiplied by the connected load savings of the measure in order to obtain the peak demand savings. (See Appendix 1 for a list of default coincidence factors that are used to calculate the peak demand savings.)

For natural gas measures, the peak savings represents the estimated savings coincident with the theoretical maximum system usage in a twenty four hour period. Since the natural gas peak is driven by cold weather, the peak savings for heating-related measures is estimated based on degree-day data and the estimated coldest 24 hour degree period. For measures that save natural gas continuously at an equal rate throughout the year, the peak savings is assumed to be the annual savings divided by 365. (The calculations for peak natural gas savings are found in Appendix 1.)

Non-Electric Benefits

In addition to electric and natural gas benefits, some measures have other non-electric benefits. Where appropriate, these benefits (or "impacts" since they can also be negative) are defined in this manual. Non-electric, non-natural gas impacts may include quantifiable changes in other fossil fuel consumption, water use, maintenance costs, productivity improvements, replacement costs, etc. Non-electric benefits are not included in the Electric System Test, as they are captured in the Total Resource Cost Test.

Savings Adjustment Factors

The savings for the measures defined in this manual are gross savings. Impact factors are applied to the gross savings to calculate the net (final) savings. Gross energy savings estimates (based on known technical parameters) represents the first step in calculating energy savings. Gross savings calculations are based on engineering algorithms or modeling that take into account technically important factors such as hours of use, differences in efficiency, differences in power consumption, etc.

When calculating the total impact of energy saving measures, there are also some other factors beyond the engineering parameters that need to be considered, such as the market effects of free-ridership, spillover or installation rate. The equation for net savings is as follows:

Net Savings = *Gross Savings* \times (1+ *spillover* – *free ridership*) \times *Installation Rate*

In some cases, evaluation work may uncover differences between calculated savings and actual (metered) savings that may not be completely attributable to the impact factors above. These differences may arise when the savings

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calculations do not accurately capture the real savings attributable to a measure. In addition to the impact factors above, savings differences can happen for a variety of reasons such as non-standard usage patterns or operating conditions. In these cases, overall net-to-gross ratios (realization rates) may be used in addition to or instead of the aforementioned impact factors to bring the observed savings values more in line with the original savings calculations.

For instance, a billing analysis may show observed savings from a refrigerator removal program to be 60 percent of the gross (calculated) savings. In this case, the differences may be attributable to a combination of factors including refrigerators that are not being used, free-ridership, units being improperly used (e.g., the refrigerator door left open for long periods of time), and units that exhibit lower energy use because they are operating in cooler basement environments. In such a case, a 60 percent realization rate would be applied to the gross (calculated) energy savings to correct it.

Realization rates can be applied to specific measures or across programs depending on their source. Since commercial and industrial ("C&I") programs typically offer a wide range of diverse measures, defining specific impact factors for C&I programs can be difficult, and therefore program specific realization rates are usually limited to C&I programs. Appendix 3 contains a list of program specific realization rates. These rates have been updated from 2010 based on recent completed studies. Realization rates are no longer included in the description of each individual measure.

Common Energy Conversions

Energy conversions used in this document to convert energy to a specific fuel type are summarized in the following table:

| Energy | Conversion | Factors |
|--------|------------|----------------|
|--------|------------|----------------|

| To Obtain: | Multiply: | By: |
|------------------------|-----------|------------|
| BTU | MMBtu | 1,000,000 |
| Ccf Of Gas | MMBtu | 1/0.1029 |
| Gal Of Oil (No. 2) | MMBtu | 1/0.138690 |
| Gal Of Propane | MMBtu | 1/0.09133 |
| kWh Electric | MMBtu | 1/0.003412 |
| kWh Electric | BTU | 1/3412 |
| Ton (air conditioning) | BTU/h | 1/12000 |

1.5 MAJOR CHANGES FROM 2012

The following high-level changes have been made:

- The definition of retirement, retrofit, and lost opportunity has been clarified (Section 1.4). Additionally, certain residential measures have been updated to reflect the clarification as follows:
 - 1. Retrofit and lost opportunity calculations are updated to better present how to calculate the appropriate savings.
 - 2. The methodology section has been updated with clarifying language.
- References used for measure lives and impact factors have been indexed (Appendix 4).

Many other measure-specific changes have been incorporated into this document. These are highlighted within individual measures under the "Changes from Last Version" subsection where applicable.

1.6 GLOSSARY

The glossary provides definitions of the energy conservation terms used in this PSD. Note that some of these terms may have alternative or multiple definitions some of which may be outside the context of the manual. Only definitions pertaining to this manual are included in the glossary.

Annual Fuel Utilization Factor (AFUE): The thermal efficiency measure of combustion equipment like furnaces and boilers. The AFUE differs from the true 'thermal efficiency' in that it is not a steady-state, peak measure of conversion efficiency, but instead attempts to represent the actual, season-long, average efficiency of that piece of equipment, including the operating transients. The method for determining the AFUE for equipment is based on ASHRAE standards.

ASHRAE: American Society of Heating, Refrigerating and Air-Conditioning Engineers, Inc., an international technical society in the fields of heating, ventilation, air conditioning, and refrigeration, known for writing the industry standards for testing and practice.

Baseline Efficiency: C&LM program savings are calculated from this efficiency value. It represents the value of efficiency of the equipment that would have been installed without any influence from the program. *Contrast compliance efficiency*.

Baseline Standard: The source or document that provides the baseline efficiency values, or a means to calculate these values. In many cases, the baseline efficiency is the minimum efficiency required by codes and standards, such as the Connecticut Energy Code.

Behavioral Conservation: Programs that encourage customer strategies to conserve energy through changes, modifications to standard practice, or changes or modifications to customer behavior.

Benefit-Cost Ratio ("BCR"): The efficiency programs determine cost effectiveness using either the Utility Cost Test (Electric System, Natural Gas System) or Total Resource Test. Energy efficiency efforts are cost-effective if the benefit-cost ratio is greater than or equal to 1.0. See Electric System Test, Natural Gas System Test, & Total Resource Test or refer to Chapter 6 of the C&LM Plan for details regarding BCR tests.

BTU: British Thermal Unit. The amount of energy needed to heat one pound of water one degree Fahrenheit (from 39°F to 40°F).

Capacity: The maximum output of equipment at the standard conditions for the specific type of equipment. These are often given in units of Btu per hour or Tons.

CcF: 100 Cubic feet of gas; used to measure a quantity of natural gas.

Coefficient of Performance (COP): The efficiency rating of heating or cooling equipment. The COP is, at specific standard conditions, based on the specific type of equipment. Typically used for heat pumps in heating mode and gas driven chillers.

Compact Fluorescent Lamp (CFL): A bulb technology that uses significantly less energy than traditional incandescent bulbs. CFLs may be classified as either General Service or Non-General Service Bulbs. *See General Service Bulb & Non-General Service Bulb.*

Coincident Demand: Demand of a measure that occurs at the same time as some other peak (building peak, system peak, etc.). In the context of this document, coincident demand is a measure of demand savings that is coincident with ISO New England's Seasonal Peak definition.

Coincidence Factor: Coincidence factors represent the fraction of connected load expected to occur at the same time as a particular system peak period on a diversified basis. Coincidence factors are normally expressed as a percent.

Compliance Efficiency: This efficiency value must be achieved in order to qualify for a C&LM program incentive. *Contrast baseline efficiency.*

Compliance Standard: The source or document that provides the compliance efficiency values, or a means to calculate these values. In many cases the compliance efficiency is based on standards from recognized programs such as ENERGY STAR®.

Connected Load: The maximum power required by the equipment, usually expressed as kW.

Cooling Degree Days (**CDD**): A measure of how hot a location is over a base temperature of 65°F over a year. *See also Degree Days*.

Degree Days: For any individual day, degree days indicate how far that day's average temperature departed from 65°F. Heating Degree Days (HDD) measure heating energy demand and indicate how far the average temperature fell below 65°F. Similarly, Cooling Degree Days (CDD), which measures cooling energy demand, indicates how far the temperature averaged above 65°F. In both cases, smaller values represent less fuel demand, but values below 0 are set equal to 0, because energy demand cannot be negative. Furthermore, since energy demand is cumulative, degree day totals for periods exceeding 1 day are simply the sum of each individual day's degree day total.

Demand: The average electric power requirement (load) during a time period. Demand is measured in kW and the time period is usually one hour. If the time period is different than one hour, i.e., 15 minutes, the time period would be stated as "15-minute demand." Demand can refer to an individual customer's load or to the load of an entire electric system. (See Peak Demand).

Demand Reduction, Demand Savings: The reduction in demand due to installation of an energy efficiency measure usually expressed as kW and measured at the customer's meter. *See discussion under Peak Demand Savings*.

Demand Resources: ISO New England classifies demand reduction from energy efficiency and conservation measures into the following two categories:

- Active Resource Demand reduction that is dispatched (i.e., demand response and emergency generation) that must respond to the electric system operator during shortage events. For example, resources entered into the ISO Demand Response program are active resources because they are called upon for specific shortage events.
- Passive Resource Demand reduction that is not dispatched (i.e., energy efficiency, plus a small amount of
 distributive generation) that reduces load during pre-defined hours and periods. Most C&LM measures are
 passive because they reduce load across a pre-defined operating period. For example, energy-efficient lighting
 will reduce load whenever lights are on throughout the year.

Diversity Factor: See Coincidence Factor.

Demand Reduction-Induced Price Effects (DRIPE): The reduction in prices in the wholesale energy and capacity markets because of the reduction in energy and demand resulting from conservation efforts.

Early Retirement: A measure is classified as early retirement when the participant replaces working equipment before the end of its useful life. In the case where the existing unit (using lower efficiency, out-of-date technology) would have been operating until failure and early retirement is stimulated by the program measure, savings may be claimed between the existing unit to the standard baseline unit (driven by the level of efficiency most standard units achieve), for the retirement measure life.

Electric System (benefit-cost ratio) Test: Defined as the present value of the avoided electric costs (including energy, capacity, DRIPE, transmission and distribution) divided by the program costs of achieving the savings. The electric system test is a tool used to screen electric measures and programs in Connecticut. Energy efficiency efforts are cost-effective if the benefit-cost ratio is greater than or equal to 1.0.

Emittance: The ratio of the radiant heat flux emitted by a specimen to that emitted by a blackbody at the same temperature and under the same conditions.

End Use: Refers to a category of measures with similar load shapes. There are several different acceptable industry standards for defining end-use categories. For the purpose of this manual, end uses are cooling, heating, lighting, refrigeration, water heating, motors, process, and others.

Energy Conservation: Energy or peak reduction resulting from changes in customer behavior(s) or program actions.

Energy Efficiency: Reducing energy usage without reducing performance.

Energy Efficiency Ratio (EER): The performance rating of electrically operated cooling equipment. The rating is calculated based on specific standard conditions based equipment type.

Equivalent Full Load Hours ("**EFLH**"): The number of hours per year that the equipment would need to draw power at its connected (full) load rating in order to consume its estimated annual kWh. It is calculated as annual kWh/connected kW. EFLH is the same as operating hours for technologies that are either on or off, such as light bulbs. EFLH is less than operating hours for technologies that operate at part load for some of the time, such as air conditioners and motors.

Evaluation Study: Studies that evaluate program impacts, free-ridership, and spillover, as well as processes, specific measures and market assessments. Results of these studies are used by program administrators to modify the programs and savings estimates.

Free-Rider: A program participant who would have installed or implemented an energy efficiency measure even in the absence of program marketing or incentives.

Free-ridership: The fraction (usually expressed as a percent) of gross program savings that would have occurred even in the absence of a C&LM program.

General Service Bulb: General Service bulbs are defined as standard base bulbs that are intended for general service applications as specified in the Energy Independence and Security Act of 2007. The term 'general service incandescent lamp' means a standard incandescent or halogen type lamp that is intended for general service applications, has a medium screw base, has a lumen range of not less than 310 lumens and not more than 2,600 lumens, and is capable of being operated at a voltage range at least partially within 110 and 130 volts. Please note that Dimmable bulbs may be either General Service or Non-General Service bulbs. See Non-General Service Bulb for exclusions.

Gross Savings: A savings estimate, calculated from objective technical factors. The gross savings do not include impact factors.

Heating Degree Days (**HDD**): A measure of how cold a location is over a base temperature of 65°F over a year. (*See also Degree Days*).

Heating Seasonal Performance Factor (HSPF): A measure of a heat pump's energy efficiency over one heating season. It represents the total heating output of a heat pump (including supplementary electric heat) during the normal heating season (in Btus) compared to the total electricity consumed (in watt-hours) during the same period. The higher the rating, the more efficient the heat pump.

High Efficiency: High efficiency equipment uses less energy than standard equipment.

Impact Evaluation: A study that assesses the energy, demand, and non-electric benefits associated with energy efficiency measures or programs.

Impact Factor: A number (usually expressed as a percent) used to adjust the gross savings in order to reflect the savings observed by an impact study. Examples of impact factors include free-ridership, spillover and installation rate.

Installation Rate: The fraction of the recorded products that are installed. For example, some screw-in compact fluorescent lamps are bought as spares, and will not be installed until another one burns out.

Lighting Power Density (LPD): The amount of electrical power required for the installed lighting in a building space or in an entire building, expressed as watts per square foot.

Load Factor: The average fractional load at which the equipment runs. It is calculated as average load/connected load.

Load Shape: The time-of-use pattern of a customer's energy consumption or measure. Load shape can be defined as hourly and/or seasonally (winter/summer).

Lost Opportunity: Refers to the new installation of an enduring unit of equipment (in the case of new construction) or the replacement of an enduring unit of equipment at the end of its useful life. An enduring unit of equipment is one that would normally be maintained, not replaced, until the end of its life. *Contrast "retrofit"*

Market Effect: A change in the behavior of a market because of conservation and energy efficiency efforts. "Market effect savings" are the result of changes in market behaviors.

MMBtu: Millions of British Thermal Units.

Measure: A product (a piece of equipment) or a process that is designed to provide energy or demand savings. Measure can also refer to a service or a practice that provides savings.

Measure Cost: For new construction or measures that are installed at their natural time of replacement (replace upon burn-out), measure cost is defined as the incremental cost of upgrading to high efficiency. For retrofit measures, measure cost is defined as the full cost of the measure. Measure cost refers to the true cost of the measure regardless of whether an incentive was paid for that measure.

Measure Lifetimes: This is the average number of years (or hours) that a group of new high efficiency equipment will continue to produce energy savings or the average number of years that a service or practice will provide savings. Lifetimes are generally based on experience or studies. For retrofit or early retirement measures, the measure lifetime may include a change in baseline over time, more accurately reflecting the lifetime energy savings.

Measure Type: Refers to a category of similar measures. There are several different acceptable industry standards for defining end-use categories. For the purpose of this manual, primary end-use categories include cooling, heating, lighting, refrigeration, water heating, motors, process, and other.

Natural Gas System (benefit-cost ratio) Test: A ratio used to assess the effectiveness of energy efficiency efforts on the natural gas system. The natural gas system test is defined as the present value of the avoided natural gas costs divided by the program-related costs of achieving the savings. The Natural Gas System test is the primary evaluation tool used to screen natural gas measures and programs in Connecticut. Energy efficiency efforts are cost-effective if the benefit-cost ratio is greater than or equal to 1.0.

Net Savings: The final value of savings that is attributable to a program or measure. Net savings differs from "gross savings" because it includes adjustments from impact factors such as free-ridership or spillover. Net savings is sometimes referred to as "verified savings" or "final savings."

Net-to-Gross: The ratio of net savings to the gross savings (for a measure or program). Net-to-gross is usually expressed as a percent.

Non-Electric Benefits: Quantifiable benefits (beyond electric savings) that are the result of the installation of a measure. Fossil fuel, water, maintenance, and increase in productivity are examples of non-electric benefits. Non-electric benefits

can be negative (i.e., increased maintenance or increased fossil fuel usage which results from a measure) and therefore are sometimes referred to as non-electric impacts. This may also include non-quantifiable benefits that are difficult or impossible to put a number on, such as increased comfort.

Non-General Service Bulb: Non-General Service CFL applications are excluded from the Energy Independence and Security Act of 2007. Listed below are all of the applications that are excluded. Applications applying to bulbs in the CEEF programs are indicated with an asterisk (*):

- * Reflector bulbs
- * 3-way bulbs
- * Candelabra based bulbs
- * G type (globe) bulbs
- Appliance bulbs
- Black light bulbs
- Bug bulbs
- Colored bulbs
- Infrared bulbs
- Left-hand thread bulbs
- Marine bulbs
- Marine signal service bulb
- Mine service bulb
- Plant light bulb
- Rough service bulb
- Shatter-resistant/proof/protected bulb
- Sign service bulb
- Silver bowl bulb
- Showcase bulb
- Traffic signal bulb
- Vibration service bulb
- T-shape bulb
- B,BA,CA,F,G16-1/2,G-25,G30,S,M-14 bulbs

Please note that Dimmable bulbs may be either General Service or Non-General Service bulbs. *Contrast General Service Bulb.*

Non-Participant: A customer who is eligible to participate in a program, but does not. A non-participant may install a measure because they became aware of the benefits through program marketing or outreach, but the installation of the measure is not through regular program channels. As a result, their actions are normally only detected through evaluations (see spillover).

Operating Hours: The annual amount of time, in hours, that the equipment is expected to operate. *Contrast Equivalent Full Load Hours*.

Participant: A customer who installs a measure through regular program channels and receives any benefit (i.e., incentive) that is available through the program because of his participation. Free-riders are a subset of this group.

Peak Day Factor: Multipliers that are used to calculate peak day reductions based on annual gas energy savings.

Peak Day, Gas: The one day (24 hours) of maximum system deliveries of gas during a year.

Peak Demand: The highest electric demand in a given period of time that is usually expressed in kW.

Peak Demand Savings: The kW demand reduction that occurs in the peak hours. The peak demand savings is usually determined by multiplying the demand reduction attributed to the measure by the appropriate seasonal or on-peak coincidence factor. There is both a summer peak and a winter peak. (Coincidence factors for different measures for each peak are shown in Appendix 1.) Two peak periods are used:

• Seasonal Peak Hours are those hours in which the actual, real-time hourly load Monday through Friday on non-holidays, during the months of June, July, August, December, and January, as determined by the ISO, is equal to or greater than 90 percent of the most recent 50/50 system peak load forecast, as determined by the ISO, for the applicable summer or winter season.

• On-Peak Hours are hours 1:00 - 5:00 p.m., Monday through Friday on non-holidays during the months of June, July, and August and from 5:00 - 7:00 p.m., Monday through Friday on non-holidays during the months of December and January.

The Seasonal Peak demand savings are used in the C&LM programs. See also Coincidence Factor, Demand Savings.

Peak Factor: Multipliers that are used to calculate peak demand reductions for measures based on the annual electric energy savings of the measure. The units of peak factors are W/kWh based on end use.

Realization of Savings: The ratio of actual measure savings to gross measure savings (sometimes referred to as the "realization rate"). This ratio takes into account impact factors that can influence the actual savings of a program such as spillover, free-ridership, etc.

Retrofit: The replacement of a piece of equipment or device before the end of its useful or planned life for the purpose of achieving energy savings. Retrofit measures are sometimes referred to as "early retirement" when the removal of the old equipment is aggressively pursued. Residential measures utilize a two-part lifetime savings calculation. In certain situations, such as early retirement, savings may be claimed in two parts, where the retirement part is additional to the lost opportunity part until the end of the remaining useful life (RUL), after which lost opportunity savings continue until the last year of the retrofits measure's effective useful life (EUL). *Contrast "Lost Opportunity."*

R-Value: A measure of thermal resistance of a material or system, equal to the reciprocal of the U-Value, used to calculate heat gain or loss. The R-Value is expressed in terms of degrees Fahrenheit multiplied by hours, multiplied by square feet per Btu.

Seasonal Energy Efficiency Ratio (SEER): The total cooling output of a central air conditioning unit in Btus during its normal usage period for cooling divided by the total electrical energy input in watt-hours during the same period, as determined using specified federal test procedures.

Sector: A system for grouping customers with similar characteristics. For the purpose of this manual, the sectors are Commercial and Industrial ("C&I"), Small Business ("SMB"), Residential, Non-Limited Income ("NLI") and Limited Income ("LI").

Spillover: Savings attributable to a program, but additional to the gross (tracked) savings of a program. Spillover includes the effects of: (a) participants who install additional energy-efficient measures as a result of what they learned in the program; or (b) non-participants who install or influence the installation of energy efficient measures as a result of being aware of the program.

Summer Demand Savings: Refers to the demand savings that occur during the summer peak period. *See discussion under Peak Demand Savings.*

Total Resource (Benefit/Cost) Test: A test used to assess the net benefit of energy efficiency resources to society. The total resource test is different from the electric system test in that the total resource benefit consists of the avoided costs of all conserved energy (electric *and* other fuels) plus other non-energy resource impacts that may have occurred because of efficiency efforts such as reduced maintenance or higher productivity. The cost for the total resource benefit consists of all program-related costs and any costs incurred by the customer related to the installation of measures.

Winter Demand Savings: Refers to average demand savings that occurs during the winter peak period. *See discussion under Peak Demand Savings.*

C&I LOST OPPORTUNITY

2.1 LIGHTING

2.1.1 STANDARD LIGHTING

Description of Measure

Installation of lighting which exceeds current energy code baseline measured in lighting watts per square foot.

Savings Methodology

The difference between installed lighting and code lighting power density (LPD, watts per square foot) for the facility is used to estimate energy and seasonal peak demand savings. In addition to the savings from reduction in power density savings are also calculated for installation of occupancy sensors and residential fixtures as applicable (Note [1]). Reduction of lighting power reduces the cooling load and provides additional savings, which are also calculated in this measure. The baseline for lighting power density is ASHRAE Standard 90.1-2007. Code requires lighting controls for buildings over 5,000 square feet. Therefore, occupancy sensor savings are only calculated if buildings >5,000 square feet have occupancy sensors in addition to the code required scheduled lighting control.

Inputs

| Symbol | Description | Units |
|---------------|-------------------------------------|-------------|
| Allowable LPD | Allowable LPD from ASHRAE 90.1-2007 | Watts/Sq ft |
| | Total fixture connected kW | kW |
| | Facility illuminated area | Square Feet |

Nomenclature

| Item | Description | Units | Values | Comments |
|----------------------|--|-----------------------|--------|---------------|
| A | Facility illuminated area | Square Feet | | |
| AKWH | Annual Gross Electric Energy savings | kWh | | |
| ASHRAE | American Society of Heating, Refrigerating and Air- | | | |
| ASTIKAL | Conditioning Engineers | | | |
| CF_L | Lighting Coincidence Factor | | | Appendix 1 |
| CF_{os} | Occupancy Sensor Coincidence Factor | | | Appendix 1 |
| CF_{hw} | Residential lighting Coincidence Factor | | | Appendix 1 |
| COP | Coefficient of Performance | | 4.5 | Note [3] |
| DeltaW _{hw} | Delta watts of hardwired fluorescent fixtures in residential | | | |
| | areas as calculated per Section 4.1.2 of this document. | | | |
| F | Fraction of lighting energy that must be removed by the | | | |
| 1 | facilities cooling system. | | | |
| G | Estimated lighting energy heat | | 0.73 | Note [4] |
| Н | Facility lighting hours of use | Hours | | Site Specific |
| | | | | or Appendix 5 |
| HVAC | Heating, Ventilation and Air Conditioning | | | |
| kW | Electric Demand | kW | | |
| LPD | Lighting Power Density | Watts/ft ² | | |
| N | Number of different fixture types with occupancy sensors | | | |
| n | Fixture number | | | |
| O _n | Quantity of fixtures of type n that have occupancy sensors | | | |

| Item | Description | Units | Values | Comments |
|----------------|--|-------|--------|----------|
| S _c | Energy savings from reduced cooling load | kWh | | |
| $S_{\rm hw}$ | Energy savings from installation of hard-wired fluorescent fixtures in residential areas | kWh | | |
| S_{lpd} | Energy savings due to lower lighting power density | kWh | | |
| Sos | Energy savings from use of occupancy sensors, if applicable | kWh | | |
| W | Fixture input wattage | Watt | | |
| W _n | Input watts for fixture type n | | | |

Lost Opportunity Gross Energy Savings, Electric

$$S = S_{lpd} + S_{os} + S_{hw} + S_c$$

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Calculation of savings due to lower lighting power density

 S_{lod} , = (Allowable LPD - Actual LPD)*H*A

Allowable LPD, in kW/ft2, is the value of Watts per ft² from ASHRAE for the facility type divided by 1000. The building area lighting power densities from ASHRAE are provided in the table below. Refer to ASHRAE 90.1-2007 for the space-by-space method. When using the space-by-space method to calculate the LPD, an increase in the spaces' power allowances can be used, in accordance with Section 9.6.2 of ASHRAE 90.1-2007.)

Actual LPD, in kW/ft², is calculated by dividing the total Fixture Wattage by the Lighted Area, ft²

Fixture Wattage is the sum of the power consumed by each fixture.

A = is calculated (measured) for each project, either from architectural drawings or by physical measurement.

Calculation of savings due to occupancy sensors

If the Actual LPD is less than or equal to the Allowable LPD, then S_{OS} will be calculated as follows; otherwise, $S_{OS} = 0$.

$$S_{OS} = \frac{0.3H}{1000} \sum_{n=1}^{N} O_n W_n$$

Explanation of numerical constants:

- 0.3 is the generally accepted average energy reduction fraction due to the use of occupancy sensors. See Ref [1].
- 1000 converts watts to kW (1/1000 is the conversion)

Calculation of savings from hard-wired fluorescent fixtures in residential areas

Refer to PSD Section 4.1.2 "CFL Fixtures (New Homes)" for this calculation. Normally the total number and type of fixtures in living areas is not known at the time of construction, so the LPD method cannot be used to calculate these savings. Where hard-wired fixtures are installed as part of new construction, they are usually shown on the building plans. Their savings are calculated per fixture according to the residential methodology.

Calculation of savings due to the reduced cooling required to remove excess heat produced by the lighting fixtures

Sc = savings resulting from reduced cooling

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$$S_{C} = \frac{\left(S_{lpd} + S_{os} + S_{hw}\right) \bullet F}{COP}$$

F = Fraction of annual kWh energy savings that must be removed by the cooling system

If the HVAC system includes an economizer,

Then F = 0.35. Otherwise, use the table below

Table 1: Fraction of annual kWh energy savings that must be removed by the cooling system (See Ref [2])

| Building Area, A, Sq ft | F |
|-------------------------|--|
| < 2,000 | 0.48 |
| 2,000 – 20,000 | $0.48 + \frac{0.195 \times (A - 2,000)}{18,000}$ |
| >20,000 | 0.675 |

COP = 4.5 (Note: [3])

Table 2: Lighting Power Densities Using the Building Area Method (Ref [3])

| Building Area Type (see note [2]) | Lighting Power Density (W/ft2) |
|-----------------------------------|--------------------------------|
| Automotive Facility | 0.9 |
| Convention Center | 1.2 |
| Court House | 1.2 |
| Dining: Bar Lounge/Leisure | 1.3 |
| Dining: Cafeteria/Fast Food | 1.4 |
| Dining: Family | 1.6 |
| Dormitory | 1.0 |
| Exercise Center | 1.0 |
| Gymnasium | 1.1 |
| Healthcare-Clinic | 1.0 |
| Hospital/Healthcare | 1.2 |
| Hotel | 1.0 |
| Library | 1.3 |
| Manufacturing Facility | 1.3 |
| Motel | 1.0 |
| Motion Picture Theatre | 1.2 |
| Multi-Family | 0.7 |
| Museum | 1.1 |
| Office | 1.0 |
| Parking Garage | 0.3 |
| Penitentiary | 1.0 |
| Performing Arts Theatre | 1.6 |
| Police/Fire Station | 1.0 |
| Post Office | 1.1 |
| Religious Building | 1.3 |
| Retail | 1.5 |
| School/University | 1.2 |
| Sports Arena | 1.1 |
| Town Hall | 1.1 |
| Transportation | 1.0 |
| Warehouse | 0.8 |
| Workshop | 1.4 |

Lost Opportunity Gross Energy Savings, Fossil Fuel

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Space heating energy consumption will increase due to reduced lighting load (cooler lighting fixtures).

Annual Oil Savings = -0.0007129 MMBtu's per annual kWh saved and Annual gas savings = -0.0003649 MMBtu's per kWh. See reference 4.

Lost Opportunity Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

$$KW(summer) = \left(CFL*(Allowable\ LPD - Actual\ LPD)*A + CF_{os}*\frac{\sum\limits_{n=1}^{N}O_{n}W_{n}}{1000} + CF_{hw}*\frac{\sum\limits_{n=1}^{N}DeltaW_{hw}}{1000}\right)*\left(1 + \frac{G}{COP}\right)$$

$$KW(\text{winter}) = \left(CFL*(Allowable\ LPD - Actual\ LPD)*A + CF_{os}*\frac{\sum\limits_{n=1}^{N}O_{n}W_{n}}{1000} + CF_{hw}*\frac{\sum\limits_{n=1}^{N}DeltaW_{hw}}{1000}\right)$$

CF_L and CF_{os} are the lighting/occupancy sensor coincidence factor (summer/winter) taken from Appendix 1.

Allowable LPD, in kW/ft2 = the value of Watts per ft2 from ASHRAE for the facility type divided by 1000.

Actual LPD, in kW/ft2 = Total Fixture Wattage (kW) divided by the Lighted Area, ft2

A = is calculated for each project, either from architectural drawings or by physical measurement.

CF_{hw} is the residential lighting coincidence factor (summer/winter) taken from Appendix 1.

 $DeltaW_{hw}$ = Delta watts of hardwired fluorescent fixtures in residential areas as calculated per Section 4.1.2 of this document.

G = 0.73

COP = 4.5 Note [3]

Changes from Last Version

The COP was modified from 2.4 to 4.5 to reflect higher estimated baseline efficiencies resulting from higher code requirements. The factors used to calculate the fossil fuel (oil and gas) energy penalty associated with more efficient lights were updated (Ref [4]).

References

[1] D. Maniccia B. Von Neida, and A. Tweed.
An analysis of the energy and cost savings potential of occupancy sensors for commercial lighting systems,
Illuminating Engineering Society of North America 2000 Annual Conference: Proceedings. IESNA: New
York, NY. Pp. 433-459.

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[2] The source of the equation for Sc and the derivation of the values for F is from "Calculating Lighting and HVAC Interactions," ASHRAE Journal 11-93 as used by KCPL.

- [3] ASHRAE 90.1-2007, TABLE 9.5.1: Lighting Power Densities Using the Building Area Method
- [4] Massachusetts Technical Reference Manual, 2012 Program Year, page 163

Notes

- [1] If sensors are installed, the heat emitted from lighting affected by this measure will decrease due to lower lighting power and use. This will result in increased space heating energy consumption.
- [2] In cases where both general building area type and a specific building area type are listed, the specific building area type shall apply.
- [3] Estimated based on Connecticut Code.
- [4] An analysis was conducted by Wood, Byk, and Associates, 829 Meadowview Road, Kennett Square, PA 19348, an engineering firm which was utilized to provide technical support for C&LM programs. The analysis was based on a DOE-2 default analysis and information was provided to David Bebrin (CL&P) on August 17, 2007.

2.2 HVAC & WATER HEATING

2.2.1 CHILLERS

Description of Measure

Installation of efficient water-cooled and air-cooled water chilling packages (chillers). Chillers must use an environmentally friendly refrigerant in order to qualify for the program.

Savings Methodology

Energy savings are custom calculated for each chiller installation based on the specific equipment, operational staging, operating profile, and load profile. A temperature bin model created by Bitterli & Associates (Ref [1]) is utilized to calculate the energy and demand savings for the chiller projects. Customer-specific information is used to estimate a load profile for the chilled water plant. Based on the loading, the chiller's actual part load performance is used to calculate chiller's demand (kW) and consumption (kWh) for each temperature bin. The spreadsheet is also used to calculate consumption for the baseline unit. The spreadsheet can also be used to calculate the consumption of the auxiliaries (chilled water pumps, condenser water pumps and cooling tower fans). The spreadsheet can be used to estimate savings for both electric and natural gas chilled water plants for up to two chillers per plant.

Inputs

| Symbol | Description | Units |
|--------|--|---------|
| | Facility occupancy hrs per week on and off-peak | h/wk |
| | Chiller plant availability per month | Y or N |
| | Peak cooling load @100°F (Occupied) | Tons |
| | Peak cooling load @100°F (Unoccupied) | Tons |
| | Economizer set point | °F |
| | Load at economizer set point (Occupied) | Tons |
| | Load at economizer set point (Unoccupied) | Tons |
| | Load at economizer set point + (Occupied) | Tons |
| | Load at economizer set point + (Unoccupied) | Tons |
| | Load at economizer set point - (Occupied) | Tons |
| | Load at economizer set point - (Unoccupied) | Tons |
| | Chiller(s) Capacity | Tons |
| | Condenser – Air or water cooled | |
| | Fuel – Electric or Gas | |
| | Compressor type | |
| | ARI part load efficiency @100% load, @75% load, @50% load, and @25% load | Ref [2] |
| | Primary and secondary pumping – Brake Horsepower (BHP) | Bhp |
| | Chilled water pump controls – single speed or Variable Frequency Drive (VFD) | |
| | Condenser water pump – BHP | Bhp |
| | Tower Fan – BHP | Bhp |
| | Tower fan control – single speed, 2 speed, VFD | _ |
| | Other (electric chiller kW not in part load performance, Gas chiller) | |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|--------|--------------------------------|----------|--------|----------|
| IPLV | Integrated Part Load Value | | | Ref [2] |
| BL100 | Baseline efficiency@ 100% load | Note [1] | | Ref [3] |
| BL75 | Baseline efficiency@ 75% load | | | |
| BL50 | Baseline efficiency@ 50% load | | | |
| BL25 | Baseline efficiency@ 25% load | | | |

Lost Opportunity Gross Energy Savings, Electric

Equipment

Each chiller plant is characterized by:

- Number of chillers,
- Sizes, in tons (the chillers may be of different sizes),
- Type, which may be:
 - Water-cooled centrifugal,
 - o Water-cooled screw and scroll, or
 - o Air-cooled
- Speed, constant or variable
- Auxiliary equipment
 - o Chilled water pumps
 - Cooling tower pumps
 - Cooling tower fans
 - Other

Operational Staging

If more than one chiller is used, their operational relationship can be defined. When the load is high enough to permit two chillers to operate, they can be designated to operate together at the same loading, or, alternatively, either one can be operated at full output while the other follows the cooling load profile.

Operating Profile

The customer's cooling load profile, for each of 12 months, is characterized by:

- On-peak occupied hours the chiller is operated each week,
- Off-peak occupied hours the chiller is operated each week,
- On-peak un-occupied hours the chiller is operated each week,
- Off-peak un-occupied hours the chiller is operated each week.

Load Profile

A customer's representative (typically design engineer) provides loads at various conditions. The customer's load profile is estimated by determining the load at the peak outdoor conditions and the load at the minimum conditions. For systems with an air-side or water-side economizer, the minimum conditions are those just above the set point of the economizer. If the customer's load profile is not known, a default load profile will be developed; in this case it is also necessary to determine the value of any process loads.

Savings Calculation

With the above information (chiller load and part load efficiencies) a calculation is made for each time period of the year based on the appropriate temperature bin data. The calculation is performed once for the chillers meeting the baseline efficiencies, Table 1, and again for the proposed chillers, and the difference determines the kWh and the kW savings for each period. These are summed to yield the total savings.

Table 1: Baseline Efficiencies for Electric¹ Chillers

| Equipment | Size Category | Units | Path A ² | | Path B ³ | |
|-----------------------|--|--------|------------------------|-------------------|------------------------|-------------------|
| Type | (tons) | | Full load ⁵ | IPLV ⁵ | Full Load ⁵ | IPLV ⁵ |
| Air Cooled | < 150 | EER | ≥9.562 | ≥12.500 | NA ⁴ | NA ⁴ |
| | ≥150 | EER | ≥9.562 | ≥12.750 | NA ⁴ | NA ⁴ |
| Water Cooled | <75 | kW/ton | ≤0.780 | ≤0.630 | ≤0.800 | ≤0.600 |
| Positive displacement | ≥ _{75 &} < ₁₅₀ | kW/ton | ≤0.775 | ≤0.615 | ≤0.790 | ≤0.586 |
| displacement | $\geq_{150 \&} <_{300}$ | kW/ton | ≤0.680 | ≤0.580 | ≤0.718 | ≤0.540 |
| | ≥300 | kW/ton | ≤0.620 | ≤0.540 | ≤0.639 | ≤0.490 |
| Water Cooled | < 150 | kW/ton | ≤0.634 | ≤0.596 | ≤0.639 | ≤0.450 |
| Centrifugal | $\geq_{150} \& <_{300}$ | kW/ton | ≤0.634 | ≤0.596 | ≤0.639 | ≤0.450 |
| | ≥300 & <600 | kW/ton | ≤0.576 | ≤0.549 | ≤0.600 | ≤0.400 |
| | ≥600 | kW/ton | ≤0.570 | ≤0.539 | ≤0.590 | ≤0.400 |

¹ Electric baseline used for natural gas chillers. For water cooled \leq 300 tons positive displacement is the baseline. For \geq 300 tons Centrifugal is the baseline.

Table 2: Baseline Part Load Efficiencies- Path A

| Equipment | Size Category | Units | Part Load Effi | iciencies | | |
|--------------|---------------|--------|----------------|-----------|----------|----------|
| Type | (tons) | | 100% Load | 75% Load | 50% Load | 25% Load |
| Air Cooled | < 150 | EER | 9.562 | 11.191 | 13.501 | 13.575 |
| | ≥150 | EER | 9.562 | 11.437 | 13.797 | 13.685 |
| Water Cooled | <75 | kW/ton | 0.780 | 0.671 | 0.561 | 0.815 |
| Positive | ≥75 & <150 | kW/ton | 0.775 | 0.655 | 0.547 | 0.799 |
| displacement | ≥150 & <300 | kW/ton | 0.680 | 0.617 | 0.516 | 0.766 |
| | ≥300 | kW/ton | 0.620 | 0.577 | 0.482 | 0.687 |
| Water Cooled | < 150 | kW/ton | 0.634 | 0.612 | 0.565 | 0.667 |
| Centrifugal | ≥150 & <300 | kW/ton | 0.634 | 0.612 | 0.565 | 0.667 |
| | ≥300 & <600 | kW/ton | 0.576 | 0.566 | 0.522 | 0.596 |
| | ≥600 | kW/ton | 0.570 | 0.555 | 0.512 | 0.590 |

Table 3: Baseline Part Load Efficiencies- Path B

| Equipment | Size Category | Units | Part Load Eff | ficiencies | | |
|-----------------------------|--|--------|---------------|------------|----------|----------|
| Type | (tons) | | 100% Load | 75% Load | 50% Load | 25% Load |
| Air Cooled | < 150 | EER | NA | NA | NA | NA |
| | ≥150 | EER | NA | NA | NA | NA |
| Water Cooled | <75 | kW/ton | 0.800 | 0.636 | 0.531 | 0.818 |
| Positive | ≥ _{75 &} < ₁₅₀ | kW/ton | 0.790 | 0.619 | 0.517 | 0.827 |
| displacement | ≥ ₁₅₀ & < ₃₀₀ | kW/ton | 0.718 | 0.573 | 0.479 | 0.721 |
| | ≥300 | kW/ton | 0.639 | 0.520 | 0.435 | 0.655 |
| Water Cooled Centrifugal | < 150 | kW/ton | 0.639 | 0.559 | 0.386 | 0.414 |
| | ≥ ₁₅₀ & < ₃₀₀ | kW/ton | 0.639 | 0.559 | 0.386 | 0.414 |
| | ≥300 & <600 | kW/ton | 0.600 | 0.498 | 0.344 | 0.358 |
| | ≥600 | kW/ton | 0.590 | 0.499 | 0.344 | 0.356 |

² Path A is intended for applications where significant operating time is expected at full load.

³ Path B is intended for applications where significant operating time is expected at part load.

⁴NA means that this requirement is not applicable and cannot be used for compliance.

⁵Rated based on Ref [2]

Lost Opportunity Gross Energy Savings, Fossil Fuel

The additional natural gas usage, if chillers are natural gas driven, is calculated on a site specific basis using the methodology shown above. The additional usage will be negative since it is an increase in natural gas over the electric baseline option.

Lost Opportunity Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

The peak demand savings from the spreadsheet are assumed to be 100% coincident to the ISO-NE Summer seasonal peak demand. There are no winter peak demand savings.

Non Energy Benefits

Because the baseline and high-efficiency technology are the same for electric chillers, the majority of the projects have no non-electric benefits. In the case of natural gas chillers, the gas chiller will have a higher maintenance cost than the baseline electric. In these cases, the non-electric benefit would be negative and calculated on a site-specific basis.

Changes from Last Version

Revised Notes 2 and 3 on Table 1 to be more consistent with ASHRAE 90.1-2007.

Notes

- [1] Bitterli & Associates, 10 Station Street, Floor 2, Simsbury, CT 06070-2220
- [2] Either EER for air cooled or kW/ton for water cooled, Part load performance based on ARI 550/590
- [3] Developed using typical chiller part load curves and the baseline efficiencies in Table 1. Table 1 is based on ANSI/ASHRAE/IESNA Standard 90.1-2007 with Addenda 2008 Supplement.

2.2.2 UNITARY AC & HEAT PUMPS

Description of Measure

Version Date: 10/30/2012

Installation of a high-efficiency Direct-Expansion (DX) unitary or split cooling system or air source heat pump.

Savings Methodology

Savings are estimated using full load hours analysis, comparing the difference in efficiency between a baseline (code compliant) and installed efficiency.

Inputs

| Symbol | Description | Units |
|-------------------|---|-------------|
| | Facility type served by equipment | |
| CAP_C | Installed Cooling Capacity | Btu/hr |
| CAP_H | Installed Heating Capacity | Btu/hr |
| EER _i | EER, ≥65,000 Btu/hr – Installed (ARI 340/360) | Btu/watt-hr |
| SEER _i | SEER, units < 65,000 Btu/hr – Installed (ARI 210/240) | Btu/watt-hr |
| HSPF _i | HSPF, Heat pumps < 65,000 Btu/hr – Installed (ARI | Btu/watt-hr |
| | 210/240) | |
| COP_i | High temperature COP, Heat pumps ≥65,000 Btu/hr- | |
| | Installed (ARI 340/360) | |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|-------------------|--|-------------|--------|------------|
| AKWH _C | Annual gross electric energy savings - Cooling | kWh | | |
| $AKWH_H$ | Annual gross electric energy savings - Heating | kWh | | |
| CAP_C | Installed Cooling Capacity | Btu/hr | | Input |
| CAP_H | Installed Heating Capacity | Btu/hr | | Input |
| CF_C | Seasonal summer cooling coincidence factor | % | | Appendix 1 |
| COP_b | High temperature COP, Heat pumps ≥65,000 Btu/h - Baseline | | | Note [1] |
| COP _i | High temperature COP, Heat pumps ≥65,000 Btu/h - Installed | Btu/watt-hr | | Input |
| EER _b | EER, \geq 65,000 Btu/h - Baseline | Btu/watt-hr | | Note [1] |
| EER _i | EER, \geq 65,000 Btu/h - Installed | Btu/watt-hr | | Input |
| EFLH _C | Equivalent Full Load Hours - Cooling | Hrs | | Appendix 5 |
| EFLH _H | Equivalent Full Load Hours - Heating | Hrs | | Appendix 5 |
| HSPF _b | HSPF, Heat pumps < 65,000 Btu/h - Baseline | Btu/watt-hr | | Note [1] |
| HSPF _i | HSPF, Heat pumps < 65,000 Btu/h - Installed | Btu/watt-hr | | Input |
| SEER _b | SEER, units < 65,000 Btu/h - Baseline | Btu/watt-hr | | Note [1] |
| SEER _i | SEER, units < 65,000 Btu/h - Installed | Btu/watt-hr | | Input |
| SKW _C | Seasonal Summer peak demand savings - Cooling | kW | | |
| WKW_H | Seasonal Winter peak demand savings - Heating | kW | 0 | |

Lost Opportunity Gross Energy Savings, Electric

Version Date: 10/30/2012

Cooling (A/C units and Air Source Heat Pumps)

$$AKWH_{C} = CAP_{C} \times \left(\frac{1}{EER_{b}} - \frac{1}{EER_{i}}\right) \times \frac{kW}{1000W} \times EFLH_{C}$$

Reminder: SEER used in place of EER for units under 65,000 Btu/h

Heating (Air source heat pumps only)

AKWH
$$_{H} = CAP_{H} \times \left(\frac{1}{HSPF_{b}} - \frac{1}{HSPF_{i}}\right) \times \frac{kW}{1000 W} \times EFLH_{H}$$

Reminder: COP multiplied by 3.412 can be used in place of HSPF for units \geq 65,000 Btu/h

Table 1: Baseline Efficiencies – Unitary and Split System AC (Note [1])

| Size (Btu/h) | Units With Electric | Units With Heating |
|-----------------------------------|---------------------|---------------------|
| | Resistance or No | Section Other Than |
| | Heating Section | Electric Resistance |
| <65,000 | 13.0 SEER | 13.0 SEER |
| \geq 65,000 and $<$ 135,000 | 11.2 EER | 11.0 EER |
| \geq 135,000 and \leq 240,000 | 11.0 EER | 10.8 EER |
| \geq 240,000 and \leq 375,000 | 10.0 EER | 9.8 EER |
| \geq 375,000 and $<$ 760,000 | 10.0 EER | 9.8 EER |
| \geq 760,000 | 9.7 EER | 9.5 EER |

Table 2: Baseline Efficiencies – Unitary and Split System Heat Pumps (Note [1])

| | Cooling Mode | Heating | |
|-----------------------------------|----------------------------|------------------------------------|------------|
| Size (Btu/h) | Units With Electric | s With Electric Units With Heating | |
| | Resistance or No | Section Other Than | db/43°F wb |
| | Heating Section | Electric Resistance | |
| <65,000 | 13.0 SEER | 13.0 SEER | 7.7 HSPF |
| \geq 65,000 and $<$ 135,000 | 11.0 EER | 10.8 EER | 3.3 COP |
| \geq 135,000 and \leq 240,000 | 10.6 EER | 10.4 EER | 3.2 COP |
| \geq 240,000 and \leq 375,000 | 9.5 EER | 9.3 EER | 3.2 COP |
| \geq 375,000 and $<$ 760,000 | 9.5 EER | 9.3 EER | 3.2 COP |
| ≥760,000 | 9.5 EER | 9.3 EER | 3.2 COP |

Lost Opportunity Gross Energy Savings, Example

A 120,000 Btu/hr rooftop A/C unit is installed on an office building. The new unit has a rated EER of 12.5. What are the annual lost opportunity savings?

Cooling (A/C units and Air Source Heat Pumps)

$$AKWH_{C} = CAP_{C} \times \left(\frac{1}{EER_{b}} - \frac{1}{EER_{c}}\right) \times \frac{kW}{1000W} \times EFLH_{C}$$

Version Date: 10/30/2012

From Appendix 5, the cooling equivalent full load hours for an office are 797 hours. EER_b from Table 1 = 11 EER

$$AKWH_{C} = 120,000 \times \left(\frac{1}{11} - \frac{1}{12.5}\right) \times \frac{kW}{1000W} \times 797 = 1,043kWh$$

Lost Opportunity Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

$$SKW_{C} = CAP_{C} \times \left(\frac{1}{EER_{b}} - \frac{1}{EER_{i}}\right) \times \frac{kW}{1000W} \times CF_{C}$$

$$WKW_{H} = 0$$

Reminder: Cooling only units have no winter demand savings since they do not operate during the winter. Air source heat pumps have no winter demand savings because they use resistance back up at low outside air temperatures.

Lost Opportunity Gross Peak Demand Savings, Example

A 120,000 Btu/h rooftop A/C unit is installed on an office building. The unit new unit has a rated EER of 12.5. What are the seasonal peak savings?

$$SKW_C = CAP_C \times \left(\frac{1}{EER_b} - \frac{1}{EER_i}\right) \times \frac{kW}{1000W} \times CF_C$$

From Appendix 1 the seasonal coincidence factor for cooling = 0.82. EER_b from table 1 = 11 EER

$$SKW_C = 120,000 \times \left(\frac{1}{11} - \frac{1}{12.5}\right) \times \frac{kW}{1000W} \times 0.82 = 1.07kW$$

$$WKW_{IJ} = 0$$

Cooling only units have no winter demand savings since they do not operate during the winter.

Changes from Last Version

Table 2 was added and minimum efficiencies were delineated based on heating section type. Heating capacity was added as input for heat pumps.

Notes

[1] Tables 1 and 2 above are based on 2009 International Energy Conservation Code (CT Code), which is consistent with ASHRAE 90.1-2007 with 2008 Supplement Addenda.

2.2.3 WATER AND GROUND SOURCE HP

Description of Measure

Version Date: 10/30/2012

High Efficiency water-source, ground water source, and ground-coupled heat pump units.

Savings Methodology

Savings are estimated using a full load hour analysis, comparing the difference in efficiency between a baseline (code compliant) and installed efficiency.

Inputs

| Symbol | Description | Units |
|------------------|--|-------------|
| | Facility type served by equipment and system type (water | |
| | source, ground water, ground loop) | |
| CAP_C | Installed Cooling Capacity | Btu/h |
| CAP_H | Installed Heating Capacity | Btu/h |
| EER _i | EER – installed (ISO 13256-1) | Btu/watt-hr |
| COPi | COP-Installed (ISO 13256-1) | |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|-------------------|--|-------------|--------|------------|
| $AKWH_C$ | Annual electric energy savings - cooling | kWh | | |
| $AKWH_H$ | Annual electric energy savings - Heating | kWh | | |
| CAP_C | Installed Cooling Capacity | Btu/hr | | Input |
| CAP _H | Installed Heating Capacity | Btu/hr | | Input |
| CF_C | Seasonal summer cooling coincidence factor | % | | Appendix 1 |
| CF _H | Seasonal summer Heating coincidence factor | % | | Appendix 1 |
| COP _b | High temperature COP, Heat pumps 65,000 Btu/h- | | | Note [1] |
| | Baseline | | | |
| COP_i | COP- installed | | | Input |
| EER _b | EER - Baseline | Btu/watt-hr | | Note [1] |
| EER _i | EER- installed | Btu/watt-hr | | Input |
| EFLH _C | Equivalent Full Load Hours - Cooling | Hrs | | Appendix 5 |
| EFLH _H | Equivalent Full Load Hours - Heating | Hrs | | Appendix 5 |
| SKW_C | Seasonal summer peak savings - cooling | kW | | |
| WKW_H | Seasonal Winter peak savings - Heating | kW | | |

Lost Opportunity Gross Energy Savings, Electric

Cooling

$$AKWH_{C} = CAP_{C} \times \left(\frac{1}{EER_{b}} - \frac{1}{EER_{i}}\right) \times \frac{kW}{1000W} \times EFLH_{C}$$

Heating

Version Date: 10/30/2012

$$AKWH_{H} = CAP_{H} \times \left(\frac{1}{COP_{h}} - \frac{1}{COP_{i}}\right) \times \frac{kW}{1000W} \times EFLH_{H}$$

Table 1: Baseline Efficiencies (Note [1])

| Water Source Heat Pump | • | | | | | |
|--|-------------------------|------------------|--|--|--|--|
| (Closed loop within a building, served by boiler and cooling tower) | | | | | | |
| Cooling Capacity Btu/hr | EER _b | COP _b | | | | |
| < 17,000 | 11.2 | 4.2 | | | | |
| ≥ 17,000 <135,000 | 12.0 | 4.2 | | | | |
| _ | | | | | | |
| Ground Water Heat Pump | | | | | | |
| (The water used by the heat pump is in co | ontact with the ground) | | | | | |
| Cooling Capacity Btu/hr | EER _b | COP _b | | | | |
| <135,000 | 16.2 | 3.6 | | | | |
| | | | | | | |
| Ground Loop Heat Pump | | | | | | |
| (The water used by the heat pump is isolated from contact with the ground) | | | | | | |
| Cooling Capacity Btu/hr | EER _b | COP _b | | | | |
| <135,000 | 13.4 | 3.1 | | | | |

Lost Opportunity Gross Energy Savings, Example

A ground loop water to air heat pump is installed in an office building. The heating capacity is 99,000 btu/hr with a COP of 3.5. The cooling capacity is 125,000 btu/h with an EER of 15. What are the annual lost opportunity savings?

Cooling

$$AKWH_{C} = CAP_{C} \times \left(\frac{1}{EER_{b}} - \frac{1}{EER_{i}}\right) \times \frac{kW}{1000W} \times EFLH_{C}$$

From Appendix 5 the cooling equivalent full load hours for an office are 797 hours. EER_b from table 1 = 13.4

$$AKWH_{C} = 125,000 \times \left(\frac{1}{13.4} - \frac{1}{15}\right) \times \frac{kW}{1000W} \times 797 = 793 \, kWh$$

Heating

$$AKWH_{H} = CAP_{H} \times \left(\frac{1}{COP_{b}} - \frac{1}{COP_{i}}\right) \times \frac{kW}{1000W} \times EFLH_{H}$$

From Appendix 5 the heating equivalent full load hours for an office are 1,248 hours. COP_b from table 1 = 3.1

$$AKWH_{H} = 99,000 \times \left(\frac{1}{3.1} - \frac{1}{3.5}\right) \times \frac{kW}{1000W} \times 1,248 = 4,555 \, kWh$$

Version Date : 10/30/2012

Lost Opportunity Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

Cooling

$$SKW_C = CF_C \times CAP_C \times \left(\frac{1}{EER_b} - \frac{1}{EER_i}\right) \times \frac{kW}{1000W}$$

Heating

$$WKW_H = CF_H \times CAP_H \times \left(\frac{1}{COP_b} - \frac{1}{COP_i}\right) \times \frac{kW}{1000W}$$

Lost Opportunity Gross Peak Demand Savings, Example

A 120,000 Btu/h water to air heat pump is installed in an office building. The heat pump is operated as a ground loop. The ground loop ratings for the unit are 18 EER and 4 COP. What are the seasonal demand savings?

Cooling

$$SKW_C = CF_C \times CAP_C \times \left(\frac{1}{EER_b} - \frac{1}{EER_i}\right) \times \frac{kW}{1000W}$$

From Appendix 1 the seasonal coincidence factor for cooling = 0.82. EER_b from table 1 = 13.4

$$SKW_C = 0.82 \times 125,000 \times \left(\frac{1}{13.4} - \frac{1}{15}\right) \times \frac{kW}{1000W} = 0.82 kW$$

Heating

$$WKW_H = CF_H \times CAP_H \times \left(\frac{1}{COP_b} - \frac{1}{COP_i}\right) \times \frac{kW}{1000W}$$

The seasonal coincidence factor is assumed to be the same as the summer factor = 0.82. COP_b from table 1 = 3.1

$$WKW_H = 0.82 \times 99,000 \times \left(\frac{1}{3.1} - \frac{1}{3.5}\right) \times \frac{kW}{1000W} = 3.0 \, kW$$

Notes

[1] The above Table 1 is based on 2009 International Energy Conservation Code (CT Code)

2.2.4 DUAL ENTHALPY CONTROLS

Description of Measure

Version Date: 10/30/2012

Upgrade to a dual enthalpy economizer instead of outside-air dry-bulb economizer. The system will continuously monitor the enthalpy of both the outside air and return air while controlling system dampers to adjust the outside quantity based on the two readings.

Savings Methodology

Wood, Byk and Associates (Note [1]) modeled the savings achieved by upgrading from single dry-bulb to dual enthalpy economizer control for a variety of typical commercial and industrial facility types and sizes using the hourly building simulation tool DOE-2. Simulation results were reviewed and annual electrical savings per ton calculated. The simulation revealed that summer and winter peak demand savings were zero because economizer cooling does not occur during the seasonal peaks.

Inputs

| Symbol | Description | |
|---------|--|------|
| CAP_i | Installed Cooling capacity controlled by economizers | Tons |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|----------|---|---------|--------|----------|
| ADET | Annual differential electrical energy savings per ton | kWh/Ton | 276 | Note [2] |
| $AKWH_C$ | Annual Electric Energy Savings, Cooling | kWh | | |
| CAPi | Installed Cooling capacity controlled by economizers | Tons | | Input |
| SKW | Summer Demand savings | kW | 0 | Note [2] |
| WKW | Winter Demand Savings | kW | 0 | Note [2] |

Lost Opportunity Gross Energy Savings, Electric

$$AKWH_C = ADET \times CAP_i$$

 $AKWH_C = 276 \times CAP_i$

Lost Opportunity Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

```
SKW = 0 (See Note [3])
WKW = 0 (See Note [3])
```

Notes

- [1] Wood, Byk, & Associates, Consulting Engineers, 829 Meadowview Road, Kennett Square, PA 19348
- [2] Results are from the modeling done by Wood, Byk, and Associates. The model provided savings for several locations throughout the Northeast. Savings for this measure is based on Hartford, CT.
- [3] Since economizers save when outdoor air temperature is relatively low outdoor temperature (<70 °F) and the seasonal peak is expected to occur at high outside air temperature the seasonal peak savings are assumed to be 0.

2.2.5 VENTILATION CO2 CONTROLS

Description of Measure

Version Date: 10/30/2012

Upgrade to CO2 control for outside air to an air handling system. The proposed systems monitor the CO2 in the spaces or return air and reduce the outside air when possible to save energy while meeting indoor air quality standards.

Savings Methodology

The energy savings are calculated based on site specific input for all projects. Savings are based on hours of operation, return air dry bulb temperature, return air enthalpy, system total air flow, percent outside air, estimated average outside air reduction, cooling and heating efficiencies. Savings are estimated using a temperature bin spreadsheet that calculates the reduction of outside air and the energy saved by not having to condition that air. The savings is calculated for each temperature bin with the exception of bins that would include economizer cooling.

Summer seasonal peak demand savings are calculated based on the top two temperature bins used in the spreadsheet. Natural gas peak day savings are calculated using the peak day factor for furnace/boiler of 0.0152 from measure 2.2.6 since the savings for this measure are consistent with the furnace/boiler savings profile.

The baseline for this measure is a system with no CO2 ventilation control.

Inputs

| Symbol | Description | Units | | | |
|--------|---|------------------|--|--|--|
| | Operation Schedule of HVAC Unit including days and time | | | | |
| | Area type Served by HVAC Unit | | | | |
| EER | Cooling Efficiency | Btu/watt-hr | | | |
| | Heating Efficiency | % | | | |
| | Total System Air Flow | CFM | | | |
| | Design Outside Air percentage | % | | | |
| | Expected occupancy | Number of people | | | |

2.2.6 GAS FIRED BOILER AND FURNACE

Description of Measure

Version Date: 10/30/2012

This measure encourages the installation of high-efficiency, gas-fired, hot water boilers and furnaces.

Savings Methodology

Energy savings are calculated using the efficiency of the proposed boiler or furnace versus the baseline efficiency. Baseline minimum efficiencies for boilers and furnaces are specified in ASHRAE 90.1-2007, Tables 6.8.1F and 6.8.1E, respectively.

The Peak day factors developed for this prescriptive approach are based on the results from a sampling of existing custom projects in which local bin weather data was used to calculate savings of both high-efficiency conventional and condensing boilers. The data from the temperature bin analysis was used to compute savings for the coldest 24-hour period of the year. The peak day factors were based on the average of these projects (Note [1]). Ratios of demand savings to annual energy savings were then developed for both conventional (0.0152) and condensing boilers (0.0133), as shown in the table below. The peak factor for furnaces is estimated at 0.0152 since furnace savings follow the same load shape as the conventional boilers. Although the magnitude of the demand savings for the condensing boilers was greater than that of the conventional boilers, the condensing boiler demand-to-energy-savings ratio was smaller. To meet the heating load, hot water reset increases the boiler water temperature as the outside air temperature decreases. The higher water temperature has a negative effect on the condensing boiler's efficiency at those conditions. The effect reduces the percent savings during the peak day.

Table 1: Annual and Peak (Demand) Savings Summary

| Building | Annual Savings (Ccf) | Peak Savings (Ccf) | Annual Savings (Ccf) | Peak Savings (Ccf) |
|----------|--|--------------------|--|--------------------|
| Number | Condensing Boilers | | Conventional Boilers | |
| 1 | 1,919 | 27 | 966 | 15 |
| 2 | 2,399 | 33 | 1,208 | 18 |
| 3 | 4,216 | 59 | 2,122 | 32 |
| 4 | 2,384 | 33 | 1,200 | 18 |
| 5 | 1,410 | 18 | 711 | 11 |
| 6 | 3,730 | 49 | 1,881 | 29 |
| 7 | 687 | 9 | 346 | 5 |
| 8 | 471 | 6 | 238 | 4 |
| 9 | 566 | 7 | 286 | 4 |
| 10 | 1,963 | 26 | 990 | 15 |
| 11 | 2,061 | 27 | 1,039 | 16 |
| 12 | 1,973 | 26 | 995 | 15 |
| 13 | 1,639 | 21 | 826 | 13 |
| 14 | 1,968 | 26 | 992 | 15 |
| 15 | 1,968 | 26 | 992 | 15 |
| 16 | 2,640 | 34 | 1,331 | 20 |
| 17 | 2,562 | 33 | 1,292 | 20 |
| Total | 34,556 | 460 | 17,416 | 265 |
| | Condensing Boiler: Peak-to-Annual Savings Ratio = 460/34,556 = 0.0133 | | Conventional Boiler: Peak-to-Annual Savings Ratio = 265/17,416 = 0.0152 | |

Version Date : 10/30/2012

Inputs

| Symbol | Description | Units |
|--------|----------------------------|--------|
| | Facility type | |
| ηр | Proposed case efficiency | |
| CAP | Boiler or furnace capacity | BTU/hr |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|--------|---------------------------------------|---------|---------|--|
| ACCF | Gross annual energy savings | CcF | | |
| CAP | Installed boiler or furnace capacity. | Btu/ hr | | |
| EFLH | Equivalent Full Load Hours | hours | Table 2 | See Appendix 5 for occupancy categories not listed below |
| OF | Oversize Factor | | | Note [2] |
| PD | Gross Peak Day Natural Gas Savings | | | |
| ηb | base case efficiency | | | ASHRAE 90.1-2007 |
| ηр | proposed case efficiency | | | |

Lost Opportunity Gross Energy Savings, Fossil Fuel

Heating Savings

$$ACCF = \frac{CAP}{OF} \times \left(\frac{EFLH}{102,900 \, {}^{Btu}/_{Ccf}}\right) \times \left(\frac{1}{\eta b} - \frac{1}{\eta p}\right)$$

Table 2: Equivalent Full Load Heating Hour Range (Note [1])

| Occupancy Category | Equivalent Full-Load Heating Hours | |
|--|------------------------------------|--|
| Residential, Hospitals, Police & Fire Stations (24/7 | 1,519 | |
| operation) | | |
| Manufacturing | 1,140 | |
| Retail Sales/Restaurants | 1,170 | |
| Offices | 1,306 | |
| Schools | 1,176 | |

Lost Opportunity Gross Peak Day Savings, Natural Gas

Conventional (non-condensing) boiler peak day gas savings (Ccf)

 $PD = 0.0152 \times ACCF$

Condensing boiler peak day gas savings (Ccf)

 $PD = 0.0133 \times ACCF$

Furnace peak day gas savings (Ccf)

 $PD = 0.0152 \times ACCF$

Changes from Last Version

Version Date: 10/30/2012

Made the oversize factor part of the equation.

Notes

- [1] Peak day factors and full load hours were developed by third party engineers (Fuss & O'Neill, Manchester, CT) in 2008 using a temperature bin analysis. The engineering analysis was provided to LDCs to help support natural gas conservation efforts.
- [2] The oversize factor (OF) is assumed to be 1.15 for single boiler/furnace installations reflecting the industry standard of installing equipment that has an output greater than estimated peak load. The oversizing factor for multiple boiler and furnace installation is 1.3 reflecting the industry practice of oversizing multiple pieces of equipment to allow for one piece of equipment to provide a higher percentage of load in emergency situations.

2.2.7 GAS RADIANT HEATER

Description of Measure

Version Date: 10/30/2012

Installation of gas-fired, low-intensity, vented, radiant heaters.

Savings Methodology

Energy savings is estimated to be 25% of the consumption of a conventional gas fired unit heater with the same heating load (based on Ref [1]).

Demand savings calculation methodology is based on the results of sample savings numbers for various building types using a temperature bin model. To calculate the peak demand factor the savings from the coldest 24-hour period of the year was divided by the total savings (See Note [1]). From this, ratios of the demand savings (Ccf) to annual energy savings (Ccf) were developed, resulting in the average demand savings fraction of annual savings of 0.00544.

Inputs

| Symbol | Description |
|--------|--------------------------------------|
| Cap | Installed heating Capacity in Btu/hr |
| | Facility type |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|--------|--|-------|----------|----------|
| ACCF | Gross annual gas energy savings | Ccf | | |
| Ccf | 100 Cubic Feet | Ccf | | |
| | The equivalent hours that the heater would need to operate | | Table 1, | Note [3] |
| EFLH | at its peak capacity in order to consume its estimated | | Appendix | |
| | consumption (Annual Btu's/ Full Load Btuh) | hours | 5 | |
| Cap | Installed heating Capacity in Btu/hr | | | Note [2] |
| OF | Oversize Factor | | | Note [2] |
| PD | Gross peak day savings | | | |
| SFR | Savings Fraction | | 25% | Ref [1] |
| ηb | base case efficiency | | 80% | Ref [2] |

Lost Opportunity Gross Energy Savings, Fossil Fuel

Heating Savings

$$ACCF = \frac{CAP}{OF} * EFLH * \frac{SFR}{(102,900btu / Ccf \times \eta b)}$$

Table 1: Equivalent Full-Load Heating Hour Range (Note [3])

| - 11-11-11-11-11-11-11-11-11-11-11-11-11 | | | |
|--|---|--|--|
| Occupancy Category | Equivalent Full-Load Heating Hours | | |
| Warehouse, Storage, Fire Stations (24/7 operation) | 1,519 | | |
| Manufacturing | 1,140 | | |
| Retail Sales/Other | 1,170 | | |

Lost Opportunity Gross Peak Day Savings, Natural Gas

PD= 0.00544 x ACCF

Version Date: 10/30/2012

Changes from Last Version

Added the oversize factor (OF) to the Heating Savings equation.

References

- [1] ASHRAE Technical Paper #4643, "Evaluation of an Infrared Two-Stage Heating System in a Commercial Application" ,2003, Conclusions page 138.
- [2] ASHRAE Standard 90.1-2007, Table 6.8.1E, for warm air unit heaters.

Notes

- [1] Peak day factors and full load hours were developed by third party engineers (Fuss & O'Neill, Manchester, CT) in 2008 using a temperature bin analysis. The engineering analysis was provided to LDCs to help support natural gas conservation efforts.
- [2] In the case of a single-heater installation, the oversize factor is 1.0. In the case of a multiple-heater installation, the total heater output capacity shall be used and the oversize factor is 1.1.
- [3] The equivalent full-load heating hour (EFLH) range is shown in Table 1. The magnitude of the EFLH's in each occupancy category considers both hours occupied and internal heat release equipment. Refer to Appendix 5 for occupancy categories not listed in Table 1.

2.2.8 GAS FIRED DHWH

Description of Measure

Installation of high-efficiency, gas-fired, storage-type, domestic hot water heaters>75,000 Btu/hr.

Savings Methodology

Energy savings are calculated using proposed water heater thermal efficiency and standby losses versus baseline efficiency and standby losses. The baseline for efficiency and standby losses were based on gas storage water heater, >75,000 Input Btu/hr as specified in ASHRAE 90.1-2007 (Ref [1]).

Based on facility type and square footage, Table 1 (Note [1]) and baseline standby losses are used to estimate the annual water heating baseline usage. Using the baseline efficiency (80%) the baseline hot water load is calculated. Using the calculated load, the installed efficiency and standby high efficiency consumption and savings can be calculated.

The demand savings is calculated using a demand savings factor, which is essentially the peak day consumption percent of the annual consumption. Multiplying annual savings by the demand savings factor determines the peak day savings.

Assumptions:

- 1. Base case heater is a code-compliant storage gas heater
- 2. Proposed case heater is a high-efficiency heater
- 3. Base case and proposed case heaters have the same output capacity and address the same DHW load.
- 4. If multiple heaters are used, they are treated as a single unit, with system input capacity and standby loss rate equal to the sum of all units.

Demand Assumptions:

- 1. Lowest cold water temperature is 44°F (Ref [3])
- 2. Annual average cold water temperature is 54°F. (Ref [3])
- 3. Hot water set point is 130°F.

Inputs

| Symbol | Description | Units |
|-------------|--|-----------------|
| $CAP_{H,i}$ | Input capacity of proposed (installed) water | MBH |
| | heater | |
| $CAP_{W,i}$ | Water Storage capacity of proposed (installed) | Gallons |
| | water heater | |
| ηb | Thermal efficiency of base case water heater | % |
| ηρ | Thermal efficiency of proposed (installed) water | % |
| | heater | |
| SLR_i | Standby loss rate of proposed (installed) water | Btu/hr |
| | heater | |
| A | Building floor area, square feet | ft ² |
| | Building Occupancy Type | |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|--------|------------------------------------|-----------------|--------|----------|
| A | Building floor area in square feet | ft ² | | Input |
| ACCF | Annual Natural Gas Energy Savings | Ccf/yr | | |

| Symbol | Description | Units | Values | Comments |
|------------------|--|-------------------------|---------|----------|
| $CAP_{H,b}$ | Heat Input capacity of base case water heater | MBH | | |
| $CAP_{H,i}$ | Heat Input capacity of proposed (installed) water heater | MBH | | Input |
| $CAP_{W,b}$ | Water Storage capacity of base case water heater | Gallons | | |
| $CAP_{W,i}$ | Water Storage capacity of proposed (installed) water heater | Gallons | | Input |
| $CCF_{W,b}$ | Annual base case DHW Gas usage | Ccf/yr | | |
| E_b | Annual base case gas energy usage rate (per sq ft ²) | Ccf/ft ² /yr | Table 1 | Ref [2], |
| | | | | Note [1] |
| $\mathbf{E_{i}}$ | Annual proposed (installed) gas energy usage rate (per ft ²) | Ccf/ft ² /yr | | |
| GPY_W | Annual Building Hot Water Usage | Gal/yr | | |
| H | Number of annual standby hours | Hrs/yr | | |
| PD | Peak Day Natural Gas Savings | Ccf | | |
| SF | Peak Day Gas Demand Savings factor | | | |
| SLR _b | Base case water heater standby loss rate | Btu/hr | | |
| SLR _i | Proposed (installed) water heater standby loss rate | Btu/hr | | Input |
| ΔΤ | Differential Temperature rise | °F | 75°F | |
| ηb | Base case water heater thermal efficiency | % | 80% | Ref [1] |
| ηρ | Thermal efficiency of proposed water heater | % | | |

Lost Opportunity Gross Energy Savings, Fossil Fuel

Natural Gas Energy Savings

Calculate annual base case DHW gas usage:

$$CCF_{W,b} = A \times E_b$$

Table 1: Annual Base Case Gas Usage Rate by Occupancy Type (Ref [2], Note [1]))

| Building Occupancy | Building Occupancy | Annual Base Case Gas Usage Rate, |
|-----------------------------|---------------------------|----------------------------------|
| Category | Code Number | $E_b(Ccf/ft^2)$ |
| Education | 1 | 0.048 |
| Grocery/Convenience Store | 2 | 0.029 |
| Restaurant/Cafeteria | 3 | 0.363 |
| Inpatient Health Care | 4 | 0.357 |
| Outpatient Health Care | 5 | 0.032 |
| Lodging | 6 | 0.265 |
| Retail (other than in mall) | 7 | 0.009 |
| Retail (in mall) | 8 | 0.028 |
| Office | 9 | 0.015 |
| Police/Fire Station/Jail | 10 | 0.137 |
| Other | 11 | 0.009 |

Calculate base case heater input capacity in BTU/hr:

$$CAP_{H,b} = CAP_{H,i} \times \frac{\eta p}{\eta b}$$

Calculate the baseline standby losses:

$$SLR_b = CAP_{H,i} \times \frac{1,000}{800} + 110 \times \sqrt{CAP}_{w,i} \text{ Ref [1]}$$

Calculate number of standby hours/year:

$$H = \frac{(8760 \, \frac{hr}{y_{yr}} \times CAP_{H,b} \times 1,000) - (CCF_{W,b} \times 102,900 \, \frac{Btu}{Ccf})}{(CAP_{H,b} \times 1,000) - \frac{SLR_b}{\eta b}}$$

Calculate annual building hot water usage (Gal hot water consumed/yr):

$$GPY_{W} = \frac{\left(CCF_{W,b} \times 102,900 \frac{Btu}{Ccf} \times \eta b\right) - \left(SLR_{b} \times H\right)}{\Delta T \times 8.33 \frac{Btu}{Gal^{\circ}F}}$$

Calculate annual gas savings using the following equation:

$$ACCF_{W} = CCF_{W,b} - \frac{(GPY_{W} \times \Delta T \times 8.33 \frac{Btu}{Gal^{\circ}F} + SLR_{i} \times H)}{102,900 \frac{Btu}{Ccf} \times \eta p}$$

Lost Opportunity Gross Energy Savings, Example

A 50,000 square foot inpatient health care facility installs a new energy efficient gas storage type domestic hot water heater with the following ratings:

- Capacity = 300 MBH
- Storage capacity = 100 gallons
- Thermal Efficiency = 91%
- Rated standby loss = 1,044 btu/hr

What are the annual energy savings?

Calculate annual base case DHW gas usage:

$$CCF_{W,b} = A \times E_b = 50,000 \times 0.357 = 17,850Ccf$$

Calculate base case heater input capacity in BTU/hr:

$$CAP_{H,b} = CAP_{H,i} \times \frac{\eta p}{\eta b} = 300 \times \frac{0.91}{0.80} = 341 \text{ MBH}$$

Calculate the baseline standby losses:

$$SLR_b = CAP_{H,i} \times \frac{1,000}{800} + 110 \times \sqrt{CAP}_{w,i} = 300 \times \frac{1,000}{800} + 110 \times \sqrt{100} = 1,475$$

Calculate number of standby hours/year:

$$H = \frac{\left(8760 \frac{hr}{yr} \times CAP_{H,b} \times 1,000\right) - \left(CCF_{W,b} \times 102,900 \frac{Btu}{Ccf}\right)}{\left(CAP_{H,b} \times 1,000\right) - \frac{SLR_b}{\eta b}}$$

$$H = \frac{\left(8760 \frac{hr}{yr} \times 341 \times 1,000\right) - \left(17,850 \times 102,900 \frac{Btu}{Ccf}\right)}{\left(341 \times 1,000\right) - \frac{1,475}{0.80}} = 3,392$$

Calculate annual building hot water usage (Gal hot water consumed/yr):

$$GPY_{W} = \frac{\left(CCF_{W,b} \times 102,900 \frac{Btu}{Ccf} \times \eta b\right) - \left(SLR_{b} \times H\right)}{\Delta T \times 8.33 \frac{Btu}{Cod^{\circ} F}}$$

$$GPY_{W} = \frac{(17,850 \times 102,900 \frac{Btu}{Ccf} \times 0.8) - (1,475 \times 3,392)}{75 \times 8.33 \frac{Btu}{Gal^{\circ}F}} = 2,343,992$$

Calculate annual gas savings using the following equation:

$$ACCF_{W} = CCF_{W,b} - \frac{(GPY_{W} \times \Delta T \times 8.33 \frac{Btu}{Gal^{\circ}F} + SLR_{i} \times H)}{102,900 \frac{Btu}{Ccf} \times \eta p}$$

$$ACCF_{W} = 17,850 - \frac{(2,343,992 \times 75 \times 8.33^{Btu}/_{Gal.^{\circ}F} + 1,044 \times 3,392)}{102,900^{Btu}/_{Cef} \times 0.91} = 2,173$$

Lost Opportunity Gross Peak Day Savings, Natural Gas

$$SF = \frac{1 \, day \times (130^{\circ}F - 46^{\circ}F)}{365 \, days \times (130^{\circ}F - 57^{\circ}F)} = 0.0032$$

$$PD = ACCF_w \times SF = ACCF_w \times 0.0032$$

Changes from Last Version

Modified the peak day savings factor.

References

- [1] ASHRAE 90.1-2007, Table 7.8.
- [2] U.S. Energy Information Administration Table E8A.Natural Gas Consumption and Energy Intensities by End Use for All Buildings, 2003
- [3] Tool for Generating Realistic Residential Hot Water Event Schedules, Reprint, NREL, August 2010.

Notes

[1] The published Ccf/ft² data in Ref [1] reflects existing DHW heating equipment performance. To factor in the increase in baseline efficiency from 2003, Fuss & O'Neill, Inc. provided and analysis comparing installed efficiency in 2003 to code-compliant efficiency. The published data (Ref [2]) was adjusted downward by a factor of 0.935 based on the analysis. The adjusted data is shown Table 1.

2.3 MOTORS AND TRANSFORMERS

2.3.2 LOW VOLTAGE DRY TYPE DISTRIBUTION TRANSFORMERS

Description of Measure

Version Date: 10/30/2012

Installation of high efficiency three phase low voltage dry type transformers, based on the Consortium for Energy Efficiency's (CEE) distribution transformers initiative.

Savings Methodology

Energy savings are based on the difference between baseline efficiency and CEE tier 1 or 2 level efficiencies. CEE Tier 1 level will demonstrate approximately 30% less total energy losses, as compared to the baseline. CEE Tier 2 performance level will demonstrate 46-50% less total energy losses, as compared to the baseline. The load is assumed to be constant at 35% of rated capacity, which is consistent with Reference [1].

The baseline efficiencies are based on the Federal Standard (Ref [1]) and listed in the table below.

Table 1: Baseline Efficiencies, Three Phase Low Voltage Transformers

| | Baseline Efficiency | CEE Tier 1 | CEE Tier 2 |
|-------|---------------------|------------|------------|
| kVA | (Federal Standard) | Efficiency | Efficiency |
| 15 | 97.0% | 97.90% | 98.40% |
| 30 | 97.5% | 98.25% | 98.65% |
| 45 | 97.7% | 98.39% | 98.78% |
| 75 | 98.0% | 98.60% | 98.93% |
| 112.5 | 98.2% | 98.74% | 99.03% |
| 150 | 98.3% | 98.81% | 99.10% |
| 225 | 98.5% | 98.95% | 99.40% |
| 300 | 98.6% | 99.02% | 99.44% |
| 500 | 98.7% | 99.09% | 99.51% |
| 750 | 98.8% | 99.16% | 99.56% |
| 1000 | 98.9% | 99.23% | 99.59% |

Inputs

| Symbol | Description |
|--------|------------------------|
| kVA | Kilovolt-Ampere Rating |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|--------|--------------------------------------|---------------------|--------|----------|
| AKWH | Annual Gross Electric Energy savings | kiloWatt-hours, kWh | | |
| kW | Electric Demand | kiloWatts | | |

Lost Opportunity Gross Energy Savings, Electric

The energy savings are stipulated based on the CEE tier level as shown in the table below.

Table 2: Stipulated Energy Savings

Version Date: 10/30/2012

| Losses(kWh/Yr) | | | Savings (AKWH) | | |
|----------------|----------|------------|----------------|------------|------------|
| kVA | Baseline | CEE Tier 1 | CEE Tier 2 | CEE Tier 1 | CEE Tier 2 |
| 15 | 1,380 | 966 | 736 | 414 | 644 |
| 30 | 2,300 | 1,610 | 1,242 | 690 | 1,058 |
| 45 | 3,173 | 2,221 | 1,683 | 952 | 1,490 |
| 75 | 4,599 | 3,219 | 2,460 | 1,380 | 2,139 |
| 112.5 | 6,209 | 4,346 | 3,346 | 1,863 | 2,863 |
| 150 | 7,818 | 5,473 | 4,139 | 2,345 | 3,679 |
| 225 | 10,348 | 7,243 | 4,139 | 3,104 | 6,209 |
| 300 | 12,877 | 9,014 | 5,151 | 3,863 | 7,726 |
| 500 | 19,929 | 13,950 | 7,512 | 5,979 | 12,417 |
| 750 | 27,594 | 19,316 | 10,118 | 8,278 | 17,476 |
| 1000 | 33,726 | 23,608 | 12,571 | 10,118 | 21,155 |

Lost Opportunity Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

The average hourly demand savings for both winter and summer are:

$$kW = \frac{AKWH}{8760}$$

| | Losses(kW) | | | Savings (kW) | |
|-------|------------|------------|------------|--------------|------------|
| kVA | Baseline | CEE Tier 1 | CEE Tier 2 | CEE Tier 1 | CEE Tier 2 |
| 15 | 0.16 | 0.11 | 0.08 | 0.047 | 0.074 |
| 30 | 0.26 | 0.18 | 0.14 | 0.079 | 0.121 |
| 45 | 0.36 | 0.25 | 0.19 | 0.109 | 0.170 |
| 75 | 0.53 | 0.37 | 0.28 | 0.158 | 0.244 |
| 112.5 | 0.71 | 0.50 | 0.38 | 0.213 | 0.327 |
| 150 | 0.89 | 0.62 | 0.47 | 0.268 | 0.420 |
| 225 | 1.18 | 0.83 | 0.47 | 0.354 | 0.709 |
| 300 | 1.47 | 1.03 | 0.59 | 0.441 | 0.882 |
| 500 | 2.28 | 1.59 | 0.86 | 0.683 | 1.418 |
| 750 | 3.15 | 2.21 | 1.16 | 0.945 | 1.995 |
| 1000 | 3.85 | 2.70 | 1.44 | 1.155 | 2.415 |

Changes from Last Version

New measure

References

[1] Federal Standard: Title 10 Part 431 - Energy Efficiency Program for Certain Commercial and Industrial Equipment; Section 431.196

Version Date: 10/30/2012 2.4.1 HVAC VFD

2.4 VARIABLE FREQUENCY DRIVES

2.4.1 HVAC VFD

Description of Measure

Addition of variable frequency (VFD) control to a fan or pump system in a HVAC application. The fan (pump) speed will be controlled to maintain the desired system pressure. The application must have a load that varies and proper controls (i.e. two-way valves, Variable Air Volume boxes) must be installed.

Savings Methodology

The baseline is a constant speed fan (Air Foil (AF), Backward incline (BI), Forward Curved (FC)) with or without inlet guide vanes or a constant speed pump. ASHRAE default performance curves (Ref [1]) are utilized to calculate the power for both the baseline equipment (constant speed) and the proposed equipment (variable speed) over the annual load profile. The difference between the base and proposed equipment determines the energy savings. Demand savings is the power (kW) savings at the highest load temperature bins.

Inputs

| Symbol | Description | Units |
|--------|----------------------------|-------|
| ВНР | Brake Horsepower | |
| EFFi | Installed Motor Efficiency | |
| Н | Annual Hours of Operation | |
| | Fan type | |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|-------------|--|---------|---------|-------------------------------------|
| AF | Air Foil | | | Fan Type |
| AKWH | Gross Annual Electric Energy Savings | kWh | | |
| BHP | System brake horsepower | HP | | |
| BI | Backward incline | | | Fan Type |
| CHWP | Chilled Water Pump | | | |
| EFF_{i} | Motor Efficiency - installed | % | | |
| FC | Forward Curved | | | Fan Type |
| Н | Annual Hours of operation | | | site specific or default Appendix 5 |
| HWP | Hot Water Pump | | | |
| IGV | Inlet Guide Vanes | | | Flow Control Device |
| SF_{kWh} | Annual kilowatt hour savings factor based on | (kW/HP) | Table 1 | |
| | typical load profile for application | | | |
| $SF_{kW,S}$ | Summer seasonal demand savings based on | (kW/HP) | Table 1 | |
| | typical load profile for application | | | |
| $SF_{kW,W}$ | Summer seasonal demand savings based on | (kW/HP) | Table 1 | |
| | typical load profile for application | | | |
| SKW | Seasonal Summer Peak Savings | kW | | |
| WKW | Seasonal Winter Peak Savings | kW | | |

Version Date: 10/30/2012 2.4.1 HVAC VFD

Lost Opportunity Gross Energy Savings, Electric

$$AKWH = \frac{BHP}{EFF_i} \times H \times SF_{kWh}$$

Refer to Table 1 below for the appropriate SF_{kWh}.

Table 1: VFD Savings Factors (See Note [1])

| HVAC Fan VFD Savings Factors | | | | | | |
|------------------------------|--------------|-------------|-------------|--|--|--|
| Baseline | SF_{kWh} | $SF_{kW,S}$ | $SF_{kW,W}$ | | | |
| AF/BI | 0.35407485 | 0.26035565 | 0.40781240 | | | |
| AF/BI IGV | 0.22666226 | 0.12954823 | 0.29144821 | | | |
| FC | 0.17889831 | 0.13552275 | 0.18745625 | | | |
| FC IGV | 0.09210027 | 0.02938371 | 0.13692166 | | | |
| HVAC Pum | p VFD Saving | s Factors | | | | |
| System | SF_{kWh} | $SF_{kW,S}$ | $SF_{kW,W}$ | | | |
| CHWP | 0.41113751 | 0.299056883 | 0.0 | | | |
| HWP | 0.42380136 | 0.0 | 0.207967853 | | | |

Lost Opportunity Peak Seasonal Demand Savings, Electric (Winter and Summer)

$$SKW = \frac{BHP}{EFF_i} \times SF_{kW,S}$$

$$WKW = \frac{BHP}{EFF_i} \times SF_{kW,W}$$

References

[1] ASHRAE 90.1-1989 User's Manual

Notes

[1] The constants in Table 1 were derived using a temperature BIN spreadsheet and typical heating, cooling and fan load profiles. For each pump application and fan type savings factors were developed. These were based on the difference in power based on the estimated load at each temperature BIN using equations from Ref [1].

2.5 REFRIGERATION

2.5.3 VENDING MACHINE OCCUPANCY CONTROLS

Description of Measure

Version Date: 10/30/2012

Vending machine occupancy sensors power down refrigerated vending machines when the surrounding area is vacant. These controls will also automatically re-power the unit at dynamic intervals to maintain product temperature.

Savings Methodology

The energy savings are based on a study performed by Nicholas Group, P.C. in 2001. No demand savings are claimed.

Inputs

| Symbol | Description | |
|--------|----------------------------|--|
| | Number of vending machines | |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|--------|--------------------------------------|--------------|-----------------------|--------------|
| AKWH | Annual Gross Electric Energy savings | kWh per year | 1,600 kWh per vending | Prescriptive |
| | | | machine (Ref [1]) | |

Lost Opportunity Gross Energy Savings, Electric

AKWH = 1,600 kwh per vending machine

References

[1] Vending Miser Monitoring Project, Final Report, Nicholas Group, P.C., April 2001.

Version Date: 10/30/2012

2.6 OTHER

2.6.1 LEAN MANUFACTURING

Description of Measure

Incorporating Process Re-engineering for Increased Manufacturing Efficiency (PRIME), also known as "lean manufacturing," into the manufacture process.

Savings Methodology

Incorporating PRIME in the manufacturing process allows a company to eliminate waste (i.e. of energy, materials, labor) and optimize flow in order to improve the efficiency of the manufacturing process. The savings calculations are based on Ref [1]. Savings are estimated based on facility's existing actual annual electrical usage. The savings are based on estimating the production increase with and without PRIME.

Savings are based on two concepts:

- 1. Producing more products in the same time period saves on the non-manufacturing consumption (mostly lighting).
- 2. Producing more products over the same time period reduces losses in the manufacturing equipment consumption (such as less idle time and increase in motor efficiency).

The PRIME process also reduces waste. Since this is very site dependent it is not considered in this calculation

Inputs

| Symbol | Description | Units |
|---------|--|------------|
| KWH_h | Facility's annual consumption based on billing history | kWh |
| PPA | Percent of facility's consumption effected by PRIME | % |
| Na | Production after PRIME | # per hour |
| Ne | Existing Production | # per hour |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|------------------|--|------------|--------|----------|
| AKWH | Annual Electric Energy Savings | kWh | | |
| EKWH | Estimated annual electric usage with increase in production | kWh | | |
| IND | Annual electric energy usage independent of production hours and production quantity | kWh | | |
| HR | Annual electric energy usage dependent on hours of production | kWh | | |
| KWH _h | Facility's annual electric usage based on billing history | kWh | | Input |
| N_a | Production rate after PRIME | # per hour | | Input |
| N _e | Existing Production rate | # per hour | | Input |
| PPA | Percent of facility's energy usage effected by PRIME | % | | Input |
| PD | Annual electric energy usage dependent on production quantity | kWh | | |
| SF | Savings factor | % | | Ref [1] |
| ···wop | Without PRIME | | | |
| ···wp | With PRIME | | | |

Version Date : 10/30/2012

Lost Opportunity Gross Energy Savings, Electric

$$AKWH = EKWH_{wop} - EKWH_{wp}$$

Estimated annual consumption with increase in productivity without PRIME:

$$EKWH_{wop} = IND_{wop} + HR_{wop} + PD_{wop}$$

$$IND_{won} = 0.65 \times PPA \times KWH_{h}$$

$$HR_{wop} = 0.20 \times PPA \times KWH_h \times \frac{N_a}{N_a}$$

$$PD_{wop} = 0.15 \times PPA \times KWH_h \times \frac{N_a}{N_e}$$

Estimated annual consumption with increase in productivity with PRIME:

$$EKWH_{wp} = IND_{wp} + HR_{wp} + PD_{wp}$$

$$IND_{wp} = 0.65 \times PPA \times KWH_h$$

$$HR_{wp} = 0.20 \times PPA \times KWH_{h}$$

$$PD_{wp} = 0.15 \times PPA \times KWH_h \times \frac{N_a}{N_a} \times (1 - SF)$$

$$SF = 0.1168 \times \left[\frac{N_a - N_e}{N_e} \right]^3 - 0.3402 \times \left[\frac{N_a - N_e}{N_e} \right]^2 + 0.4732 \times \left[\frac{N_a - N_e}{N_e} \right] + 0.0011$$

Savings algorithms come directly from Reference [1].

Lost Opportunity Gross Energy Savings, Example

A manufacturing plant that has an annual electricity consumption of 1,000,000 kWh (KWH_h), It goes though the PRIME process on production lines that represent 25% or 0.25 (PPA) of their production. Production of those lines increase from 300 to 330 products per hour.

$$AKWH = EKWH_{wop} - EKWH_{wp}$$

Estimated annual consumption with increase in productivity without PRIME:

$$EKWH_{wop} = IND_{wop} + HR_{wop} + PD_{wop}$$

$$IND_{wop} = 0.65 \times 0.25 \times 1,000,000 = 162,500 kWh$$

$$HR_{wop} = 0.20 \times 0.25 \times 1,000,000 \times \frac{330}{300} = 55,000 kWh$$

$$PD_{wop} = 0.15 \times 0.25 \times 1,000,000 \times \frac{330}{300} = 41,250 \text{kWh}$$

$$EKWH_{wop} = 162,500 + 55,000 + 41,250 = 258,750kWh$$

Version Date: 10/30/2012

Estimated annual consumption with increase in productivity with PRIME:

$$EKWH_{wp} = IND_{wp} + HR_{wp} + PD_{wp}$$

$$IND_{wp} = 0.65 \times 0.25 \times 1,000,000 = 162,500 kWh$$

$$HR_{wn} = 0.20 \times 0.25 \times 1,000,000 = 50,000 kWh$$

$$SF = 0.1168 \times \left[\frac{330 - 300}{300} \right]^{3} - 0.3402 \times \left[\frac{330 - 300}{300} \right]^{2} + 0.4732 \times \left[\frac{330 - 300}{300} \right] + 0.0011 = .045$$

$$PD_{wp} = 0.15 \times 0.25 \times 1,000,000 \times \frac{330}{300} \times (1 - 0.045) = 39,394 kWh$$

$$EKWH_{wp} = 162,500 + 50,000 + 39,394 = 251,894kWh$$

$$AKWH_0 = 258,750 - 251,894 = 6,856kWh$$

Lost Opportunity Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

SKW = 0

WKW = 0

Non Energy Benefits

The customer's cost savings from the increase in productivity and reduction in scrap varies considerably from project to project. Therefore, it may be calculated on a case-by-case basis.

References

[1] Process Reengineering for Increased Manufacturing Efficiency (PRIME) Program Evaluation, Energy & Resource Solutions, March 26, 2007, Section 4.

2.6.2 COMMERCIAL KITCHEN EQUIPMENT

Description of Measure

Version Date: 10/30/2012

Installation of ENERGY STAR qualified commercial kitchen equipment.

Savings Methodology

Energy savings for this measure are calculated using the savings calculator for ENERGY STAR qualified commercial kitchen equipment located on the ENERGY STAR website (Ref [1]). Note that the input and equipment tabs within the spreadsheet have default values that can be overridden by the user when project specific details are available. The peak electric and gas demand savings are calculated as specified below. The baselines from which savings are calculated are provided in Table below.

Table 1: Savings Baseline

| Tuble 1. Suvings Busenie | | | |
|--------------------------|--|--|--|
| Equipment | Baseline | | |
| Convection Oven | Conventional unit per Reference [1] calculator | | |
| Dishwasher | Conventional unit per Reference [1] calculator | | |
| Freezer | Reference [3] | | |
| Fryer | Conventional unit per Reference [1] calculator | | |
| Griddle | Conventional unit per Reference [1] calculator | | |
| Hot Food Holding Cabinet | Conventional unit per Reference [1] calculator | | |
| Ice Machine | Reference [2] | | |
| Refrigerator | Reference [3] | | |
| Steam Cooker | Conventional unit per Reference [1] calculator | | |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|-------------------|---|------------|--------|----------|
| ACCF _o | Annual Natural gas savings | Ccf | | |
| AHAM | Association of Home Appliance Manufacturers | | | |
| AKWH | Annual Gross Electric Energy savings | kiloWatt- | | |
| | | hours, kWh | | |
| AKW | Average Hourly Summer Demand Savings | kW | | |
| kW | Electric Demand | kiloWatts | | |
| PD_{O} | Peak day gas savings | Ccf | | |

Lost Opportunity Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

The average hourly demand savings for refrigerators, freezers and ice machines (winter and summer) are:

$$AKW = \frac{AKWH}{8760 \frac{hrs}{yr}}$$

Lost Opportunity Gross Peak Demand Savings, Natural Gas

$$PD_o = \frac{ACCF_o}{365 days / yr}$$

Version Date: 10/30/2012

Changes from Last Version

Combined refrigerators and freezers into this measure. Refer to ENERGY STAR website (www.EnergyStar.gov) for savings calculator.

References

- [1] ENERGY STAR, http://www.energystar.gov/index.cfm?c=products.pr find es products
- [2] Federal Standard: Title 10 Part 431 Energy Efficiency Program for Certain Commercial and Industrial Equipment; Section 431.136
- [3] Federal Standard: Title 10 Part 431 Energy Efficiency Program for Certain Commercial and Industrial Equipment; Section 431.66

Notes

- [1] The AHAM volume is the interior volume of a refrigerator as calculated by AHAM Standard Household Refrigerators/Household Freezers (ANSI/AHAM HRF-1-2004).
- [2] Actual full load hours should be used, when known, in the savings calculator in lieu of the default hours

2.6.3 LOST OPPORTUNITY CUSTOM

Description of Measure

Version Date: 10/30/2012

This measure may apply to any C&I Lost Opportunity installations whose scope may be considered custom or comprehensive and not covered by a prescriptive measure.

Savings Methodology

Energy and demand savings are calculated on a custom basis for each customer's specific situation. Savings are calculated as the difference between baseline energy usage/peak demand and the energy use/peak demand after implementation of the custom measure. Energy savings estimates should be calibrated against billing or metered data where possible to test the reasonableness of energy savings. Also, the energy and demand savings analysis must be reviewed for reasonableness by either a third party consulting engineer or a qualified in-house engineer.

Demand savings methodologies are categorized as follows:

- 1. Temperature-dependent (HVAC measures that vary with ambient temperature)
- 2. Non-temperature-dependent (process, lighting, time control)

Temperature-dependent measures:

Savings from temperature-dependent measures are typically determined by either full load hour analysis, bin temperature analysis, or a detailed computer simulation:

- 1. When annual savings are calculated using a full load hour analysis, an appropriately derived coincidence factor (based on the measure end use and peak time period [Seasonal]) will be used for a measure that has a connected load that can be determined from rated or nameplate data. Demand savings will be determined by multiplying the connected load kW savings by the appropriate coincidence factor.
- 2. When using a temperature bin analysis to calculate the energy savings, the demand (kW) savings are averaged over the appropriate temperature bins (Seasonal).
- 3. When a computer simulation is used to calculate savings, the demand savings will be averaged over the appropriated peak time period (Seasonal).

Non-temperature-dependent measures:

- Demand savings for measures that are not temperature-dependent will be determined by either the coincidence factors from Appendix 1 or the average estimated savings over the appropriate peak time periods (Seasonal). For example, for a process VFD measure, the savings will depend on cycling of the load. This cycling may occur many times during an hour.
- 2. If the process is operating throughout the Seasonal summer period, the average demand savings will be:

$$Average \ Demand \ Savings = \frac{Annual \ kWh \ savings}{Annual \ Equivalent \ Full \ Load \ Hours \ of \ Operation}$$
 Or,
$$AKW = \frac{AKWH}{EFLH}$$

3. If the process is operated only a portion of that time period the demand savings will be pro-rated based on that portion.

Baseline efficiencies are based on code or common practice, whichever is more efficient.

2.6.4 COMMERCIAL CLOTHES WASHERS

Description of Measure

Version Date: 10/30/2012

The installation of an ENERGY STAR Commercial Clothes Washer.

Savings Methodology

Savings for this measure are calculated using the appropriate water heating and dryer fuel source. The basis of the savings is the Consortium for Energy Efficiency (CEE) savings calculator (Ref [1]). The usage per load by fuel source for baseline (Federal Standard) and ENERGY STAR units were calculated based on (Ref [1]). Using the average loads per year the annual savings are calculated. Number of annual loads will either be based on the CEE default calculator default values (Laundromats (2,190 loads per year) or multi-family (1,241 Loads per year)) or project specific information for any facility type. Installed energy use will be based on the installed modified energy factor.

Inputs

| Symbol | Description | Units |
|--------|---|----------------------------|
| N | Number of units | |
| | Water heating fuel source (Electric, natural gas, propane, oil) | |
| | Dryer Fuel Source (none, electric, natural gas, propane) | |
| | Type of facility (Laundromat or Multi-family) | |
| MEFi | Modified Energy Factor - installed | ft ³ /kWh/cycle |
| LDS | Average number of loads per week | loads/wk |
| WK | Average number of weeks per year | wk/yr |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|---------------------|--|----------------------------|--------|-----------------|
| AKWH | Annual electric energy savings | kWh | | |
| $AKWH_{O}$ | Annual electric energy savings - other | kWh | | |
| AKWH _W | Annual electric energy savings – water heating | kWh | | |
| ABTU _O | Annual Btu savings - other | Btu | | |
| $ABTU_W$ | Annual Btu savings – water heating | Btu | | |
| ACCF | Annual natural gas savings - total | Ccf | | |
| ACCF ₀ | Annual natural gas savings - other | Ccf | | |
| ACCF _w | Annual natural gas savings – water heating | Ccf | | |
| APG | Annual propane savings - total | Gallons | | |
| APGo | Annual propane savings - other | Gallons | | |
| APG_W | Annual propane savings – water heating | Gallons | | |
| AOG_W | Annual Oil savings – water heating | Lbs/h | | |
| $DKWH_b$ | Dryer kWh per load - baseline | kWh/ld | 1.107 | Note [1] |
| DKWH _{es} | Dryer kWh per load – ENERGY STAR | kWh/ld | 0.698 | Note [1] |
| $DRBTU_b$ | Dryer Btus - baseline | Btus/ld | 3,771 | Note [1] |
| DRBTU _{es} | Dryer Btus – ENERGY STAR | Btus/ld | 2,376 | Note [1] |
| AGW | Annual water savings | Gallons/year | | |
| Gal _b | Gallons of water - baseline | Gallons | 29.45 | Note [1] |
| Gal _{es} | Gallons of water – ENERGY STAR | Gallons | 18.60 | Note [1] |
| LDS | Average number of Loads per week | Loads/wk | | Input, Note [2] |
| MEFi | Modified energy Factor - installed | ft ³ /kWh/cycle | | Input |
| MEF _{es} | Modified energy factor – ENERGY STAR | ft ³ /kWh/cycle | 2.0 | Note [1] |

| Symbol | Description | Units | Values | Comments |
|---------------------|--------------------------------------|---------|---------|------------|
| N | Number of units | | | Input |
| PD_{W} | Peak day factor – water heating | | 0.00321 | Appendix 1 |
| PD | Peak day savings | Ccf | | |
| WK | Average Weeks per year | Wk/yr | | Input |
| WKWH _b | Washer kWh per load - baseline | kWh/ld | 0.148 | Note [1] |
| WKWH _{es} | Washer kWh per load – ENERGY STAR | kWh/ld | 0.093 | Note [1] |
| WHKWH _b | Hot Water kWh per load - baseline | kWh/ld | 1.206 | Note [1] |
| WHKWH _{es} | Hot Water kWh per load – ENERGY STAR | kWh/ld | 0.760 | Note [1] |
| WHBTU _b | Hot Water BTUs - baseline | Btus/ld | 4,122 | Note [1] |
| WHBTUes | Hot Water BTUs – ENERGY STAR | Btus/ld | 2,597 | Note [1] |

Lost Opportunity Gross Energy Savings, Electric

Version Date : 10/30/2012

Electric savings will be calculated in three pieces. Electric dryer and water heating savings are only if the heat element fuel source is electric.

Annual savings = Washer savings + Water heating savings + Dryer Savings

$$AKWH = AKWH_{O-washer} + AKWH_{O-eletric driver} + AKWH_{W-electric}$$

$$AKWH = N \times LDS \times WK \times \begin{bmatrix} \left(WKWH_b - WKWH_{es} \times \frac{MEF_{es}}{MEF_i}\right) + \left(WHKWH_b - WHKWH_{es} \times \frac{MEF_{es}}{MEF_i}\right) \\ + \left(DKWH_b - DKWH_{es} \times \frac{MEF_{es}}{MEF_i}\right) \end{bmatrix}$$

Lost Opportunity Gross Energy Savings, Fossil Fuel

Fossil fuel savings will be calculated in two pieces. Fossil fuel dryer and water heating savings are only if the heat element fuel source is fossil fuel.

Annual savings = Water heating savings + Dryer Savings

$$ABTU = ABTU_{O-FossilFueldryer} + ABTU_{W-fossilfuel}$$

$$ABTU_{W} = N \times LDS \times WK \times \left(WHBTU_{b} - WHBTU_{es} \times \frac{MEF_{es}}{MEF_{i}}\right)$$

$$ABTU_{O} = N \times LDS \times WK \times \left(DRBTU_{b} - DRBTU_{es} \times \frac{MEF_{es}}{MEF_{i}}\right)$$

Savings by fuel source:

Water Heating

$$ACCF_{W} = \frac{ABTU_{W}}{102,900Btu/ccf}$$

$$AOG_{W} = \frac{ABTU_{W}}{138,690Btu/Gal}$$

$$APG_{W} = \frac{ABTU_{W}}{91,330Btu/Gal}$$

Version Date : 10/30/2012

$$ACCF_O = \frac{ABTU_O}{102,900Btu/ccf}$$

$$APG_O = \frac{ABTU_O}{91,330Btu/Gal}$$

Lost Opportunity Gross Energy Savings, Example

A new Laundromat installs 25 new ENERGY STAR washing machines that have an MEF of 2.2. The Laundromat has natural gas water heat and gas dryers. What are the energy savings?

Electric savings:

$$AKWH = N \times LDS \times WK \times \begin{bmatrix} \left(WKWH_b - WKWH_{es} \times \frac{MEF_{es}}{MEF_i}\right) + \left(WHKWH_b - WHKWH_{es} \times \frac{MEF_{es}}{MEF_i}\right) \\ + \left(DKWH_b - DKWH_{es} \times \frac{MEF_{es}}{MEF_i}\right) \end{bmatrix}$$

Dryer and Water heater electric usage = 0

N = 25

LDS x WK = 2,190 (default loads per year)

 $WKWH_b = 0.148 \text{ kWh/ld}$

 $WKWH_{es} = 0.093 \text{ kWh/ld}$

 $MEF_{es} = 2.0$

 $MEF_i = 2.2$

$$AKWH = 25 \times 2,190 \times \left[\left(0.148 - 0.093 \times \frac{2.0}{2.2} \right) + \left(0 - 0 \right) + \left(0 - 0 \right) \right] = 3,474kWh$$

Natural Gas savings:

$$ABTU \ = ABTU_{O-FossilFueldryer} + ABTU_{W-fossilfuel}$$

$$ABTU_{W} = N \times LDS \times WK \times \left(WHBTU_{b} - WHBTU_{es} \times \frac{MEF_{es}}{MEF_{i}}\right)$$

$$ABTU_W = 25 \times 2,190 \times \left(4,122 - 2,597 \times \frac{2.0}{2.2}\right) = 96,419,727 Btus$$

$$ACCF_W = \frac{ABTU_W}{102.900Btu/ccf} = \frac{96,419,727Btus}{102.900Btu/ccf} = 937Ccfs$$

$$ABTU_O = N \times LDS \times WK \times \left(DRBTU_b - DRBTU_{es} \times \frac{MEF_{es}}{MEF_i}\right)$$

$$ABTU_O = 25 \times 2,190 \times \left(3,771 - 2,376 \times \frac{2.0}{2.2}\right) = 88,202,250 Btus$$

$$ACCF_{O} = \frac{ABTU_{O}}{102,900Btu/ccf} = \frac{88,202,250Btus}{102,900Btu/ccf} = 857Ccfs$$

$$ACCF = ACCF_O + ACCF_{WI} = 937 + 857 = 1,794Ccfs$$

Lost Opportunity Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

Assumed to be zero.

Lost Opportunity Gross Peak Demand Savings, Example

Same example as above:

$$PD = \frac{ACCF_O}{365 days/yr} + PD_W \times ACCF_W = PD = \frac{857}{365 days/yr} + 0.00321 \times 937 = 5.4 Ccfs$$

Lost Opportunity Gross Peak Day Savings, Natural gas

$$PD = \frac{ACCF_O}{365 days/yr} + PD_W \times ACCF_W$$

Lost Opportunity Gross Peak Demand Savings, Example

Same example as above:

$$PD = \frac{ACCF_O}{365 days/yr} + PD_W \times ACCF_W = PD = \frac{857}{365 days/yr} + 0.00321 \times 937 = 5.4 Ccfs$$

Non Energy Benefits

ENERGY STAR washers use less water than the base unit.

Water savings:

$$AGW = N \times LDS \times WK \times \left(GAL_b - GAL_{es} \times \frac{MEF_{es}}{MEF_i}\right)$$

Changes from Last Version

New measure

References

[1] http://www.ceeforum.org/sites/default/files/CEE_CommCW_SpecSavingsCalc_2011.xls

Notes

- [1] Baseline and ENERGY STAR usage values used in energy savings calculation tool on website identified in Ref [1]
- [2] Default loads per year for Laundromats and Multi-family from Ref [1]

Version Date: 10/30/2012 2.7.1 COOL ROOF

2.7 ENVELOPE

2.7.1 COOL ROOF

Description of Measure

Upgrade a roof's reflectance at the time of replacement or new construction.

Savings Methodology

Wood, Byk and Associates (Note [1]) developed a number of typical HVAC system scenarios using the hourly building simulation tool DOE-2. Savings were calculated using a baseline reflectance of 0.3 (Note [2]), a high efficiency roof reflectance of 0.70, and a high efficiency roof emittance of 0.75, as certified and labeled by the Cool Roof Rating Council (CRRC, Note [4]). Simulation results were separated into two categories based on the location of the cooling equipment's condenser. Based on the study results, savings ratios were developed per square foot of "cool" roof over electrically air conditioned space, which can be applied to estimate energy savings. The reflectance and emittance requirements in ASHRAE 90.1-2007 are the same as 90.1-2001. Therefore, this analysis is still valid.

Inputs

| Symbol | Description | Units |
|-----------------|--|-----------------|
| | Location of air conditioning systems (Rooftop vs. other). | |
| | Heating Fuel | |
| A _{ac} | Area of upgraded roof that is over electrically air conditioned spaces | ft ² |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|----------|--|---------------------|-------------|----------|
| A_{ac} | Area of upgraded roof that is over electrically air conditioned spaces | ft ² | | Input |
| $ABTU_H$ | Annual Btu savings – Heating | Btu | | |
| $ACCF_H$ | Annual natural gas savings –Heating | Ccf | 102,900 Btu | |
| $AKWH_C$ | Annual Electric Energy Savings -Cooling | kWh | | |
| AOG_H | Annual oil savings – Heating | Gal | 138,690 Btu | |
| APG_H | Annual propane savings – Heating | Gal | 91,330 Btu | |
| F_{C} | Cooling Factor | kWh/ft ² | 0.29872 or | Note [3] |
| | | | 0.08145 | |
| F_{H} | Heating Factor | BTU/ft ² | -0.0017 | Note [3] |
| SKF | Summer Factor | kW/ft2 | 0.00045 or | Note [3] |
| | | | 0.00019 | |
| SKW | Seasonal Summer Peak Demand Savings | kW | | |
| WKW | Seasonal Winter Peak Demand Savings | kW | | |

Version Date: 10/30/2012 2.7.1 COOL ROOF

Lost Opportunity Gross Energy Savings, Electric

When air conditioning equipment is located on the roof (rooftop units, split systems, air cooled chillers), the savings are calculated as follows:

$$F_{C} = 0.29872$$

$$AKWH_{C} = F_{C} \times A_{ac}$$

$$AKWH_{C} = 0.29872 \times A_{ac}$$

Reminder: This does not include cooling towers that serve water cooled chillers. Water cooled chillers are grouped with cooling equipment that is not located on the roof.

When air conditioning equipment is not located on the roof (split systems, air cooled chillers, water cooled chillers), the savings are calculated as follows:

$$F_{C} = 0.08145$$

$$AKWH_{C} = F_{C} \times A_{ac}$$

$$AKWH_{C} = 0.08145 \times A_{ac}$$

Lost Opportunity Gross Energy Savings, Fossil Fuel

$$\begin{split} F_{H} &= -0.0017 \\ ABTU_{H} &= F_{H} \times A_{ac} \\ ABTU_{H} &= -0.0017 \times A_{ac} \\ ACCF_{H} &= \frac{ABTU_{H}}{102,900Btu/Ccf} \\ AOG_{H} &= \frac{ABTU_{H}}{138,690Btu/Gal} \\ APG_{H} &= \frac{ABTU_{H}}{91,330Btu/Gal} \end{split}$$

Reminder: Increasing the reflectance of a roof causes an increase in heating energy usage (thus the negative factor above) because it will decrease the temperature of the roof which will result in higher heating loads.

Lost Opportunity Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

When air conditioning equipment is located on the roof (rooftop units, split systems, air cooled chillers), the demand savings are as follows:

$$SKF_C = 0.00045$$

$$SKW_C = SKF_C \times A_{ac}$$

$$SKW_C = 0.00045 \times A_{ac}$$

$$WKW_C = 0$$

Reminder: This does not include cooling towers that serve water cooled chillers. Water cooled chillers are grouped with cooling equipment that is not located on the roof.

Version Date: 10/30/2012 2.7.1 COOL ROOF

When air conditioning equipment is not located on the roof (split systems, air cooled chillers, water cooled chillers), the savings are as follows:

$$SKF_{C} = 0.00019$$

$$SKW_{C} = SKF_{C} \times A_{ac}$$

$$SKW_{C} = 0.00019 \times A_{ac}$$

$$WKW_{C} = 0$$

Notes

- [1] Wood, Byk, & Associates, Consulting Engineers, 829 Meadowview Road, Kennett Square, PA 19348
- [2] ASHRAE 90.1-2001, Energy Cost Budget Method.
- [3] Results from the modeling done by Wood, Byk, and Associates.
- [4] Reflectance is defined as the ratio of the light reflected by a surface to the light incident upon it.

C&I RETROFIT

3.1 LIGHTING

3.1.1 STANDARD LIGHTING

Description of Measure

Replacement of inefficient lighting with efficient lighting.

Savings Methodology

The energy and seasonal peak demand savings come from reduced fixture wattage, reduced cooling load, and use of occupancy sensors. The baseline is the wattage and existing operating hours of the fixtures being replaced. Note [1].

The heat emitted by lighting will be reduced by the installation of more efficient lighting and, if sensors are installed, lower hours of use. This will result in increased space heating energy use and decreased cooling energy use.

Inputs

| Symbol | Description | Units |
|--------|-----------------------------------|-------|
| | Existing fixture connected kW | |
| | Replacement Fixture connected kW | |
| | Hours of operation (if available) | |

<u>Nomenclature</u>

| Item | Description | Units | Values | Comments |
|------------------|--|-------|--------|--------------------------------|
| AKWH | Annual Gross Electric Energy savings | kWh | | |
| CF _L | Lighting Coincidence Factor from Appendix 1 | | | Appendix 1 |
| CF _{os} | Occupancy Sensor Coincidence Factor from Appendix 1 | | | Appendix 1 |
| COP | Coefficient of Performance | | 3.5 | |
| F | Fraction of lighting energy that must be removed by the facility's cooling system. | | | |
| G | Estimated lighting energy heat to space based on modeling | | 0.73 | |
| Н | Facility lighting hours of use | Hours | | Site specific or Appendix 5 |
| HVAC | Heating, Ventilation and Air Conditioning | | | |
| kW | Fixture input | kW | | |
| kW | Electric Demand | kW | | |
| N | Number of different fixture types with occupancy sensors | | | |
| n | Fixture number | | | |
| O _n | Quantity of fixtures of type n that have occupancy sensors | | | |
| S_{r} | Energy savings due to lighting retrofit | kWh | | |
| S_{os} | Energy savings from use of occupancy sensors, if applicable | kWh | | |
| S_c | Energy savings from reduced cooling load | kWh | | |
| SKW | Seasonal Summer Peak Summer Demand Savings | kW | | |
| W_n | Input watts for fixture type n | Watts | | |
| WKW | Seasonal Winter Peak Summer Demand Savings | kW | | |

Retrofit Gross Energy Savings, Electric

$$AKWh = S_r + S_{os} + S_c$$

Calculation of savings due to fixture retrofit

$$S_r = (kW_B - kW_A) H$$

kW_B = The total power usage of the lighting fixtures that are being replaced, kW. See note [1].

 kW_A = The total power usage of the new lighting fixtures that are being installed, kW.

Calculation of savings due to occupancy sensors

$$S_{os} = \frac{0.3H}{1000} \sum_{n=1}^{N} O_n W_n$$

Where, 0.3 is the generally accepted average hour reduction due to the use of occupancy sensors (Ref [1]).

Calculation of savings due to the reduced cooling required to remove excess heat produced by the lighting fixtures

$$S_C = \frac{\left(S_r + S_{OS}\right) \times F}{COP}$$

COP = 3.5 (Note [2])

If the HVAC system includes an economizer,

Then F=0.35

Otherwise, use Table 1 below

Table 1: Fraction of lighting energy that must be removed by the facilities' cooling system (See Ref [2])

| Building Area, A, Sq ft | F |
|-------------------------|--|
| < 2,000 | 0.48 |
| 2,000 – 20,000 | $0.48 + \frac{0.195(A - 2,000)}{18,000}$ |
| >20,000 | 0.675 |

Retrofit Gross Energy Savings, Fossil Fuel

Space heating energy consumption will increase due to reduced lighting load (cooler lighting fixtures).

Annual Oil Savings = -0.0007129 MMBtu's per annual kWh saved and Annual gas savings = -0.0003649 MMBtu's per kWh. Reference [3].

Retrofit Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

$$SKW = \left(CF_L \times \left(\sum KW_B - \sum KW_A\right) + CF_{OS} \times \frac{\sum_{n=1}^{N} O_n W_n}{1000}\right) \times \left(1 + \frac{G}{COP}\right)$$

$$WKW = CF_L \times \left(\sum KW_B - \sum KW_A\right) + CF_{os} \times \frac{\sum_{n=1}^{N} O_n W_n}{1000}$$

CF_L and CF_{os} are the lighting/occupancy sensor coincidence factor (summer/winter) taken from Appendix 1.

G = 0.73

COP = 3.5 Note [2]

Non Energy Benefits

O&M savings due to the installation of new equipment.

Changes from Last Version

The factors used to calculate the fossil fuel energy penalty associated with more efficient lights for oil and gas were updated (Ref [4]). Updated the COP (from 2.4 to 3.5) and added the note [1] that adjusts baseline of incandescent bulbs.

References

- [1] D. Maniccia B. Von Neida, and A. Tweed. An analysis of the energy and cost savings potential of occupancy sensors for commercial lighting systems Illuminating Engineering Society of North America 2000 Annual Conference: Proceedings. IESNA: New York, NY. Pp. 433-459. Accessed online at http://www.lrc.rpi.edu/resources/pdf/dorene1.pdf
- [2] The source of the equation for S_c and the derivation of the values for F is from "Calculating Lighting and HVAC Interactions," ASHRAE Journal 11-93 as used by KCPL.
- [3] Massachusetts Technical Reference Manual, 2012 Program Year, page 170

Notes

[1] To account for the Energy Independence and Security Act of 2007 the baseline for existing (installed) General Service bulbs shall be based on high efficiency incandescent bulbs (such as halogen). Therefore, if the existing incandescent bulb is not a halogen, 75% of actual installed wattage is used for the baseline calculation. General Service bulbs are defined as medium base bulbs that are intended for general service applications as specified in the Energy Independence and Security Act of 2007.

Version Date: 10/30/2012 3.1.2 REFRIGERATOR LED

3.1.2 REFRIGERATOR LED

Description of Measure

The replacement of older fluorescent lighting in commercial display refrigerators, coolers and freezers with LED lighting.

Savings Methodology

The savings are based on the wattage reduction achieved by replacing fluorescent lighting with LED lighting. Interactive refrigeration savings are also achieved due to the reduced heat loads associated with lighting power reduction from more efficient lighting.

Inputs

| Symbol | Description | Units |
|--------|--|-------|
| EER | Energy Efficiency Ratio of Refrigeration Units | |
| h | Lighting annual run hours | Hours |
| N | Number of lights | |
| L | Ballast location factor | |
| ΔkW | Reduction in power for each light | kW |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|-------------|--|-------|--------|------------|
| ACOP | Average Coefficient of Performance | | | |
| AKWH | Annual Gross Electric Energy savings | kWh | | |
| CF | Seasonal peak demand coincident factor for refrigeration | | | Appendix 1 |
| COP | Coefficient of Performance | | | |
| EER | Energy Efficiency Ratio | | | |
| AkW | Kilowatts, average demand savings for both summer and winter | kW | | |
| L | Ballast location factor | | | |
| N | Number of lights | | | |
| h | Lighting annual run hours | | | |
| ΔkW | Reduction in power for each light | kW | | |

Retrofit Gross Energy Savings, Electric

$$AKWH = N \times \Delta kW \times h \times \left(1 + \frac{L}{ACOP}\right)$$

ACOP = 2.03 for freezers and 2.69 for coolers (used for interactive effects). Note [1]

L= 1 if ballast is located in refrigerated area, 0 if not in refrigerated area and 0.5 if unknown.

If existing EER's are available then ACOP = Average EER/3.413

Average EER = Full Load EER/0.85

Version Date: 10/30/2012 3.1.2 REFRIGERATOR LED

Retrofit Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

$$AKW = N \times \Delta kW \times \left(1 + \frac{CF \times L}{COP}\right)$$

COP = 1.72 for freezers and 2.29 for coolers (used to calculate interactive affects). Note [1]

L= 1 if ballast is located in refrigerated area, 0 if not in refrigerated area and 0.5 if unknown.

If existing EER's are available then COP = EER/3.413

Coincidence Factors (CF) for refrigeration is assumed to be the same for both winter and summer.

Notes

[1] Refrigeration interactive factors are based on email communication with Nick Gianakas. The EER and COP values are derived from ASHRAE handbook for refrigeration equipment as well as experience from submitted projects.

3.2.1 SPRAY VALVE REPLACEMENT

Description of Measure

Version Date: 10/30/2012

This measure replaces existing standard pre-rinse spray valves used for dish cleaning with new low flow spray valves with an average flow rate of 1.6 gpm or less. This measure is applicable to both grocery and non-grocery applications.

3.2 HVAC & WATER HEATING

Savings Methodology

Savings are based on the results of a spray valve replacement program in California (Ref[1]).

Inputs

| Symbol | Description | Units |
|--------|------------------------|-------|
| | Number of Spray Valves | |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|------------|--|-------|-------------|------------|
| $AKWH_{w}$ | Annual Gross Electric Energy savings – water heating | kWh | 957 or 126 | Ref [1] |
| $ACCF_w$ | Annual natural gas consumption- water heating | Ccf | 40.8 or 5.3 | Ref [1] |
| gpm | Gallons per minute | | | |
| PD_{W} | Peak Day Savings | Ccf | | |
| PDF_{w} | Peak Day Factor – water heating | | 0.00321 | Appendix 1 |

Retrofit Gross Energy Savings, Electric

If hot water is supplied via an electric water heater then energy savings are:

| Facility Type | AKWH _w per Spray Valve |
|---------------|-----------------------------------|
| Grocery | 126 kWh |
| Non-grocery | 957 kWh |

Retrofit Gross Energy Savings, Fossil Fuel

If hot water is supplied via a gas water heater then annual energy savings are:

| Facility Type | ACCF _w per Spray Valve |
|---------------|-----------------------------------|
| Grocery | 5.3 CcF (5.5 Therms) |
| Non-grocery | 40.8 CcF (42 Therms) |

Retrofit Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

Assumed to be zero.

Retrofit Gross Peak Day Savings, Natural Gas

$$PD_W = PDF_W \times ACCF_W = 0.00321 \times ACCF_W$$

| Facility Type | PD _w per Spray Valve |
|---------------|---------------------------------|
| Grocery | 0.0172 CcF |
| Non-grocery | 0.1310 CcF |

Non Energy Benefits

Version Date: 10/30/2012

Water savings are estimated to be:

| Facility Type | Gallons per year |
|---------------|------------------|
| Grocery | 1,496 |
| Non-grocery | 8,603 |

Changes from Last Version

Natural gas peak savings was added. Savings was provided based for two facility types: grocery and non-grocery (the 2012 PSD presented savings used in non-grocery applications only). The conversion from therms to Ccf was adjusted from 42 to 40.8 (non-grocery) and from 5.5 to 5.3 (grocery).

References

[1] Impact and Process Evaluation Final Report for California Urban Water Conservation Council, 2004-5 Pre-Rinse Spray Valve Installation Program (Phase 2), February 21, 2007. Table 3-9 page 26 Version Date: 10/30/2012 3.2.2 PIPE INSULATION

3.2.2 PIPE INSULATION

Description of Measure

Installation of insulation on bare hydronic supply heating pipes located in unconditioned spaces.

Savings Methodology

Savings were determined using 3E Plus v4.0 software (Ref [1]) with 50°F ambient temperature and 180°F fluid temperature. If the difference between the actual average ambient temperature and fluid temperature varies significantly from this difference (130°F), the savings should be scaled using linear interpolation. The hourly heat loss savings per linear foot for various pipe and insulation sizes/material are provided in Table 1 below.

Table1: Hourly Heat Loss Savings per Linear Foot of Pipe Insulation

| | • | Loss Savings per Linear Poor o | Insulation Thickness | Insulation Thickness | Insulation Thickness | Insulation Thickness |
|------------------|-----------------|--------------------------------|-------------------------|-------------------------|-------------------------|-------------------------|
| Pipe Material | Nominal Pipe | Insulation Material | 0.5(in) | 1.0(in) | 1.5 (in) | 2.0 (in) |
| | | | HL | HL | HL | HL |
| | Size (In) | | Savings | Savings | Savings | Savings |
| | | | Btu/hr/ft | Btu/hr/ft | Btu/hr/ft | Btu/hr/ft |
| | 0.5 | Polyethylene foam tube | 40 | 47 | 50 | 52 |
| | 0.75 | Polyethylene foam tube | 50 | 57 | 61 | 63 |
| | 1.0 | Polyethylene foam tube | 62 | 73 | 77 | 79 |
| | 1.25 | Polyethylene foam tube | 76 | 88 | 96 | 98 |
| <u>.</u> | 1.5 | Polyethylene foam tube | 86 | 103 | 109 | 113 |
| Copper | 2.0 | Polyethylene foam tube | 110 | 127 | 135 | 139 |
| do, | 0.5 | Mineral fibers | 46 | 52 | 54 | 55 |
| | 0.75 | Mineral fibers | 57 | 63 | 66 | 68 |
| | 1.0 | Mineral fibers | 71 | 79 | 82 | 84 |
| | 1.25 | Mineral fibers | 86 | 96 | 102 | 103 |
| | 1.5 | Mineral fibers | 97 | 111 | 115 | 119 |
| | 2.0 | Mineral fibers | 123 | 137 | 142 | 145 |
| | 0.5 | Polyethylene foam tube | 47 | 54 | 57 | 59 |
| | 0.75 | Polyethylene foam tube | 59 | 66 | 71 | 73 |
| | 1.0 | Polyethylene foam tube | 74 | 84 | 88 | 91 |
| | 1.25 | Polyethylene foam tube | 91 | 103 | 111 | 113 |
| | 1.5 | Polyethylene foam tube | 103 | 120 | 126 | 130 |
| Steel | 2.0 | Polyethylene foam tube | 132 | 149 | 156 | 160 |
| | 0.5 | Mineral fibers | 54 | 59 | 62 | 63 |
| | 0.75 | Mineral fibers | 67 | 72 | 75 | 77 |
| | 1.0 | Mineral fibers | 82 | 91 | 94 | 96 |
| | 1.25 | Mineral fibers | 101 | 111 | 117 | 118 |
| | 1.5 | Mineral fibers | 114 | 128 | 132 | 136 |
| | 2.0 | Mineral fibers | 144 | 158 | 164 | 167 |

Inputs

| Symbol | Description | Units |
|--------|----------------------------|--------|
| | Nominal Pipe size diameter | Inches |
| | Insulation Material | |
| | Insulation Thickness | Inches |

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| Symbol | Description | Units |
|--------|-----------------------------|-------------|
| L | Length of Insulation | Linear foot |
| | Heating Fuel Type(Oil, Gas) | |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|--------|---|-----------|------------|----------|
| ACCF | Annual Natural Gas Savings | Ccf | | |
| EFLH | Equivalent heating full load hours for the facility type | hours | Appendix 5 | |
| HL | Heat loss savings per linear foot of pipe | Btu/ft/hr | Table 1 | |
| L | Length of pipe being insulated | Linear ft | | |
| AFUE | Annual Fuel Utilization Efficiency, estimated boiler efficiency | unit less | 0.80 | |
| PD | Peak day savings natural gas | Ccf | | |

Retrofit Gross Energy Savings, Fossil Fuel

Annual Gas Heating Savings

$$ACCF = \frac{HL \times EFLH}{(102,900 \times 0.80)} \times L$$

Annual Oil Heating Savings

$$AOG = \frac{HL \times EFLH}{(138,690 \times 0.80)} \times L$$

Retrofit Gross Energy Savings, Example

One inch (1") thick polyolefin C1427-04 insulation was installed on 100 feet un-insulated hot water heating supply pipe (copper). The pipe nominal size is 1 inch and is located in unconditioned space of an office/retail type business. What are the energy savings resulting from adding the insulation?

Based on these data and using table1 above, the corresponding HL heat loss savings is 73 Btu/ft/hr. The length of pipe being insulated L=100 ft. Using Appendix 5, (hours of use), heating EFLH for an office/retail is 1248. Using the savings formula:

$$ACCF = \frac{HL \times EFLH}{(102,900 \times 0.80)} \times L = \frac{73 \times 1248}{(102,900 \times 0.80)} \times 100 = 110.7Ccf$$

Retrofit Gross Peak Day Savings, Natural Gas

$$ACCF = \frac{ACCF}{EFLH} \times 24$$

Changes from Last Version

Savings for additional pipe sizes and insulation thicknesses were added. Gas peak day savings and oil savings were also included.

References

[1] NAIMA, 3EPlus Version4.0 -Pipe and duct insulation software-

Version Date: 10/30/2012 3.2.3 DUCT SEALING

3.2.3 DUCT SEALING

Description of Measure

Seal ducting located in unconditioned spaces. This measure is applicable to buildings that are similar to residential construction or buildings where performing duct blaster/blower door testing is practical.

Savings Methodology

Refer to the duct sealing measure in the residential section of this document (Measure 4.2.9).

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3.2.4 DUCT INSULATION

Description of Measure

Installation of insulation on ducting located in unconditioned spaces in commercial buildings.

Savings Methodology

The savings were determined using 3E Plus v4.0 software (Ref [1]). The savings are based on insulating existing bare ducting with R-6 insulation. Savings presented in table 1 below are for example purposes only and should only be used when the parameters (inputs) match the inputs here (like average air supply/return temperatures are 130deg F/ 65deg F for heating). For all other scenarios, the 3E software or a similar methodology should be used to develop estimates of the appropriate energy savings under actual conditions.

Table 1: Assumed temperature conditions

| Duct Location | Season | Ambient Temp (°F) | Supply Air Temp (°F) | Return Air Temp (°F) |
|----------------------|---------|-------------------|----------------------|----------------------|
| Attic | Heating | 30 | 130 | 65 |
| | Cooling | 120 | 50 | 80 |
| Basement | Heating | 50 | 130 | 65 |
| | Cooling | 70 | 50 | 80 |

Table 2: Heat transfer rates per hour per square foot of insulation

| | BTUH | (Bare) | BTUH _a (Ins | ulated R-6) |
|----------------------|-----------------------------------|-----------------------------------|-----------------------------------|-----------------------------------|
| Duct Location | Heating BTU/hr/ft ² | Cooling BTU/hr/ft ² | Heating BTU/hr/ft ² | Cooling BTU/hr/ft ² |
| Supply Basement | 132.34 | 25.22 | 12.04 | 2.73 |
| Return Basement | 18.12 | - | 2.03 | - |
| Supply Attic | 167.14 | 112.11 | 14.67 | 10.42 |
| Return Attic | 45.86 | 61.93 | 4.63 | 6.18 |

Inputs

| Symbol | Description |
|--------|---|
| A | Insulation area in square feet |
| | Heating Fuel /Heating system type (Elect Heat Pump, Gas Furnace,) |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|--------------------|--|------------------------|-----------------------|----------|
| $AKWH_C$ | Annual gross electric cooling savings | kWh | | |
| $AKWH_H$ | Annual gross electric heating savings | kWh | | |
| BTUH _{ca} | Cooling heat transfer rate of insulated ducting | BTU/hr/ft ² | Table 2 | |
| BTUH _{cb} | Cooling heat transfer rate of un-insulated ducting | BTU/hr/ft ² | Table 2 | |
| $BTUH_{ha}$ | Heating heat transfer rate of insulated ducting | BTU/hr/ft ² | Table 2 | |
| $BTUH_{hb}$ | Heating heat transfer rate of un-insulated ducting | BTU/hr/ft ² | Table 2 | |
| COP_H | Coefficient of Performance of heating equipment | Unitless | 1.0 for Elect furnace | |
| | | | 2.0 for Heat Pump | |
| | | | 3.0 for Ground Source | |
| | | | Heat Pump | |

| Symbol | Description | Units | Values | Comments |
|--------|---|-------|------------|----------|
| EFLH | Equivalent heating or cooling full load hours for the | hours | Appendix 5 | |
| | facility type | | | |
| A | Insulation area in square feet | | | |

Retrofit Gross Energy Savings, Electric

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Annual gross electric heating savings for electrically heated buildings:

$$AKWH_{H} = \frac{(BTUH_{hb} - BTUH_{ha}) \times EFLH \times A}{3412 \times COP_{H}}$$

Annual gross electric cooling savings for building equipped with Central AC or Heat pump:

$$AKWH_{C} = \frac{(BTUH_{cb} - BTUH_{ca}) \times EFLH \times A}{3412 \times 3.5}$$

Where:

3412 = converts BTU to kWh

3.5 = estimated cooling equipment efficiency, COP

Retrofit Gross Energy Savings, Fossil Fuel

Annual gross gas savings Gas heated buildings:

$$ACCF = \frac{(BTUH_{hb} - BTUH_{ha}) \times EFLH \times A}{102,900 \times 0.80}$$

Where:

0.80 = estimated heating equipment efficiency

Retrofit Gross Energy Savings, Example

R-6 Insulation was installed on 100 sqft of bare supply ducting located in the basement of a small retail store. This system is utilizes a heat pump and provides both heating and cooling. What are the savings?

Annual gross electric heating savings:

$$AKWH_{H} = \frac{(BTUH_{hb} - BTUH_{ha}) \times EFLH \times A}{3412 \times 2}$$

From table 2 BTUH_{hb}=132.34

From table 2 BTUH_{ha}=12.04

From Appendix 5 EFLH heating=1248 hr

A = 100 sqft

From Nomenclature table COP_H for Heat pump = 2.0

$$AKWH_{H} = \frac{(132.34 - 12.04) \times 1248 \times 100}{3412 \times 2} = 2200.09kWh$$

Annual gross electric cooling savings:

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$$AKWH_{c} = \frac{(BTUH_{cb} - BTUH_{ca}) \times EFLH \times A}{3412 \times 3.5}$$

From table 2 BTUH_{cb}=25.22 From table 2 BTUH_{ca}=2.73

From Appendix 5 EFLH cooling=797

A = 100 sqft

$$AKWH_{c} = \frac{(25.22 - 2.73) \times 797 \times 100}{3412 \times 3.5} = 150.10kWh$$

Retrofit Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

Currently, no demand savings are claimed for this measure.

Changes from Last Version

The cooling COP was changed from 3.0 to 3.5 to reflect newer, more efficient cooling equipment.

References

[1] NAIMA, 3E plus software tool, version 4.0, released 2005.

3.2.5 SET BACK THERMOSTAT

Description of Measure

Version Date: 10/30/2012

Installation of programmable thermostats in place of non-programmable thermostats in small business applications.

Savings Methodology

Savings estimates below are based on computer simulation models (Ref [1]). Seven models were developed assuming different occupancy schedules. A 10 degree setback for unoccupied periods is assumed for both heating and cooling modes. A relationship between hours of occupancy and savings was developed from these models based on installed capacity (kW-electric heating, Tons-cooling, MBh-gas heat). Savings will only be realized if the facility currently maintains a constant temperature for both occupied and unoccupied periods.

There are no electric demand savings since savings occur during off peak periods. Peak day savings are calculated using a peak day factor (0.0477) calculated for setback thermostats. A temperature bin analysis was used to calculate the reduction for the temperature bins during set back period. The sum load reductions from the coldest 24 hours were divided by the total sum of load reduction for the entire year

Inputs

| Symbol | Description | Units |
|--------|--|---------------|
| CAP | Output capacity of gas heating equipment | MBh |
| Hrs | Occupied Hours per week | Hrs |
| Tons | Installed Cooling Capacity | Tons |
| Nr | Nameplate Rating of baseboard electric resistance heat | kW (Note [2]) |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|--------------|--|---------|--------|----------|
| ACCF | Annual Natural Gas Savings | Ccf | | |
| AKWH | Annual Gross Electric Energy savings | kWh | | |
| CAP | Output capacity of gas heating equipment | MBh | | Input |
| Hrs | Occupied Hours per week | Hours | | Input |
| MBh | Thousands of Btu's per hour | | | |
| Nr | Nameplate Rating of baseboard electric resistance heat | kW | | Input |
| PDF | Peak Day Factor | | 0.0477 | |
| PD | Peak Day Savings | Ccf | | |
| SF_{CCF} | CcF savings factor | Ccf/MBh | | Note [1] |
| $SF_{kWh,H}$ | kWh savings factor – electric heat | kWh/kW | | Note [1] |
| $SF_{kWh,C}$ | kWh savings factor – cooling | kWh/Ton | | Note [1] |
| Tons | Installed cooling capacity | Tons | | Input |

Retrofit Gross Energy Savings, Electric

Heating (Applicable only if the facility has an existing electric resistance heat)

$$SF_{kWh,H} = 239.48 - (1.5569 \times Hrs)$$

$$AKWH_H = Nr \times SF_{kWh,H} = Nr \times (239.48 - 1.5569 \times Hrs)$$

Cooling (Applicable only if the facility has an existing cooling system)

$$SF_{kWh,C} = 167.01 - (1.0929 \times Hrs)$$

$$AKWH_C = Tons \times SF_{kWh,C} = Tons \times [167.01 - (1.0929 \times Hrs)]$$

Retrofit Gross Energy Savings, Fossil Fuel

Heating (Applicable only if the facility has an existing gas heat)

$$SF_{CCF} = 2.79 - (0.0181 \times Hrs)$$

$$ACCF = CAP \times SF_{CCF} = CAP \times [2.79 - (0.0181 \times Hrs)]$$

Retrofit Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

There are no demand savings since savings occurs during off peak periods

Retrofit Gross Peak Day Savings, Natural gas

$$PD = PDF \times ACCF = 0.0477 \times ACCF$$

Changes from Last Version

Savings calculations were updated based on an hourly occupancy schedule versus a daily occupancy schedule. Added Natural Gas Peak Day savings calculation.

References

[1] Trane System Analyzer version 6.1

Notes

- [1] Ref [1] to model a number of different occupancy schedules. These results were used to develop a correlation between occupancy schedule and energy savings. These equations are used to adjust savings for different occupancy schedules.
- [2] If nameplate kW is not available for electric baseboard use 200 watts per foot for baseboards < 3 feet and 250 watts per foot for all others. These values are based on research of typical existing equipment.

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3.2.6 STEAM TRAP REPLACEMENT

Description of Measure

This measure replaces steam traps that are leaking or have failed open in commercial and industrial applications. It is not applicable to orifice type traps.

Savings Methodology

The savings estimates below are based on Table 4.1 in Reference (1), which provides steam loss through orifices at various pressures. The steam flows from Reference (1) are adjusted down based on whether the trap is leaking or failed open. Not all steam energy will be lost to the environment.

Inputs

| Symbol | Description |
|-------------|--|
| lb_m | Steam flow through orifice per Reference (1) |
| EFLH | Equivalent full load hours |
| $L_{\rm f}$ | Steam loss adjustment factor |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|-----------------|------------------------------|---------------------|---------------------------|---------------|
| ACCF | Annual natural gas savings | Ccf | 102,900 Btu | |
| Е | Enthalpy of steam | Btu/lb _m | Varies based on pressure. | |
| Eff | Boiler efficiency | % | 80% | |
| EFLH | Equivalent full load hours | Hours | 8760 for process steam. | |
| | | | 5376 for heating steam. | |
| lb _m | Steam flow through orifice | lb _m /hr | | Reference (1) |
| $L_{\rm f}$ | Steam loss adjustment factor | % | 50% for failed traps. | |
| | | | 12.5% for leaking traps. | |
| PD | Peak day natural gas savings | Ccf | | |

Retrofit Gross Energy Savings, Fossil Fuel

$$ACCF = \frac{lb_m \times E \times EFLH \times L_f}{Eff \times 102,900}$$

Savings based on orifice size are provided in tables below:

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| | Failed Traps - Heating System | | | | | | | | | | | | |
|---------|-------------------------------|-----------------|-------|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | | CCF Savings/Yr | | | | | | | | | | | |
| Orifice | | Pressure (psig) | | | | | | | | | | | |
| Size | 2 | 5 | 10 | 15 | 25 | 50 | 75 | 100 | 125 | 150 | 200 | 250 | 300 |
| 1/32 | 12 | 18 | 27 | 32 | 44 | 72 | 100 | 128 | 157 | 185 | 242 | 299 | 159 |
| 1/16 | 47 | 74 | 106 | 129 | 176 | 285 | 399 | 513 | 627 | 738 | 968 | 1,194 | 1,423 |
| 3/32 | 106 | 168 | 239 | 293 | 393 | 643 | 596 | 1,154 | 1,411 | 1,664 | 2,179 | 2,689 | 3,204 |
| 1/8 | 169 | 298 | 424 | 521 | 699 | 1,148 | 1,599 | 2,052 | 2,506 | 2,961 | 3,879 | 4,790 | 5,700 |
| 5/32 | 294 | 464 | 659 | 810 | 1,089 | 1,791 | 2,497 | 3,206 | 3,897 | 4,609 | 6,034 | 7,460 | 8,884 |
| 3/16 | 422 | 668 | 951 | 1,167 | 1,570 | 2,580 | 3,601 | 4,625 | 5,651 | 6,640 | 8,699 | 10,758 | 12,815 |
| 7/32 | 576 | 913 | 1,296 | 1,593 | 2,135 | 3,513 | 4,878 | 6,296 | 7,678 | 9,062 | 11,872 | 14,645 | 17,415 |
| 1/4 | 753 | 1,193 | 1,690 | 2,079 | 2,792 | 4,583 | 6,388 | 8,200 | 10,016 | 11,835 | 15,477 | 19,120 | 22,761 |
| 9/32 | 949 | 1,506 | 2,145 | 2,630 | 3,533 | 5,816 | 8,092 | 10,377 | 12,667 | 14,999 | 19,592 | 24,224 | 28,815 |
| 5/16 | 1,174 | 1,861 | 2,641 | 3,246 | 4,355 | 7,164 | 9,989 | 12,825 | 15,668 | 18,515 | 24,176 | 29,878 | 35,576 |
| 11/32 | 1,419 | 2,250 | 3,198 | 3,915 | 5,271 | 8,666 | 12,080 | 15,507 | 18,942 | 22,382 | 29,270 | 36,160 | 43,046 |
| 3/8 | 1,690 | 2,680 | 3,789 | 4,675 | 6,265 | 10,322 | 14,364 | 18,461 | 22,527 | 26,639 | 34,834 | 43,031 | 51,222 |
| 13/32 | 1,984 | 3,144 | 4,471 | 5,474 | 7,372 | 12,093 | 16,881 | 21,647 | 26,464 | 31,248 | 40,868 | 50,491 | 60,107 |
| 7/16 | 2,300 | 3,646 | 5,191 | 6,348 | 8,557 | 14,058 | 19,591 | 25,145 | 30,673 | 36,248 | 47,411 | 58,578 | 69,738 |
| 15/32 | 2,643 | 4,190 | 5,949 | 7,298 | 9,817 | 16,137 | 22,456 | 28,837 | 35,233 | 41,600 | 54,425 | 67,255 | 80,077 |
| 1/2 | 3,004 | 4,756 | 6,783 | 8,324 | 11,154 | 18,333 | 25,554 | 32,801 | 40,066 | 47,341 | 61,909 | 76,521 | 91,084 |

| | Leaking Traps - Heating System | | | | | | | | | | | | |
|---------|--------------------------------|-----------------|-------|-------|-------|-------|-------|-------|--------|--------|--------|--------|--------|
| | | CCF Savings/Yr | | | | | | | | | | | |
| Orifice | | Pressure (psig) | | | | | | | | | | | |
| Size | 2 | 5 | 10 | 15 | 25 | 50 | 75 | 100 | 125 | 150 | 200 | 250 | 300 |
| 1/32 | 3 | 5 | 7 | 8 | 11 | 18 | 25 | 32 | 39 | 46 | 60 | 75 | 40 |
| 1/16 | 12 | 19 | 27 | 32 | 44 | 71 | 100 | 128 | 157 | 185 | 242 | 298 | 356 |
| 3/32 | 26 | 42 | 60 | 73 | 98 | 161 | 149 | 289 | 353 | 416 | 545 | 672 | 801 |
| 1/8 | 42 | 75 | 106 | 130 | 175 | 287 | 400 | 513 | 627 | 740 | 970 | 1,197 | 1,425 |
| 5/32 | 73 | 116 | 165 | 202 | 272 | 448 | 624 | 802 | 974 | 1,152 | 1,509 | 1,865 | 2,221 |
| 3/16 | 105 | 167 | 238 | 292 | 392 | 645 | 900 | 1,156 | 1,413 | 1,660 | 2,175 | 2,689 | 3,204 |
| 7/32 | 144 | 228 | 324 | 398 | 534 | 878 | 1,220 | 1,574 | 1,920 | 2,266 | 2,968 | 3,661 | 4,354 |
| 1/4 | 188 | 298 | 422 | 520 | 698 | 1,146 | 1,597 | 2,050 | 2,504 | 2,959 | 3,869 | 4,780 | 5,690 |
| 9/32 | 237 | 377 | 536 | 658 | 883 | 1,454 | 2,023 | 2,594 | 3,167 | 3,750 | 4,898 | 6,056 | 7,204 |
| 5/16 | 294 | 465 | 660 | 812 | 1,089 | 1,791 | 2,497 | 3,206 | 3,917 | 4,629 | 6,044 | 7,470 | 8,894 |
| 11/32 | 355 | 562 | 800 | 979 | 1,318 | 2,166 | 3,020 | 3,877 | 4,735 | 5,595 | 7,317 | 9,040 | 10,761 |
| 3/8 | 423 | 670 | 947 | 1,169 | 1,566 | 2,580 | 3,591 | 4,615 | 5,632 | 6,660 | 8,708 | 10,758 | 12,806 |
| 13/32 | 496 | 786 | 1,118 | 1,368 | 1,843 | 3,023 | 4,220 | 5,412 | 6,616 | 7,812 | 10,217 | 12,623 | 15,027 |
| 7/16 | 575 | 912 | 1,298 | 1,587 | 2,139 | 3,514 | 4,898 | 6,286 | 7,668 | 9,062 | 11,853 | 14,645 | 17,434 |
| 15/32 | 661 | 1,047 | 1,487 | 1,825 | 2,454 | 4,034 | 5,614 | 7,209 | 8,808 | 10,400 | 13,606 | 16,814 | 20,019 |
| 1/2 | 751 | 1,189 | 1,696 | 2,081 | 2,789 | 4,583 | 6,388 | 8,200 | 10,016 | 11,835 | 15,477 | 19,130 | 22,771 |

| | Failed Traps - Process System | | | | | | | | | | | | |
|---------|-------------------------------|-----------------|--------|--------|--------|--------|--------|--------|--------|--------|---------|---------|---------|
| | | CCF Savings/Yr | | | | | | | | | | | |
| Orifice | | Pressure (psig) | | | | | | | | | | | |
| Size | 2 | 5 | 10 | 15 | 25 | 50 | 75 | 100 | 125 | 150 | 200 | 250 | 300 |
| 1/32 | 19 | 30 | 43 | 53 | 71 | 117 | 163 | 209 | 255 | 302 | 394 | 487 | 259 |
| 1/16 | 77 | 121 | 173 | 211 | 286 | 464 | 650 | 836 | 1,022 | 1,203 | 1,577 | 1,945 | 2,319 |
| 3/32 | 172 | 273 | 389 | 477 | 641 | 1,048 | 972 | 1,881 | 2,299 | 2,711 | 3,550 | 4,382 | 5,221 |
| 1/8 | 276 | 486 | 692 | 849 | 1,139 | 1,870 | 2,606 | 3,344 | 4,084 | 4,825 | 6,321 | 7,805 | 9,288 |
| 5/32 | 478 | 757 | 1,074 | 1,319 | 1,774 | 2,918 | 4,069 | 5,225 | 6,351 | 7,510 | 9,832 | 12,155 | 14,477 |
| 3/16 | 687 | 1,089 | 1,550 | 1,901 | 2,558 | 4,205 | 5,867 | 7,536 | 9,209 | 10,820 | 14,174 | 17,529 | 20,882 |
| 7/32 | 938 | 1,488 | 2,112 | 2,595 | 3,479 | 5,723 | 7,949 | 10,259 | 12,511 | 14,766 | 19,346 | 23,863 | 28,377 |
| 1/4 | 1,227 | 1,944 | 2,754 | 3,388 | 4,550 | 7,468 | 10,410 | 13,362 | 16,322 | 19,285 | 25,220 | 31,156 | 37,088 |
| 9/32 | 1,546 | 2,454 | 3,495 | 4,286 | 5,758 | 9,476 | 13,186 | 16,909 | 20,640 | 24,441 | 31,924 | 39,473 | 46,953 |
| 5/16 | 1,914 | 3,032 | 4,304 | 5,289 | 7,096 | 11,673 | 16,277 | 20,898 | 25,530 | 30,169 | 39,394 | 48,685 | 57,971 |
| 11/32 | 2,312 | 3,666 | 5,211 | 6,380 | 8,590 | 14,120 | 19,684 | 25,268 | 30,865 | 36,470 | 47,694 | 58,921 | 70,141 |
| 3/8 | 2,754 | 4,367 | 6,174 | 7,618 | 10,208 | 16,819 | 23,406 | 30,081 | 36,708 | 43,408 | 56,760 | 70,117 | 83,465 |
| 13/32 | 3,233 | 5,124 | 7,286 | 8,919 | 12,013 | 19,706 | 27,507 | 35,274 | 43,122 | 50,918 | 66,593 | 82,273 | 97,941 |
| 7/16 | 3,748 | 5,942 | 8,459 | 10,344 | 13,943 | 22,907 | 31,923 | 40,973 | 49,981 | 59,065 | 77,255 | 95,452 | 113,635 |
| 15/32 | 4,306 | 6,827 | 9,694 | 11,892 | 15,997 | 26,295 | 36,592 | 46,989 | 57,411 | 67,785 | 88,684 | 109,590 | 130,482 |
| 1/2 | 4,895 | 7,750 | 11,052 | 13,564 | 18,175 | 29,873 | 41,639 | 53,449 | 65,286 | 77,141 | 100,879 | 124,688 | 148,418 |

| | Leaking Traps - Process System | | | | | | | | | | | | |
|---------|--------------------------------|-----------------|-------|-------|-------|-------|--------|--------|--------|--------|--------|--------|--------|
| | | CCF Savings/Yr | | | | | | | | | | | |
| Orifice | | Pressure (psig) | | | | | | | | | | | |
| Size | 2 | 5 | 10 | 15 | 25 | 50 | 75 | 100 | 125 | 150 | 200 | 250 | 300 |
| 1/32 | 5 | 8 | 11 | 13 | 18 | 29 | 41 | 52 | 64 | 75 | 98 | 122 | 65 |
| 1/16 | 19 | 30 | 43 | 53 | 72 | 116 | 162 | 209 | 256 | 301 | 394 | 486 | 580 |
| 3/32 | 43 | 68 | 97 | 119 | 160 | 262 | 243 | 470 | 575 | 678 | 887 | 1,096 | 1,305 |
| 1/8 | 69 | 121 | 173 | 212 | 285 | 468 | 651 | 836 | 1,021 | 1,206 | 1,580 | 1,951 | 2,322 |
| 5/32 | 120 | 189 | 269 | 330 | 443 | 730 | 1,017 | 1,306 | 1,588 | 1,878 | 2,458 | 3,039 | 3,619 |
| 3/16 | 172 | 272 | 387 | 475 | 640 | 1,051 | 1,467 | 1,884 | 2,302 | 2,705 | 3,544 | 4,382 | 5,221 |
| 7/32 | 235 | 372 | 528 | 649 | 870 | 1,431 | 1,987 | 2,565 | 3,128 | 3,692 | 4,836 | 5,966 | 7,094 |
| 1/4 | 307 | 486 | 688 | 847 | 1,138 | 1,867 | 2,602 | 3,341 | 4,080 | 4,821 | 6,305 | 7,789 | 9,272 |
| 9/32 | 386 | 614 | 874 | 1,072 | 1,439 | 2,369 | 3,296 | 4,227 | 5,160 | 6,110 | 7,981 | 9,868 | 11,738 |
| 5/16 | 478 | 758 | 1,076 | 1,322 | 1,774 | 2,918 | 4,069 | 5,225 | 6,383 | 7,542 | 9,848 | 12,171 | 14,493 |
| 11/32 | 578 | 916 | 1,303 | 1,595 | 2,147 | 3,530 | 4,921 | 6,317 | 7,716 | 9,118 | 11,923 | 14,730 | 17,535 |
| 3/8 | 689 | 1,092 | 1,544 | 1,905 | 2,552 | 4,205 | 5,852 | 7,520 | 9,177 | 10,852 | 14,190 | 17,529 | 20,866 |
| 13/32 | 808 | 1,281 | 1,821 | 2,230 | 3,003 | 4,926 | 6,877 | 8,818 | 10,780 | 12,730 | 16,648 | 20,568 | 24,485 |
| 7/16 | 937 | 1,485 | 2,115 | 2,586 | 3,486 | 5,727 | 7,981 | 10,243 | 12,495 | 14,766 | 19,314 | 23,863 | 28,409 |
| 15/32 | 1,076 | 1,707 | 2,423 | 2,973 | 3,999 | 6,574 | 9,148 | 11,747 | 14,353 | 16,946 | 22,171 | 27,398 | 32,620 |
| 1/2 | 1,224 | 1,937 | 2,763 | 3,391 | 4,544 | 7,468 | 10,410 | 13,362 | 16,322 | 19,285 | 25,220 | 31,172 | 37,104 |

Retrofit Gross Peak Day Savings, Natural Gas

PD=ACCF/EFLH

Version Date: 10/30/2012

Where

EFLH = 8,760 for process steam EFLH = 5,376 for heating steam

Changes from Last Version

New measure

References

[1] Steam Efficiency Improvement, Boiler efficiency Institute, 1987

Version Date: 10/30/2012 3.3.1 CUSTOM MEASURE

3.3 OTHER

3.3.1 CUSTOM MEASURE

Description of Measure

This measure may apply to any C&I Retrofit installations whose scope may be considered custom or comprehensive and not covered by a another specific measure.

Savings Methodology

Energy and demand savings are calculated on a custom basis for each customer's specific situation. Savings are calculated as the difference in energy usage between the baseline energy use and energy use after implementation of the custom measure. Energy savings estimates should be calibrated against billing or metered data where possible to test the reasonableness of energy savings. Also, the energy and demand savings analysis must be reviewed for reasonableness by either a third party consulting engineer or a qualified in-house engineer. Demand savings methodologies are categorized as follows:

- 1. Temperature-dependent (HVAC measures that vary with ambient temperature)
- 2. Non-temperature-dependent (process, lighting, time control)

Temperature-dependent measures:

Energy and demand savings from temperature-dependent measures are typically determined by either full load hour analysis, bin temperature analysis, or a detailed computer simulation:

- 1. When annual savings are calculated using a full load hour analysis, an appropriately derived coincidence factor (based on the measure end use and peak time period [Seasonal]) will be used for a measure that has a connected load that can be determined from rated or nameplate data. Demand savings will be determined by multiplying the connected load kW savings by the appropriate coincidence factor.
- 2. When using a temperature bin analysis to calculate the energy savings, the demand (kW) savings are averaged over the appropriate temperature bins (Seasonal).
- 3. When a computer simulation is used to calculate savings, the demand savings will be averaged over the appropriated peak time period (Seasonal).

Non-temperature-dependent measures:

- Demand savings for measures that are not temperature-dependent will be determined by either the coincidence factors from Appendix 1 or the average estimated savings over the appropriate peak time periods (Seasonal). For example, for a process VFD measure, the savings will depend on cycling of the load. This cycling may occur many times during an hour.
- 2. If the process is operating throughout the Seasonal summer period, the average demand savings will be:

$$Average\ Demand\ Savings = \frac{Annual\ kWh\ savings}{Annual\ equivalent\ full\ load\ hours\ of\ operation}$$

Or,
$$AKW = \frac{AKWH}{EFLH}$$

3. If the process is operated only a portion of that time period the demand savings will be pro-rated based on that portion.

Version Date: 10/30/2012 3.3.1 CUSTOM MEASURE

There are no set baseline and compliance efficiencies. The energy savings are calculated as the difference between what is observed before this measure is installed and what is observed after this measure is installed. The final energy and demand savings analysis must be reviewed for reasonableness by either a third party consulting engineer or a qualified inhouse engineer.

3.4 REFRIGERATION

3.4.1 COOLER NIGHT COVERS

Description of Measure

Version Date: 10/30/2012

Installation of retractable covers for open-type multi-deck refrigerated display cases. The covers are deployed during the unoccupied times in order to reduce the energy loss.

Savings Methodology

The savings values below are based on a test conducted by Southern California Edison (SCE) at its state-of-the-art Refrigeration Technology and Test Center (RTTC) in Irwindale, CA (Ref [1]). The RTTC's sophisticated instrumentation and data acquisition system provided detailed tracking of the refrigeration system's critical temperature and pressure points during the test period. These readings were then utilized to quantify various heat transfer and power related parameters within the refrigeration cycle. The results of SCE's test focused on three typical scenarios found mostly in supermarkets.

There are no demand savings for this measure (covers will not be in use during the peak period).

Inputs

| Symbol | Description |
|--------|--|
| h | Hours per year the cover are in use |
| W | Width of the opening that the covers protect, ft |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|--------|---|--------------|--------|----------|
| AKWH | Annual gross electric energy savings | kWh per year | | |
| h | Hours per year the cover are in use | Hours/yr | | |
| SF | Savings factor based on the temperature of the case | kW/ft | | |
| W | Width of the opening that the covers protect | ft | | |

Retrofit Gross Energy Savings, Electric

 $AKWH = W \times h \times SF$

Table 1: Savings Factor based on case temperature (Ref [1])

| Case Temperature | SF (kW/ft) |
|--------------------------------|------------|
| Low temperature (-35F to -5F) | 0.03 |
| Medium temperature (0F to 30F) | 0.02 |
| High temperature (35F to 55F) | 0.01 |

Retrofit Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

There are no demand savings for this measure because the covers will not be in use during the peak period

<u>References</u>

Version Date: 10/30/2012

[1] "Effects of the Low Emissivity Shields on Performance and Power Use of a Refrigerated Display Case" Southern California Edison Refrigeration Technology and Test Center Energy Efficiency Division August 8, 1997.

3.4.2 EVAPORATOR FAN CONTROLS

Description of Measure

Version Date: 10/30/2012

Installation of evaporator fan controls to walk-in coolers and freezers using evaporator fans that run constantly. The evaporator fan control system either shuts off or reduces the speed of the evaporator fans when the cooler's thermostat is not calling for cooling.

Savings Methodology

The savings from this measure are derived from a reduction in fan speed or the number of hours that the evaporator fans are running. If fan motors are also replaced with ECM motors in conjunction with this measure then savings are based on the reduced fan motor wattage. Interactive refrigeration savings are also achieved due to reduced fan speed or run-hours. The off hours, power reduction factors and power factor are stipulated values based on vendor experience. Fans with two speed controllers are assumed to operate at approximately 52% speed when on the low speed setting. This assumption is based on data provided by one of the controller manufacturers.

Inputs

| Symbol | Description |
|--------|--|
| A | Amperage |
| EER | Energy Efficiency Ratio of Refrigeration Units |
| N | Number of fans |
| V | Volts |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|--------|--|-------|-----------|------------|
| A | Amperage of existing fans | | | |
| ACOP | Average Coefficient of Performance | | | |
| AKWH | Annual Gross Electric Energy savings | kWh | | |
| CF | Seasonal peak demand coincident factor for refrigeration | | | Appendix 1 |
| COP | Coefficient of Performance | | | |
| DP | Power reduction factor | % | | |
| ECM | Electronically Commutated Motor | | | |
| EER | Energy Efficiency Ratio | | | |
| AkW | Average hourly demand savings for both summer and winter | kW | | |
| N | Number of fans | | | |
| Pf | Power factor of existing fans | | | |
| PSC | Permanent Split Capacitor motor | | | |
| R | Adjustment factor for two speed controllers | | 1 or 0.86 | |
| V | Volts of existing fans | | | |
| h | Fan off hours after measure installation | | | |

Retrofit Gross Energy Savings, Electric

If the fan motors are single-phase then calculate the energy savings as follows:

Version Date : 10/30/2012

$$AKWH = N \times V \times A \times Pf \times r \times (1 - DP) \times \frac{h}{1000 \frac{W_{kW}}{W}} \times \left(1 + \frac{1}{ACOP}\right)$$

If the fan motors are three-phase then calculate the energy savings as follows:

$$AKWH = N \times V \times A \times \sqrt{3} \times Pf \times r \times (1 - DP) \times \frac{h}{1000 \%_{kW}} \times \left(1 + \frac{1}{ACOP}\right)$$

If existing fan motors are being replaced concurrently with this measure then DP = 0.40 for PSC motors and 0.65 for shaded pole motors. If fan motors are not being replaced or if the volt/amp readings were taken after fans were replaced, then DP = 0. See Note [1].

Pf = estimated to be 0.65.

h = 3,000. See Note [2].

r= 1 for on/off controllers and 0.86 for two speed controllers.

ACOP = 2.03 for freezers and 2.69 for coolers (used for interactive affects). See Note [3].

If existing EER's are available then ACOP = Average EER/3.413

Average EER = Full Load EER/0.85

Retrofit Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

If the fan motors are single-phase then calculate the demand savings as follows:

$$AKW = CF \times N \times V \times A \times Pf \times r \times \frac{(1 - DP)}{1000 \%_{kW}} \times \left(1 + \frac{1}{COP}\right)$$

If the fan motors are three-phase then calculate demand savings as follows:

$$AKW = CF \times N \times V \times A \times \sqrt{3} \times Pf \times \frac{(1 - DP)}{1000 \%_{bW}} \times \left(1 + \frac{1}{COP}\right)$$

$$AKW = CF \times N \times V \times A \times \sqrt{3} \times Pf \times r \times \frac{\left(1 - DP\right)}{1000 \frac{w}{kW}} \times \left(1 + \frac{1}{COP}\right)$$

If existing fan motors are being replaced concurrently with this measure then DP = 0.40 for PSC motors and 0.65 for shaded pole motors. If fan motors are not being replaced or if the volt/amp readings were taken after fans were replaced, then DP = 0. See Note [1].

Pf = estimated to be 0.65

r= 1 for on/off controllers and 0.86 for two speed controllers.

COP = 1.72 for freezers and 2.29 for coolers (used to calculate interactive affects).

If existing EER's are available then COP = EER/3.413

CF for refrigeration is the same for both winter and summer.

Changes from Last Version

Added savings for two-speed controllers.

References

[1] 2010 ASHRAE Handbook - Refrigeration. Retail Food Store Refrigeration and Equipment, Chapter 15, Figure 24.

Notes

- [1] Power reduction factors of existing fans are based on email communications with NRM representative, March 3 and June 6 of 2011. If motors are being replaced concurrently with this measure then savings calculation for this measure should be coordinated with 3.4.3 to ensure the ending point of one measure (fan power/hours) is the starting point for the other.
- [2] Fan off hours after measure installation (h) is based on email communication with Nick Gianakos, June 27, 2010.
- [3] Refrigeration interactive factors are derived from Reference [1] and email communication with Nick Gianakos, June 27, 2010.

3.4.3 EVAPORATOR FANS MOTOR REPLACEMENT

Description of Measure

Version Date: 10/30/2012

Installation of an electronically commutated motor in place of existing integral electric motor connected to evaporator fans in walk-in coolers, freezers and reach-in display cases.

Savings Methodology

The savings estimates are based on the wattage reduction from replacing an existing PSC or shaded pole motor with an electronically commutated motor. Interactive refrigeration savings are also achieved due to reduced heat loads resulting from fan power reduction. The run hours, power reduction factors and power factor are stipulated values based on vendor experience.

Inputs

| Symbol | Description |
|--------|--|
| A | Amperage |
| EER | Energy Efficiency Ratio of Refrigeration Units |
| N | Number of fans |
| V | Volts |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|--------|--------------------------------------|-------|------------------------------------|----------------|
| A | Amperage of existing fans | | | |
| ACOP | Average Coefficient of Performance | | Estimate from existing EER when | Notes [4], [3] |
| | (used for interactive affects) | | available per Note [4], otherwise: | |
| | | | Freezers: 2.03 | |
| | | | Coolers: 2.69 | |
| AKWH | Annual Gross Electric Energy savings | kWh | | |
| CF | Seasonal peak demand coincident | | | Appendix 1 |
| | factor for refrigeration (Same for | | | |
| | Summer and Winter) | | | |
| COP | Coefficient of Performance (used to | | Freezers: 1.72 | |
| | calculate interactive affects) | | Coolers: 2.29 | |
| DP | Power reduction factor | | PSC motors: 0.40 | Note [1] |
| | | | Shaded pole motors:0.65 | |
| EER | Energy Efficiency Ratio | | | |
| h | Hours of operation | hours | With existing controls: 5,500 | Note [2] |
| | | | Without controls: 8,500 | |
| N | Number of fans | | | |
| Pf | Power factor of existing fans | | 0.65 | Estimated |
| PSC | Permanent Split Capacitor motor | | | |
| V | Volts of existing fans | | | |

Retrofit Gross Energy Savings, Electric

Version Date : 10/30/2012

If the existing fan motors are single-phase then calculate the energy savings as follows:

$$AKWH = N \times V \times A \times Pf \times DP \times \frac{h}{1000} \times \left(1 + \frac{1}{ACOP}\right)$$

If the existing fan motors are three-phase then calculate the energy savings as follows:

$$AKWH = N \times V \times A \times \sqrt{3} \times Pf \times DP \times \frac{h}{1000\%_{hW}} \times \left(1 + \frac{1}{ACOP}\right)$$

Retrofit Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

If the existing fan motors are single-phase then calculate demand savings as follows:

$$AKW = N \times V \times A \times Pf \times \frac{DP}{1000 \%_{kW}} \times \left(\frac{h}{8760 \frac{hrs}{yr}} + \frac{CF \times 1}{COP}\right)$$

If the existing fan motors are three-phase then calculate demand savings as follows:

$$AKW = N \times V \times A \times \sqrt{3} \times Pf \times \frac{DP}{1000 \%_{kW}} \times \left(\frac{h}{8760 \frac{hrs}{yr}} + \frac{CF \times 1}{COP}\right)$$

References

 2010 ASHRAE Handbook - Refrigeration. Retail Food Store Refrigeration and Equipment, Chapter 15, Figure 24

Notes

- [1] Power reduction factors of existing fans are based on email communications with NRM representative on March 3 and June 6 of 2011.
- [2] Fan off hours after measure installation (h) is based on email communication with a C&LM consulting engineer (Nick Gianakos), June 27, 2010. If fan controls are being installed concurrently with this measure then savings calculation for this measure should be coordinated with 3.4.2 to ensure the ending point of one measure (fan power/hours) is the starting point for the other.
- [3] Refrigeration interactive factors are derived from Reference [1] and email communication with Nick Gianakos, June 27, 2010.
- [4] If existing EER's are available then ACOP = Average EER/3.413 Average EER = Full Load EER/0.85

3.4.4 DOOR HEATER CONTROLS

Description of Measure

Version Date: 10/30/2012

Installation of a control system to an existing facility where door heaters operate continuously. This measure is applicable to walk-in coolers and freezers that have electric heaters on the doors whose purpose is to prevent condensation from forming. The control system shuts off the door heaters when the facility's humidity is too low to allow condensation to occur.

Savings Methodology

The savings from this measure result from a reduction in the operating hours of the door heaters. The off hours are stipulated values and are overall averages based on vendor experience (See Note [1]). They are applicable to all store types and sizes.

Inputs

| Symbol | Description |
|--------|-------------------------|
| A | Amperage |
| N | Number of Door heaters |
| V | Volts |
| | Type: Cooler or Freezer |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|--------|--|-------|-----------------|----------|
| A | Amperage of door heater | | | |
| AKW | Annual summer and winter electric demand savings | kW | | |
| AKWH | Annual Gross Electric Energy savings | kWh | | |
| CF | Seasonal peak demand coincident factor for | | Appendix 1 | |
| | refrigeration (Same for Summer and Winter) | | | |
| h | heater off hours after measure installation | hours | Coolers: 6,500 | Note [1] |
| | | | Freezers: 4,070 | |
| kW | KiloWatts | | | |
| N | Number of heaters | | | |
| Pf | Power Factor | | 1 | Note [2] |
| V | Volts of door heater | | | |

Retrofit Gross Energy Savings, Electric

$$AKWH = \frac{N \times V \times A \times Pf \times h}{1000 \frac{w}{kW}}$$

Retrofit Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

$$AKW = \frac{CF \times N \times V \times A \times Pf}{1000 \%_{kW}}$$

Notes

[1] Heater off hours after measure installation for freezers and refrigerators are based on email communications with Nexus Market Research (NMR) representative, June 8, 2011. For the purposes of electric demand savings calculations, CF for refrigeration is assumed to be the same for both winter and summer.

[2] Assumes single phase power.

3.4.5 VENDING MACHINE CONTROLS

Description of Measure

Version Date: 10/30/2012

Installation of on/off control for vending machines that both illuminate and refrigerate products. The controller can be part of a central system or a local programmable control of the individual appliance.

Savings Methodology

Savings from this measure are due to reduced hours of operation of the vending machine. The off hours are multiplied by 45% to account for compressor cycling. See Note [1]. The stipulated adjustment factor and power factor values are based on vendor experience.

Reminder: There are no demand savings for this measure.

Inputs

| Symbol | Description |
|------------------|---|
| A | Amperage of power serving vending machine |
| h_A | Hours vending machine turned on after measure installation |
| h_{B} | Hours vending machine turned on before measure installation |
| N | Number of vending machines |
| V | Volts of power serving vending machine |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|------------------|---|-------|---------------|----------|
| A | Amperage of power serving vending machine | amps | | |
| AKWH | Annual Gross Electric Energy Savings | kWh | | |
| h_A | Hours vending machine turned on after measure installation | | | |
| h_{B} | Hours vending machine turned on before measure installation | | Usually 8,760 | |
| N | Number of vending machines | | | |
| Pf | Power factor | | 0.85 | |
| V | Volts of power serving vending machine | | | |

Retrofit Gross Energy Savings, Electric

$$AKWH = \frac{N \times V \times A \times Pf \times (h_B - h_A) \times 0.45}{1000 \frac{w}{kW}}$$

Note: The above formula assumes single phase power

Changes from Last Version

Added Note 1.

Notes

[1] The 45% factor to account for compressor cycling is based on NRM field experience and email communication with Nick Gianakos, June 27, 2010.

RESIDENTIAL

4.1 LIGHTING

4.1.1 LIGHT BULB

Description of Measure

Lighting savings defined in this section are for the replacement of low efficiency screw-based light bulbs with high efficiency screw-based bulbs of equivalent lumen output. This also includes luminaires with screw-based connections. Examples of efficient lighting technologies may include Solid State Lighting (SSL), Light Emitting Diode (LED), Induction Lamps, and Compact Fluorescent Lamps (CFL).

Savings Methodology

The following assumptions are made to calculate savings for bulbs:

- Measure lives vary according to the type of bulb and its rated lifetime hours (found in Appendix 1)
- The baseline for all bulbs is a screw-base incandescent bulb

Direct install bulbs are different than "retail bulbs" because their installation is performed or verified (in the situation that the builder installs the bulbs) by a professional home energy assessor. Actual rated bulb wattage and location of both the existing and replacement bulbs should be used to calculate savings for direct install bulbs.

General Service bulbs are defined as medium base bulbs that are intended for General Service applications as specified in the Energy Independence and Security Act of 2007 (EISA 2007, Ref [4]). Non-General Service bulbs include, but are not limited to, reflector bulbs, 3-way bulbs, globe bulbs, and candelabra based bulbs. (See Compact Fluorescent Lamp in Glossary, Section 1.6). LED down light savings are separate from other Non-General Service LEDs as the directionality of a down light gives the LED technology an efficiency advantage over non-directional technologies.

Certain General Service bulbs are required to comply with EISA standards according to Table 5 (Note [9]). The baseline for these bulbs at the reduced savings level is based on high-efficiency incandescent bulbs (such as halogen) having 75% of the wattage of the previous (non-EISA compliant) bulb (Ref [4]). This baseline change is being phased in throughout the 2012-2015 program years and will impact the Watt ratio component of the savings calculation (see Note [7]). Watt ratios given in Tables 2, 2A, and 3 reflect the equivalent value of savings taken over the lifetime of the bulb. Please refer to Note [9] for further details.

Inputs

| Symbol | Description | Units |
|----------------------|---|-------|
| Watt _{post} | Rated wattage of installed or purchased high efficiency bulb. | Watts |
| Watt _{pre} | Rated wattage of low efficiency bulb being replaced by direct install. If this input is not collected | Watts |
| | then an assumed Watt _{ratio} is used instead. | |
| Location | Location of direct install bulb. See Table 1 for available options. | |
| Bulb Type | Technology of new bulb. Used primarily to determine measure life. | |
| Rated Life | Rated lifetime of the bulb in hours. This value is not the same as the measure life, but is used to | Hours |
| | determine the measure life for Non-General Service bulbs. | |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|--------|--------------------------------|--------|--------|------------|
| AKWH | Annual Electric Energy Savings | kWh/yr | | Calculated |

| Symbol | Description | Units | Values | Comments |
|-----------------------|---|------------------|--|---|
| CF_S | Average summer seasonal peak coincidence factor for Residential (Lighting) | unit-less | | Appendix 1, Ref [3] |
| CF_{w} | Average winter seasonal peak coincidence factor for Residential (Lighting) | unit-less | | Appendix 1, Ref [3] |
| h _d | Daily hours of use, by room type for direct install. For Lost Opportunity or Retail, use "Unknown" as the room type. | Hours per day | Table 1 for all known locations Retail: 2.77 | Ref [2], Ref [1] |
| LI | Corresponding to the Low Income sector | | | |
| Lifetime | The measure life of the bulb | Years | Lifetime | The measure life of the bulb |
| LKWH | Lifetime Electric Energy Savings | kWh | | Calculated |
| Lumens | Lumen output of installed or purchased light bulb. This input is optional. | | 310-2600 | Lumen output of installed or purchased light bulb. |
| NLI | Corresponding to all Non-Low Income sector | | | |
| RP | Corresponding to the Retail Products sector | | | |
| SKW | Summer Demand Savings | kW | | Calculated |
| $Watt_{\Delta}$ | Delta Watts, the difference between the wattage of the lower efficiency baseline bulb and the wattage of the new bulb. | Watts (W) | | Calculated |
| Watt _{post} | Rated wattage of high efficiency bulb. | Watts (W) | Input | |
| Watt _{pre} | Rated wattage of existing low efficiency bulb. | Watts (W) | Optional Input | Direct install only |
| Watt _{ratio} | Wattage ratio between low efficiency bulb and high efficiency bulb. Defined as Watt _{post} /Watt _{pre} , or if Watt _{pre} unknown, an assumed value. | unit-less | Tables 2, 2A,3 | Tables 2, 2A for Retrofit, Table 3 for Retail |
| WKW | Winter Demand Savings | kW | | Calculated |

Retrofit Gross Energy Savings, Electric

$$Watt_{\Delta} = (Watt_{ratio} - 1) \times Watt_{post}$$

$$AKWH = \frac{Watt_{\Delta} \times h_d \times 365^{\frac{days}{yr}}}{1000^{\frac{W}{kW}}}$$

$$LKWH = AKWH \times Lifetime$$

Please refer to Table 1 for the correct hours of use per day by location (h_{d}) :

Table 1: Hours of Use per Day by Location (h_d)

| Location | Non-Low Income | Low Income |
|-------------|--|---------------------------------------|
| Location | $\mathbf{h}_{\mathbf{d},\mathrm{NLI}}$ | $\mathbf{h}_{\mathbf{d},\mathrm{LI}}$ |
| Bedroom | 1.08* | 1.60*** |
| Bathroom | 0.65* | 1.60*** |
| Den/Office | 2.97** | 2.97** |
| Garage | 1.32* | 1.32* |
| Hallway | 6.25* | 1.74*** |
| Kitchen | 2.97** | 3.66*** |
| Living Room | 2.97** | 3.20*** |
| Dining Room | 2.97** | 2.97** |
| Exterior | 2.89* | 2.89* |
| Basement | 1.29* | 1.45*** |
| Closet | 1.24* | 1.24* |
| Other | 2.05** | 2.05** |
| Unknown † | 2.77** | 2.77** |

^{*} Ref [5]

Please refer to Table 2 for the appropriate Watt_{ratio} to be used in calculations.

Table 2: Retrofit and Direct Install Watt_{ratio} Values

| Existing | 1 | New High Efficiency | Bulb | † 2013 Watt _{ratio} (EISA Compliant) | | |
|------------------------------------|------------------------|---------------------------|---|--|----------|--|
| Bulb | Install Type | Bulb Type | Bulb | All Bulbs Watt _{ratio} | | |
| Incandescent, | General Service | Both Non-Low | CFL/LED/ | For CFLs, see Table 2A For LEDs, see Table 2B | Note [1] | |
| Known wattage | Non-General Service | Income and Low- Income | Induction | $\frac{\textit{Watt}_{\textit{pre}}}{\textit{Watt}_{\textit{post}}}$ | Note [5] | |
| | General | Non-Low Income | CFL/LED/ | For CFLs, see Table 2A | Ref [2] | |
| | Service | Low Income | Induction | For LEDs, see Table 2B | Ref [1] | |
| 4.3.8, Incandescent, Unknown | Non Consul | Non-Low Income | CFL/Non- Directional LED/ Induction | 4.00 | Ref [2] | |
| wattage | Non-General Service | | Directional/ Downlight LED | 5.00 | | |
| | | Low Income | CFL/LED/ Induction | 3.40 | Ref [1] | |

[†] For High Efficiency bulb types not listed use the Wattratio values for CFL bulbs

Table 2A presents the Watt ratios to be used for bulbs impacted by EISA standards. Please note that Lumen ranges are provided for reference.

^{**} Ref [2]

^{***} Ref [1]

[†] Note [2]

Table 2A: Watt_{ratio} Values for CFL General Service Bulbs, Existing Incandescent Wattage

| New Hig | gh Efficiency Bulb | 2013 Watt _{ratio} | | |
|-------------------------|-----------------------------------|--|--|-----------------------------|
| Lumenpost | CFL Bulbs: | Known Wattage: | Unknown Wattage: | Notes |
| Range | Approximate Equivalent Wattage | CFL Bulbs Watt _{ratio} | | |
| Above 2600 or below 310 | Above 30W or below 9W | $\frac{\textit{Watt}_{\textit{pre}}}{\textit{Watt}_{\textit{post}}}$ | Non-Low Income: 4.0 Low Income: 3.4 | Ref [1,2] |
| 1490-2600 | 23W-30W | $\frac{0.75 \times Watt_{pre}}{Watt_{post}}$ | Non-Low Income: 3.0 Low Income: 2.55 | Ref [1,2], Notes [1,9] |
| 1050-1489 | 18W- <23W | $\frac{0.8125 \times Watt_{pre}}{Watt_{post}}$ | Non-Low Income: 3.25 Low Income: 2.7625 | Ref [1,2], Notes [1,9] |
| 310-1049 | 9W-<18W | $\frac{0.875 \times Watt_{pre}}{Watt_{post}}$ | Non-Low Income: 3.5 Low-Income: 2.975 | Ref [1,2], Notes [1,6,9] |

Table 2B: Wattratio Values for LED General Service Bulbs, Existing Incandescent Wattage

| New Hig | New High Efficiency Bulb | | 2013 Watt _{ratio} (EISA Compliant) | | |
|-------------------------|-----------------------------------|--|---|---------------|--|
| Lumenpost | LED Bulbs: | Known Wattage: | Unknown Wattage: | Notes | |
| Range | Approximate Equivalent Wattage | LED Bu | ulbs Watt _{ratio} | | |
| Above 2600 or below 310 | Above 30W or below 6W | $\frac{\textit{Watt}_{\textit{pre}}}{\textit{Watt}_{\textit{post}}}$ | 4.0 | | |
| 1490-2600 | 23W to 30W | $\frac{0.75 \times Watt_{pre}}{Watt_{post}}$ | 3.0 | Notes [1,9] | |
| 1050-1489 | 13W - <23W | $\frac{0.775 \times Watt_{pre}}{Watt_{post}}$ | 3.1 | Notes [1,9] | |
| 310-1049 | 6W - <13W | $\frac{0.80 \times Watt_{pre}}{Watt_{post}}$ | 3.2 | Notes [1,6,9] | |

Retrofit Gross Energy Savings, Example

Example 1. A 60-Watt General Service incandescent bulb is replaced with a 15-Watt General Service CFL bulb in the living room of a Non-Low Income home by direct install in 2013. What are the annual savings?

Using the equations from above:

$$Watt_{\Delta} = (Watt_{ratio} - 1) \times Watt_{post}$$

$$AKWH = \frac{Watt_{\Delta} \times h_d \times 365^{days/yr}}{1000^{W/yw}}$$

This bulb is affected by the EISA standards. From Table 1 we obtain h_d for the Non-Low Income location given. Tables 2 and 2A provide the appropriate Watt_{ratio}. Since Watt_{pre} is known we can calculate directly:

$$Watt_{\Delta} = \left(0.875 \times \frac{60 \ Watts}{15 \ Watts} - 1\right) \times 15 \ Watts$$

$$Watt_{\Delta} = 37.5 \ Watts$$

$$AKWH = (37.5 \ Watts) \times 2.97 \ hrs / day \times 365 \ days / year \div 1000 \ Watts / Watt - hr$$

$$AKHW = 40.65 \ kWh / yr$$

Example 2. A 19-Watt General Service CFL bulb is installed in the kitchen of a Low-Income home by direct install in 2013. The wattage of the incandescent bulb that was replaced is not known. What are the annual savings?

Using the equations from above:

$$Watt_{\Delta} = (Watt_{ratio} - 1) \times Watt_{post}$$
$$AKWH = \frac{Watt_{\Delta} \times h_{d} \times 365^{days}/_{yr}}{1000^{W/_{bW}}}$$

This bulb is affected by the EISA standards. From Table 1 we obtain h_d for the Low-Income location given. Table 2 provides the Watt_{ratio} to be used in calculations for unknown Watt_{pre}:

$$\begin{aligned} &Watt_{\Delta} = (2.5-1)\times 19 \ Watts \\ &Watt_{\Delta} = 28.5 \ Watts \\ &AKWH = (28.5 \ Watts)\times 3.66 \ \frac{hrs}{day}\times 365 \ \frac{days}{year} \div 1000 \ \frac{Watts}{Watt-hr} \\ &AKHW = 38.1 \ \frac{kWh}{yr} \end{aligned}$$

Retrofit Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

$$SKW = Watt_{\Delta} \times CF_S \div 1000 \frac{w}{kW}$$

 $WKW = Watt_{\Delta} \times CF_W \div 1000 \frac{w}{kW}$

Note: General Service Bulbs affected by EISA compliance will utilize the same calculation methodology as described for annual and lifetime savings.

Values for CF_s and CF_w can be found in Appendix 1 as the Residential; Lighting Coincidence Factors.

Retrofit Gross Peak Demand Savings, Example

Example 3. A 60-Watt General Service incandescent bulb is replaced with a 15-Watt General Service CFL bulb in the living room of a Non-Low Income home by direct install in 2013. What are the savings?

$$Watt_{\Delta} = \left(0.875 \times \frac{60 \text{ Watts}}{15 \text{ Watts}} - 1\right) \times 15 \text{ Watts}$$

$$Watt_{\Delta} = 37.5 \text{ Watts}$$

$$SKW = 37.5 \text{ Watts} \times 0.09 \div 1000 \frac{W}{kW}$$

$$SKW = 0.003375 \text{ kW}$$

$$WKW = 37.5 \ Watts \times 0.26 \div 1000 \ \frac{W}{kW}$$

 $WKW = 0.00975 \ kW$

Example 4. A 19-Watt General Service CFL bulb is installed in the kitchen of a Low-Income home by direct install in 2013. The wattage of the incandescent bulb that was replaced is not known. What are the savings?

$$Watt_{\Lambda} = (2.5-1) \times 19 Watts$$

$$Watt_{\Lambda} = 28.5 Watts$$

$$SKW = 28.5 Watts \times 0.09 \div 1000 W/kW$$

$$SKW = 0.00257 \ kW$$

$$WKW = 28.5 \ Watts \times 0.26 \div 1000 \ W_{kW}$$

$$WKW = 0.00741 \, kW$$

Lost Opportunity Gross Energy Savings, Electric

$$Watt_{\Delta} = (Watt_{ratio} - 1) \times Watt_{post}$$
$$AKWH = \frac{Watt_{\Delta} \times h_d \times 365^{\frac{days}{yr}}}{1000^{\frac{W}{kW}}}$$

If the location of the installed bulb is known, use the value from Table 1. Otherwise, use $h_d = 2.77$ ("Unknown" from Table 1, as it cannot be verified where a purchased bulb is installed).

Please refer to Table 3 for the appropriate Watt_{ratio} to be used in all Lost Opportunity, Residential New Construction, and Retail Product calculations.

Table 3: Lost Opportunity and Retail Wattratio Values

| | New Bulb | | | | | nr Watt _{ratio} npliant) | |
|--|-------------|----------------|------------------------------------|---|------------------------------|--------------------------------------|-----------------|
| Install Type | Bulb | Lumen Range | Approximate CFL Equivalent Wattage | Approximate LED Equivalent Wattage | CFL Watt _{ratio} | LED Watt _{ratio} | Notes |
| | | 1490-2600 | 23W-30W | 23W to 30W | 3.00 | 3.0 | Notes [1,3,9] |
| General Service | CFL,LED, | 1050-1489 | 18W- <23W | 13W - <23W | 3.25 | 3.1 | Notes [1,3,9] |
| Scrvice | & Induction | 310-1049 | 9W-<18W | 6W - <13W | 3.50 | 3.2 | Notes [1,3,6,9] |
| Non- | | A 11 1 | | | | 00 | Notes [1,6] |
| General Service & Directional ranges Directional ranges | | All Equivalent | Wattages | 4.00 | 5.00 | Note [1,6] | |

[†] For bulb types not listed use the Wattratio values for CFL bulbs

Lost Opportunity Gross Energy Savings, Example

Example 5. What are the electric energy savings when a 13-Watt General Service CFL is purchased through a retailer?

This bulb is subject to EISA standards. Table 1 provides h_d and Table 3 provides the equivalent Watt_{ratio}.

$$Watt_{\Delta} = (3.50 - 1) \times 13 \, Watts$$

$$Watt_{\Delta} = 32.5 \, Watts$$

$$AKWH = (32.5 \, Watts) \times 2.77 \, \frac{hrs}{day} \times 365 \, \frac{days}{year} \div 1000 \, \frac{Watts}{Watt - hr}$$

$$AKHW = 32.9 \, \frac{kWh}{yr}$$

Example 6. What are the electric energy savings from an 11-Watt Non-General Service CFL bulb rated for 8,000 hours purchased through a retailer?

This bulb is not subject to EISA standards.

$$Watt_{\Delta} = (4.0 - 1) \times 11 \, Watts$$

$$Watt_{\Delta} = 33 \, Watts$$

$$AKWH = (33 \, Watts) \times 2.77 \, \frac{hrs}{day} \times 365 \, \frac{days}{year} \div 1000 \, \frac{Watts}{Watt - hr}$$

$$AKHW = 33.4 \, \frac{kWh}{yr}$$

Lost Opportunity Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

$$SKW = Watt_{\Delta} \times CF_S \div 1000 \%_{kW}$$

 $WKW = Watt_{\Delta} \times CF_W \div 1000 \%_{kW}$

Note: General Service Bulbs affected by EISA compliance will utilize the same calculation methodology as described for annual and lifetime savings.

Lost Opportunity Gross Peak Demand Savings, Example

Example 7. What are the electric energy savings when a 13-Watt General Service CFL is purchased through a retailer in 2013?

This bulb is subject to EISA standards.

$$Watt_{\Lambda} = (3.50 - 1) \times 13 Watts$$

$$Watt_{\Lambda} = 32.5 Watts$$

$$SKW = 32.5 \ Watts \times 0.09 \div 1000 \ W_{kW}$$

$$SKW = 0.00293 \ kW$$

$$WKW = 32.5 \ Watts \times 0.26 \div 1000 \ W_{hW}$$

$$WKW = 0.00845 \ kW$$

Example 8. What are the electric energy savings from an 11-Watt Non-General Service CFL bulb rated for 8,000 hours purchased through a retailer in 2013?

This bulb is not subject to EISA standards.

$$Watt_{\Lambda} = (4.00 - 1) \times 11 Watts$$

$$Watt_{\Lambda} = 33 Watts$$

$$SKW = 33 Watts \times 0.09 \div 1000 W/_{kW}$$

$$SKW = 0.00297 \ kW$$

$$WKW = 33 Watts \times 0.26 \div 1000 \frac{W}{kW}$$

$$WKW = 0.00858 \, kW$$

Non Energy Benefits

Table 4: One time O&M benefit per bulb (Note [4]):

| General Service CFL bulb | \$3.00 |
|------------------------------|---------|
| Non-General Service CFL bulb | \$4.00 |
| LED General Service bulb | \$11.50 |
| LED Non-General Service bulb | \$11.50 |
| LED Directional/Downlight | \$14.00 |

Changes from Last Version

Clarified tables, examples, and organization for ease-of-use, while maintaining EISA compliance. Re-calculated Watt ratios based on lifetimes found in Appendix 4. Updated the measure to account for LED lighting, and calculated appropriate Watt ratios for those bulbs. Added the one-time O&M benefit per bulb for LED Non-General Service bulbs.

References

- [1] KEMA, Evaluation of the Weatherization Residential Assistance Partnership (WRAP) and Helps Programs, September 10, 2010. Table 22, page 7-2.
- [2] Nexus Market Research (NMR), Residential Lighting Markdown Impact, January 20, 2009. Table 5-15, page 51.
- [3] RLW Analytics, Coincidence Factor Study Residential and Commercial & Industrial Lighting Measures, March 25, 2007. Tables i-3 and i-4, page IV.
- [4] US Congress, Energy Independence and Security Act of 2007 (EISA), Title III, "ENERGY SAVINGS THROUGH IMPROVED STANDARDS FOR APPLIANCE AND LIGHTING," January 4, 2007.
- [5] RLW Analytics, Northeast Utilities SPECTRUM Lighting Catalog and Retail Lighting Programs Hours of Use Re-Analysis, December 20, 2001. Table 7, page 14.

Notes

- [1] The Watt ratio is modified to reflect the upcoming (to be implemented 2012 through 2014) 2007 EISA federal standards (Ref [4]) which will require new General Service incandescent bulbs to have about 75% lower wattage. Non-General Service bulbs continue to use the established Watt ratio, while all General Service bulbs use 75% of this established Watt ratio.
- [2] The h_d value for "Unknown" location is the average hours per day across all locations. This may not be used for direct install after installation, since location must be verified by the installer. It is most applicable for retail bulbs since the final location is unknown.

[3] The upcoming federal standard requires incandescent bulbs to use 75% of the wattage of standard General Service incandescent bulbs. 4/3 is the Watt ratio reflecting this.

- [4] One time O&M benefits are based on the avoided expense of replacement incandescent bulbs over the lifetime of the new bulb. For instance, using \$0.50 per incandescent bulb, 10,000-hr CFLs avoid the use of 8 1000-hr incandescent bulbs: \$4.00. 25,000-hr General Service LEDs avoid the use of 23 1000-hr incandescent bulbs: \$11.50.
- [5] In the case of Non-General Service bulbs where existing wattage is known, the Delta Watts calculation simplifies to its definition of Watt_{Δ} = Watt_{pre} Watt_{post}.
- [6] LED Watt ratios based on the labeled efficacy in lumens/Watt (lm/W) of typical LED bulbs compared to the lm/W of a typical incandescent bulb.
- [7] Note that the baseline does not change until the second year of the standard; this is due to several factors causing a delay in the immediate effects of the standard such as the lifetime of existing incandescent bulbs being about a year, stockpiling, and other unknowns.
- [8] Years at full and reduced level are based on the implementation schedule of EISA compliance (Ref [4]).
- [9] Table 5 shows the EISA schedule and number of years at full savings level for certain General-Service bulbs, all programs, for the benefit of the reader:

Table 5: EISA Schedule and Number of Years at Full Savings Level for Certain General-Service Bulbs, All Programs

| | Approximate CFL Wattage within lumen | Year EISA standard becomes | Baseline Implementation | | | t Full Savi | _ |
|---------------------|--|----------------------------------|----------------------------|------|------|-------------|------|
| Lumen Ranges | range | effective | Year (BIY) | 2012 | 2013 | 2014 | 2015 |
| 1490-2600 | 23W to 30W | 2012 | 2013 | 1 | 0 | 0 | 0 |
| 1050-1489 | 18W to <23W | 2013 | 2014 | 2 | 1 | 0 | 0 |
| 310–749, 750–1049 | 9W to <18W | 2014 | 2015 | 3 | 2 | 1 | 0 |

The weighted average Watt ratios presented in this measure serve as a means to simplify calculation of annual and lifetime savings. Values presented for General Service CFL bulbs in the EISA Lumen range are based on a 4 year lifetime while those presented for General Service LED bulbs are based on a 10 year lifetime (from Appendix 1).

Using General Service CFL bulbs as an example, 3 years at full savings would utilize a Watt_{ratio} = 4, with the 4^{th} (and final) year at reduced savings with Watt_{ratio} = 3. This is mathematically equivalent to 4 years of savings at Watt_{ratio} = 3.25. Using Example 3 from the measure, this is demonstrated as follows:

Example 3: What are the electric energy savings when a 13 Watt General Service program CFL is purchased through a retailer?

The two calculations below demonstrate that the lifetime savings using the weighted equivalent Watt_{ratio} are equal to the lifetime savings as calculated individually for each year in the lifetime:

- First, the weighted equivalent Watt_{ratio} from Table 2A is used to calculate AKWH and LKWH: $Watt_{\Delta} = (3.50-1) \times 13 Watts = 32.5 Watts$ $AKWH_{full} = (32Watts) \times 2.77 \frac{hrs}{day} \times 365 \frac{days}{year} \div 1000 \frac{Watts}{Watt} \bullet hr = 32.9 kWh$ $LKWH = (32.9 kWh) \times 4 = 131.4 kWh$
- Next, each year is calculated out separately as the EISA bulb moves through the implementation cycle (Notes [7,8]):

$$Watt_{\Lambda full} = (4.0 - 1) \times 13Watts = 39Watts$$

$$AKWH_{full} = (39Watts) \times 2.77 \frac{hrs}{day} \times 365 \frac{days}{year} \div 1000 \frac{Watts}{Watt} \bullet hr = 39.4 kWh$$

For Years 3-4 (Reduced Savings)

$$Watt_{\Delta,reduced} = (3.0-1) \times 13Watts = 26Watts$$

$$AKWH_{reduced} = (26Watts) \times 2.77 \, \frac{hrs}{day} \times 365 \, \frac{days}{year} \div 1000 \, \frac{Watts}{Watt} \bullet hr = 26.3 \, kWh$$

For the lifetime add the years together:

$$LKWH = \left(39.4 \frac{kWh}{yr} \times 2 \text{ years}\right) + \left(26.3 \frac{kWh}{yr} \times 2 \text{ years}\right) = 131.4 kWh$$

4.1.2 LUMINAIRE

Description of Measure

Replacement of low efficiency hardwired or portable luminaires/lighting fixtures with luminaires/lighting fixtures incorporating high efficiency lights, excluding those with screw-based lampholders (which are treated as light bulbs in Measure 4.1.1 for savings calculations). An efficient luminaire is a complete lighting unit that meets ENERGY STAR specifications, and consists of all the parts designed to distribute the light, position and protect the lamps, and connect to the power supply.

Savings Methodology

The savings methodology can be applied to the following examples of fixture types: hardwired exterior, security exterior, hardwired indoor (such as recessed downlights, fan lighting kits-separate or included with fan), portable lamps (such as table lamps, desk lamps, floor lamps), torchieres. Multiple pin-based or integrated lighting technologies are covered that might include Solid State Lighting (SSL, LED), Induction Lamp, Fluorescent, and Compact Fluorescent Lamp (CFL). Fixtures with screw-based lampholders are not included here in order to ensure that only qualified high-efficiency bulbs will be used in the fixture. See Note [5] for restrictions to Torchieres.

High efficiency Lighting products are those that meet the ENERGY STAR specification for Luminaires.

Note that only the energy savings from the light is considered. Therefore, savings for this measure is based on the total light wattage of the assembly. Any fan motor savings (e.g. from ceiling fans) are negligible, and cooling savings have not been determined.

A lighting project should be custom only if it clearly exhibits outlier type behavior which would clearly make the existing savings algorithms inappropriate to use and if the existing savings assumptions would produce an error of unacceptable magnitude. In such a case, the energy and demand savings should be well documented. Since linear fluorescent fixtures are less common in a residential setting, they shall be treated as a custom measure, as well as any other technology not specifically referenced in this document.

Inputs

| Symbol | Description | Units |
|----------------------|---|-------|
| Watt _{post} | Rated wattage of installed or purchased high efficiency fixture. For fixtures with multiple | Watts |
| • | bulbs, this is the total wattage (not the wattage of one bulb). | |
| Watt _{pre} | Rated wattage of low efficiency fixture being replaced by direct install. For fixtures with | Watts |
| • | multiple bulbs, this is the total wattage (not the wattage of one bulb). | |
| Location | Location of direct install fixture. Table 1 lists the available options for this. | N/A |
| Bulb Type | Technology of new bulb. Used primarily to determine measure life. | |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|-----------------|---|-----------|-----------------|---------------------|
| AKWH | Annual Electric Energy Savings | kWh | | Calculated |
| CF _S | Average summer seasonal peak coincidence | unit-less | | Appendix A, Ref [3] |
| | factor | | | |
| CF _S | Average winter seasonal peak coincidence factor | unit-less | | Appendix A, Ref [3] |
| h_d | Daily hours of use, by room type for direct | hours per | RP: Table 2 | Ref [2] |
| | install, By fixture type or Unknown for RP | day | Direct Install: | |
| | | | Table 1 | |
| LI | Corresponding to the Low Income sector | | | |
| RNC | Corresponding to Residential New Construction | | | |
| | sector | | | |

| Symbol | Description | Units | Values | Comments |
|-----------------------|---|-----------|---------|---|
| RP | Corresponding to the Retail Products sector | | | |
| SKW | Summer Demand Savings | kW | | Calculated |
| $Watt_{\Delta}$ | Delta Watts, the difference between the wattage | Watts (W) | | Calculated |
| | of the lower efficiency baseline and the wattage | | | |
| | of the new fixture. | | | |
| Watt _{post} | Rated wattage of high efficiency fixture. | Watts (W) | Input | |
| Watt _{pre} | Rated wattage of existing low efficiency fixture. | Watts (W) | Input | Direct install only |
| Watt _{ratio} | Wattage ratio between low efficiency fixture and | unit-less | Table 2 | Defined as: |
| | high efficiency fixture. | | | $Watt_{ratio} = \frac{Watt_{pre}}{Watt_{post}}$ |
| WKW | Winter Demand Savings | kW | | Calculated |

Retrofit Gross Energy Savings, Electric

$$Watt_{\Delta} = (Watt_{ratio} - 1) \times Watt_{post} \text{ (Note [4])}$$

$$AKWH = \frac{Watt_{\Delta} \times h_d \times 365^{\frac{days}{yr}}}{1000^{\frac{w}{kW}}}$$

Table 1: Hours of Use per Day by Location, Direct Install

| Location | Non-Low Income | Low Income |
|---------------------|----------------|------------|
| Location | $h_{d,NLI}$ | $h_{d,LI}$ |
| Bedroom | 1.08* | 1.60*** |
| Bathroom | 0.65* | 1.60*** |
| Den/Office | 2.97** | 2.97** |
| Garage | 1.32* | 1.32* |
| Hallway | 6.25* | 1.74*** |
| Kitchen | 2.97** | 3.66*** |
| Living Room | 2.97** | 3.20*** |
| Dining Room | 2.97** | 2.97** |
| Exterior | 2.89* | 2.89* |
| Basement | 1.29* | 1.45*** |
| Closet | 1.24* | 1.24* |
| Security Exterior † | 11.4 | 11.4 |
| Other | 2.05** | 2.05** |
| Unknown †† | 2.77** | 2.77** |

^{*}Ref [4]

^{**}Ref [2]

^{***}Ref [1]

[†] Note [1], Security Exterior install locations do not claim Summer Peak savings, since hours of operation are outside Summer Peak boundaries

^{† †} Note [2], Table 5-15

| Table 2: Wattratio | Values for | Luminaires, | both Retrofit | and Lost (| Opportunity Installs |
|--------------------|------------|-------------|---------------|------------|----------------------|
| | | | | | |

| Existing Wattage | Technology | Watt _{ratio} | Notes |
|---------------------|--------------------------------|---|----------------------------|
| | Fluorescent Torchieres | 3.40 | Ref [2], Table 5-19, p. 57 |
| Unknown | Retail CFL | 3.948 | Note [5] |
| | Retail LED | 4.00 | |
| | †CFL/LED Directional/Downlight | See 4.1.1 Light Bulbs, Table 3 | Note [6] |
| Known | All | $Watt_{ratio} = \frac{Watt_{pre}}{Watt_{post}}$ | |

[†] CFL/LED Directional/Downlight products are treated as a lighting product. See Table 3 in measure 4.1.1 Lighting for details

Retrofit Gross Energy Savings, Example

Example 1: A 60-Watt ceiling fixture is replaced with a 15-Watt CFL pin based fixture in the bathroom of a home by direct install.

$$Watt_{\Delta} = \left(\frac{60 \text{ Watts}}{15 \text{ Watts}} - 1\right) \times 15 \text{ Watts}$$

$$Watt_{\Delta} = 45 \text{ Watts}$$

$$AKWH = (45 \text{ Watts}) \times 1.60 \frac{hrs}{day} \times 365 \frac{days}{year} \div 1000 \frac{Watts}{kWh}$$

$$AKHW = 26.3 \frac{kWh}{yr}$$

Example 2: An existing fixture is replaced with a 18-Watt equivalent CFL fixture in the living room of a low-income home by direct install. The existing wattage is not known. What are the energy savings?

$$Watt_{\Delta} = (3.948 - 1) \times 15 Watts$$
 $Watt_{\Delta} = 53 Watts$

$$AKWH = (53 Watts) \times 3.20 \frac{hrs}{day} \times 365 \frac{days}{year} \div 1000 \frac{Watts}{kWh}$$

$$AKHW = 52.6 \frac{kWh}{yr}$$

Retrofit Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

$$SKW = Watt_{\Delta} \times CF_S \div 1000 \frac{W}{kW}$$

 $WKW = Watt_{\Delta} \times CF_W \div 1000 \frac{W}{kW}$

Retrofit Gross Peak Demand Savings, Example

Example 1: A 60-Watt ceiling fixture is replaced with a 15-Watt CFL pin based fixture in the bathroom of a home by direct install.

$$Watt_{\Delta} = \left(\frac{60 \, Watts}{15 \, Watts} - 1\right) \times 15 \, Watts$$

$$Watt_{\Lambda} = 45 Watts$$

$$SKW = 45 Watts \times 0.09 \div 1000 W/kW$$

$$SKW = 0.00405 \ kW$$

$$WKW = 45 Watts \times 0.26 \div 1000 W/_{kW}$$

$$WKW = 0.012 \ kW$$

Example 2: An existing fixture is replaced with a 18-Watt equivalent CFL fixture in the living room of a low-income home by direct install. The existing wattage is not known. What are the peak demand savings?

$$Watt_{\Lambda} = (3.948 - 1) \times 18 Watts$$

$$Watt_{\Lambda} = 53 Watts$$

$$SKW = 53 Watts \times 0.09 \div 1000 W/_{kW}$$

$$SKW = 0.00477 \ kW$$

$$WKW = 53 Watts \times 0.26 \div 1000 \frac{W}{kW}$$

$$WKW = 0.0138 \, kW$$

Lost Opportunity Gross Energy Savings, Electric

$$Watt_{\Delta} = (Watt_{ratio} - 1) \times Watt_{post} \text{ (for Torchieres, Note [5], Watt_{\Delta} is capped at 190 - Watt_{post})}$$

$$AKWH = \frac{Watt_{\Delta} \times h_d \times 365^{\frac{days}{yr}}}{1000^{\frac{W}{kW}}}$$

Please refer to Table 2 for Watt_{ratio} values.

Table 3: Hours of Use per Day by Fixture Type, Retail (Ref [2])

| Fixture Type | $\mathbf{h_d}$ |
|-----------------------|----------------|
| Hardwired Indoor | 2.53 |
| Portable – Table Lamp | 2.38 |
| Portable - Torchiere | 2.38 |
| Hardwired Exterior | 2.53 |
| Security Exterior † | 11.4 |
| Unknown †† | 2.77 |

[†] Note [1], Security Exterior install locations do not claim Summer Peak savings, since hours of operation are outside Summer Peak boundaries

Lost Opportunity Gross Energy Savings, Example

Example 3: A 26-Watt ceiling fixture (using two 13 Watt pin-based CFLs) is purchased through a retailer.

$$Watt_{\Lambda} = (3.948 - 1) \times 26 Watts$$

$$Watt_{\Delta} = 77 Watts$$

^{††} Ref[2], Table 5-15

$$AKWH = (77 Watts) \times 1.60 \frac{hrs}{day} \times 365 \frac{days}{year} \div 1000 \frac{Watts}{kWh}$$
$$AKHW = 77.9 \frac{kWh}{yr}$$

Lost Opportunity Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

$$SKW = Watt_{\Delta} \times CF_S \div 1000 \frac{w}{kW}$$

 $WKW = Watt_{\Delta} \times CF_W \div 1000 \frac{w}{kW}$

Lost Opportunity Gross Peak Demand Savings, Example

Example 3: A 26-Watt CFL ceiling fixture is purchased through a retailer. What are the peak demand savings?

$$SKW = 77.9 \ Watts \times 0.09 \div 1000 \ W_{kW}$$

 $SKW = 0.00701 \, kW$

$$WKW = 77.9 \ Watts \times 0.26 \div 1000 \ W_{kW}$$

 $WKW = 0.0203 \ kW$

Non Energy Benefits

Table 4: One time O&M Benefit per Bulb (Note [3])

| Туре | Benefit |
|-----------------------|---------|
| Hardwired Indoor | \$14.00 |
| Portable – Table Lamp | \$6.00 |
| Portable – Torchiere | \$5.00 |
| Hardwired Exterior | \$14.00 |
| Security Exterior | \$14.00 |

Changes from Last Version

Collected Watt ratios into Table 2; clarifying language added to Description and Methodology sections

References

- [1] KEMA, Evaluation of the Weatherization Residential Assistance Partnership (WRAP) and Helps Programs, September 10, 2010. Table 22, page 7-2.
- [2] Nexus Market Research (NMR), Residential Lighting Markdown Impact, January 20, 2009. Table 5-13, page 50, and Table 5-15, page 51.
- [3 RLW Analytics, Coincidence Factor Study Residential and Commercial & Industrial Lighting Measures, March 25, 2007. Tables i-3 and i-4, page IV.
- [4] RLW Analytics, Northeast Utilities SPECTRUM Lighting Catalog and Retail Lighting Programs Hours of Use Re-Analysis, December 20, 2001. Table 7, page 14.

Notes

[1] The "Security" location refers only to exterior lights that are programmed to run continuously through the night. The hours are based on UI annual hours for rate class MH for street lighting. The "Security" designation does not refer to exterior lights that operate sporadically.

- [2 The "Other" location (Ref [2]) included exterior, mudroom, playroom, sunroom, studio, closet, laundry, and various workrooms.
- [3] One time O&M benefits are based on the avoided expense of replacement incandescent bulbs over the lifetime of the new bulb.
- [4] Note that in the case of direct install, where existing wattage is known, the Delta Watts calculation simplifies to its definition of $Watt_{\Delta} = Watt_{pre} Watt_{post}$.
- [5] Public Act 04-85, An Act Concerning Energy Efficiency Standards, July 2004, limits torchiere wattage to 190 Watts. Therefore, the baseline for torchieres is capped at 190 watts, and: Watt_{ratio} is capped at 3.4, and Watt_{pre} is capped at 190 Watts.

4.2 HVAC

4.2.1 ENERGY EFFICIENT CENTRAL AC

Description of Measure

Installation of an energy efficient central air conditioning (AC) system and replacement of a working inefficient AC system.

Savings Methodology

Lost Opportunity Measure:

• Lost Opportunity savings are the difference in energy use between a baseline new model (Note [3]), and the chosen high efficiency new model, continuing for the Effective Useful Life (EUL) from Appendix 4.

Retrofit Measure:

- Uses the same methodology as a Lost Opportunity measure.
- In the case of early retirement of a working unit where the unit would have otherwise been installed until failure, lifetime "Retirement" savings are claimed additional to the lifetime "Lost Opportunity" savings (see Section 1.4).
- Retirement savings are the difference in energy use between the older unit (Note [2]) and a baseline new model (Note [3]), continuing for the Remaining Useful Life (RUL) from Appendix 4.

Savings are based on the Residential Central AC Regional Evaluation (CAC) (Ref [1]). The regional study metered the usage of recently installed residential AC units in New England. Using these measurements the study provided factors and equations (see below) to calculate the savings using the installed capacity and the Energy Efficiency Ratio (EER).

Inputs

| Symbol | Description | Units |
|------------------|--|-------------|
| $CAP_{C,i}$ | Installed cooling capacity of new unit | Tons |
| EER _i | Installed EER of new unit | Btu/Watt-hr |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|------------------|--|-------------|-------------------|----------|
| $AKWH_C$ | Annual electric energy savings - cooling | kWh | | |
| ASF | Annual Savings factor | kWh/ton | 357.6 | Note [1] |
| $CAP_{C,i}$ | Installed cooling capacity | Tons | | Input |
| DSF | Seasonal demand savings factor | kW/ton | 0.591 | Note [1] |
| EER _b | Baseline EER, representing baseline new | Btu/Watt-hr | 11 | Note [2] |
| | model | | | |
| EER _e | Existing EER of removed unit | Btu/Watt-hr | Use 8 if existing | Note [3] |
| | | | EER is not known | |
| EER _i | Installed EER of new efficient unit | Btu/Watt-hr | | Input |
| EUL | Effective Useful Life | Years | Appendix 4 | |
| $LKWH_C$ | Lifetime electric energy savings - cooling | kWh | | |
| RUL | Remaining Useful Life | Years | Appendix 4 | |
| SKW_C | Summer Seasonal Demand savings-cooling | kW | | |
| · · · Retire | Associated with Retirement | | | |
| · · · Lost Opp | Associated with Lost Opportunity | | | |

Retrofit Gross Energy Savings, Electric

Reminder: Retrofit savings are the sum of Retirement savings and Lost Opportunity savings. This section presents the Retirement portion of savings while the Lost Opportunity portion of the savings is presented further on in this measure. To obtain the lifetime savings, the following formula should be used:

$$LKWH_{C, Total} = AKWH_{C, Retire} \times RUL + AKWH_{C, Lost Opp} \times EUL$$

Retirement Component:

$$AKWH_{C, Retire} = ASF \times CAP_{C,i} \times \left(1 - \frac{EER_e}{EER_b}\right)$$

The equation simplifies when the existing EER is not known:

$$AKWH_{C, Retire} = 357.6 \, \frac{kWh}{ton} \times CAP_{C,i} \times \left(1 - \frac{8}{11}\right) = 97.53 \, \frac{kWh}{ton} \times CAP_{C,i}$$

Retrofit Gross Energy Savings, Example

An existing working central A/C is replaced by an energy efficient unit. The new installed unit has a 3 ton cooling capacity, at 13.0 EER. What are the annual energy savings?

To calculate the lost opportunity component, use the equation from "Lost Opportunity":

$$AKWH_{C, Lost Opp} = 357.6 \, \text{kWh/ton} \times CAP_{C,i} \times \left(\frac{EER_i}{11} - 1 \right)$$

Input the new unit's cooling capacity and rated EER:

$$AKWH_{C, Lost Opp} = 357.6 \, kWh_{ton} \times 3 \, tons \times \left(\frac{13.0}{11} - 1\right) = 195 \, kWh$$

Because the existing unit is verified to be in working condition, use the Retirement equation to calculate annual Retirement savings (a constant times the new unit's cooling capacity):

$$AKWH_{C,Retire} = 97.53 \, \frac{kWh}{ton} \times CAP_{C,i}$$

 $AKWH_{C,Retire} = 97.53 \, \frac{kWh}{ton} \times 3 \, tons = 293 \, kWh$

Retrofit Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

Reminder: Retrofit savings are the sum of Retirement savings and Lost Opportunity savings. This section presents the Retirement portion of savings while the Lost Opportunity portion of the savings is presented further on in this measure.

Retirement Component:

$$SKW_{C, Retire} = DSF \times CAP_{C,i} \times \left(1 - \frac{EER_e}{EER_h}\right)$$

The equation simplifies when the existing EER is not known:

$$SKW_{C, Retire} = 0.591 \, \text{kW/ton} \times CAP_{C,i} \times \left(1 - \frac{8}{11}\right) = 0.161 \, \text{kW/ton} \times CAP_{C,i}$$

Note: There is no need to apply a coincidence factor as coincidence is already factored into the demand equation.

Retrofit Gross Peak Demand Savings, Example

What are the summer demand savings for the above retrofit example?

Using the equation for Lost Opportunity summer demand savings, input the size and efficiency of the new unit:

$$SKW_{C, Lost Opp} = 0.591^{kW}/_{ton} \times CAP_{C,i} \times \left(\frac{EER_i}{11} - 1\right)$$

$$SKW_{C, Lost Opp} = 0.591^{kW}/_{ton} \times 3 \ tons \times \left(\frac{13.0}{11} - 1\right) = 0.322 \ kW$$

Using the equation for Retirement summer demand savings, input the cooling capacity in tons:

$$SKW_{C, Retire} = 0.161^{kW}/_{ton} \times CAP_{C,i}$$

$$SKW_{C, Retire} = 0.161^{kW}/_{ton} \times 3 \ tons = 0.483 \ kW$$

Lost Opportunity Gross Energy Savings, Electric

$$AKWH_{C,Lost\ Opp} = ASF \times CAP_{C,i} \times \left(\frac{EER_i}{EER_b} - 1\right)$$

$$AKWH_{C,Lost\ Opp} = 357.6 \, \frac{kWh}{ton} \times CAP_{C,i} \times \left(\frac{EER_i}{11} - 1\right)$$

Lost Opportunity Gross Energy Savings, Example

A rebate is provided for the installation of a new energy efficient unit. The old unit is unknown. The new installed unit has a 3 ton cooling capacity, 13.0 EER. What are the annual savings?

To calculate annual savings, use the Lost Opportunity equation:

$$AKWH_{C, Lost Opp} = 357.6 \, \frac{kWh}{ton} \times CAP_{C,i} \times \left(\frac{EER_i}{11} - 1\right)$$

Input the new unit's cooling capacity and rated EER

$$AKWH_{C, Lost Opp} = 357.6 \, kWh_{ton} \times 3 \, tons \times \left(\frac{13.0}{11} - 1\right) = 195 \, kWh$$

Lost Opportunity Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

$$SKW_{C,Lost\ Opp} = DSF \times CAP_{C,i} \times \left(\frac{EER_i}{EER_b} - 1\right)$$

$$SKW_{C,Lost\ Opp} = 0.591^{kW}/_{ton} \times CAP_{C,i} \times \left(\frac{EER_i}{EER_b} - 1\right)$$

Note: There is no need to apply a coincidence factor as coincidence is already factored into the demand equation

Lost Opportunity Gross Peak Demand Savings, Example

A rebate is provided for the installation of a new energy efficient unit. The old unit is unknown. The new installed unit has a 3 ton cooling capacity, 13.0 EER. What are the annual demand savings?

Using the equation for Lost Opportunity demand savings,

$$SKW_{C, Lost Opp} = 0.591 \, \text{kW/}_{ton} \times CAP_{C,i} \times \left(\frac{EER_i}{11} - 1\right)$$

Input the size and efficiency of the new unit:

$$SKW_{C, Lost Opp} = 0.591 \, \frac{kW}{ton} \times 3 \, tons \times \left(\frac{13.0}{11} - 1\right) = 0.322 \, kW$$

Changes from Last Version

The presentation of retirement savings has been refreshed. Retrofit measure is more clearly presented as two-part savings that may be added together if qualified. However, there are no changes to the methodology or calculations.

References

[1] Residential Central AC Regional Evaluation, ADM Associates, Inc., November 2009.

Notes

[1] The values were calculated based on the ADM study (Ref [1], Table 4-7, page 4-9, and Table 6-2, page 6-1):

$$Total \ tons \ in \ study = \frac{Annual \ Savings}{Annual \ Savings \ per \ ton} = \frac{368,531 \ kWh}{39 \ kWh/_{ton}} = 9,450 \ tons$$

$$ASF = \frac{Total \ Annual \ Usage}{Total \ tons} = \frac{3,379,210 \ kWh}{9,450 \ tons} = 357.6 \ kWh/_{ton}$$

$$DSF = \frac{Total \ Average \ Annual \ Demand}{Total \ tons} = \frac{5,588.3 \ kW}{9,450 \ tons} = 0.591 \ kW/_{ton}$$

- [2] Ref [1], ADM study page 4-1. "Because there were no instances of early replacement of CAC units in the monitoring sample, the baseline for estimating savings is the minimum standard for new installations, namely 11 EER."
- [3] EER for the existing unit is estimated based on average installed efficiency for an approximately 15 year old unit. ASHRAE/IESNA Standard 90.1-1999 Table 6.2.1A has a minimum requirement of 10 SEER for 2011. *Note:* Units of that vintage were only rated on SEER. EER is approximately 80% of SEER (Ref [1], page ES-1 gives the ratio 11 EER / 14 SEER). 8 EER is used as the estimated existing efficiency.

4.2.2 HEAT PUMP

Description of Measure

Installation of an energy efficient air source heat pump and replacement of a working, less efficient electric heating system, including heat pumps and electric resistance heating.

Savings Methodology

Lost Opportunity Measure:

• Lost Opportunity savings are the difference in energy use between a baseline new model (Note [2]), and the chosen high efficiency new model, continuing for the Effective Useful Life (EUL) from Appendix 4.

Retrofit Measure:

- Uses the same methodology as a Lost Opportunity measure.
- In the case of early retirement of a working unit where the unit would have otherwise been installed until failure, lifetime "Retirement" savings are claimed additional to the lifetime "Lost Opportunity" savings (see Section 1.4).
- Retirement savings are the difference in energy use between the older unit (Note [1]) and a baseline new model (Note [2]), continuing for the Remaining Useful Life (RUL) from Appendix 4.

The savings methodology presented here is for heating only; cooling savings from an efficient heat pump are the same as the cooling savings for an efficient central air conditioner, as presented in measure 4.2.1 of this manual.

Note: the savings here do not apply to a Ductless Heat Pump; see Measure 4.2.12 for Ductless Heat Pump methodology.

Inputs

| Symbol | Description | Units |
|-------------------|--|-----------------|
| $CAP_{H,i}$ | Installed Heating Capacity | Btu/hr |
| HSPF _e | Heating Season Performance Factor of existing unit (AHRI-Verified) | Btu/Watt- hr |
| HSPF _i | Heating Season Performance Factor, installed unit (AHRI-Verified) | Btu/Watt- hr |
| | Existing heating system type | |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|-------------------|--|------------|-----------------------------|----------|
| AKWH | Annual Electric Energy Savings | kWh | | |
| $CAP_{H,i}$ | Installed Heating Capacity | Btu/hr | | Input |
| EFLH _H | Heating Equivalent Full-Load Hours | Hours | 1307 | Note [3] |
| HSPF _b | Heating Season Performance Factor, Baseline, | Btu/ Watt- | 7.7 | Note [1] |
| | representing baseline new model | hr | | |
| HSPF _e | Heating Season Performance Factor, Existing | Btu/ Watt- | Use 6.8 if HSPF existing is | Note [2] |
| | (AHRI-Verified) | hr | not known; 3.41 for | |
| | | | electric resistance heat | |
| $HSPF_i$ | Heating Season Performance Factor, Installed | Btu/ Watt- | | Input |
| | (AHRI-Verified) | hr | | |
| SKW | Summer Demand Savings | kW | | |
| WKW | Winter Demand Savings | kW | | |

Retrofit Gross Energy Savings, Electric

Reminder: Retrofit savings are the sum of Retirement savings and Lost Opportunity savings. This section presents the Retirement portion of savings while the Lost Opportunity portion of the savings is presented further on in this measure. To obtain the lifetime savings, the following formula should be used:

$$LKWH_{C, Total} = AKWH_{C, Retire} \times RUL + AKWH_{C, Lost Opp} \times EUL$$

Early Retirement component:

$$AKWH_{H,Retire} = EFLH_{H} \times CAP_{H,i} \times \left(\frac{1}{HSPF_{e}} - \frac{1}{HSPF_{b}}\right) \times \frac{1}{1000W_{kW}}$$

The equation simplifies when the existing HSPF is not known:

$$AKWH_{H,Retire} = 1307 \frac{hrs}{yr} \times CAP_{H,i} \times \left(\frac{1}{6.8} - \frac{1}{7.7}\right) \times \frac{1}{1000 \frac{W}{kW}} = 0.02247 \times CAP_{H,i}$$

Cooling: If the unit also provides cooling, calculate savings as presented in Central AC measure (4.2.1).

Retrofit Gross Energy Savings, Example

A new air source heat pump with both heating and cooling capacity of 36,000 BTU/hr, HSPF_i of 9.00, SEER of 15.50, and EER of 13.0 is installed in a home to replace an old working heat pump with heating capacity of 36,000 BTU/hr, and HSPF_e of 6.

To calculate the lost opportunity component for heating, use the equation from "Lost Opportunity":

$$AKWH_{H, Lost Opp} = EFLH_{H} \times CAP_{H,i} \times \left(\frac{1}{HSPF_{b}} - \frac{1}{HSPF_{i}}\right) \times \frac{1}{1000}$$

Input the HSPF and heating capacity of the new heat pump:

$$AKWH_{H, Lost Opp} = 1307 \ hrs \times 36,000 \ {}^{Btu}/_{hr} \times \left(\frac{1}{7.7} - \frac{1}{9.0}\right) \times \frac{1}{1000} = 883 \ kWh$$

Because the existing unit is verified to be in working condition, use the Retirement equation to calculate annual Retirement savings, using the capacity of the new unit and HSPF of the existing unit.

$$AKWH_{H, Re tire} = EFLH_{H} \times CAP_{H,i} \times \left(\frac{1}{HSPF_{e}} - \frac{1}{HSPF_{b}}\right) \times \frac{1}{1000W_{kW}}$$

$$AKWH_{H, Re tire} = 1307 \frac{hrs}{yr} \times 36,000 \frac{Btu}{hr} \times \left(\frac{1}{6} - \frac{1}{7.7}\right) \times \frac{1}{1000W_{kW}} = 1,731 kWh$$

Because the HP also provides cooling, calculate cooling savings as presented in the Central AC measure (4.2.1).

Retrofit Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

Heating: WKW= 0; Note [4]

Cooling: If the unit also provides cooling, calculate demand savings as presented in Central AC measure (4.2.1).

Lost Opportunity Gross Energy Savings, Electric

$$AKWH_{H,Lost\ Opp} = EFLH_{H} \times CAP_{i} \times \left(\frac{1}{HSPF_{b}} - \frac{1}{HSPF_{i}}\right) \times \frac{1}{1000}$$

$$AKWH_{H,Lost\ Opp} = 1307 \, \frac{hrs}{yr} \times CAP_{i} \times \left(\frac{1}{7.7} - \frac{1}{HSPF_{i}}\right) \times \frac{1}{1000}$$

Cooling: If the unit also provides cooling, calculate savings as presented in Central AC measure (4.2.1).

Lost Opportunity Gross Energy Savings, Example

A rebate is provided for the installation of a new air source heat pump with an installed cooling capacity of 36,000 BTU/hr and HSPF of 9. What are the annual electric heating and cooling savings?

Using the Lost Opportunity equation, input the capacity and HSPF of the new unit:

$$AKWH_{H,Lost\ Opp} = 1307 \frac{hrs}{y_r} \times CAP_i \times \left(\frac{1}{7.7} - \frac{1}{HSPF_i}\right) \times \frac{1}{1000}$$

$$AKWH_{H,Lost\ Opp} = 1307 \frac{hrs}{y_r} \times 36,000 \frac{Btu}{hr} \times \left(\frac{1}{7.7} - \frac{1}{9}\right) \times \frac{1}{1000} = 883 \ kWh$$

Lost Opportunity Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

Heating: WKW= 0; Note [4]

Cooling: If the unit also provides cooling, calculate demand savings as presented in Central AC measure (4.2.1).

Changes from Last Version

The presentation of retirement savings has been refreshed. Retrofit measure is more clearly presented as two-part savings that may be added together if qualified. Added equations for Lost Opportunity section consistent with previous methodology. Provided reference for EFLH calculation. Additional examples were added.

References

- [1] Residential Central AC Regional Evaluation, ADM Associates, Inc., November 2009, page 4-1.
- [2] National Climatic Data Center, Divisional Data Select, http://www7.ncdc.noaa.gov/CDO/CDODivisionalSelect.jsp
- [3] 1989 ASHRAE Fundamentals, Chapter 28: Energy Estimating Methods, page 28.2 Fig. 1: Correction Factor versus Degree-Days
- [4] 1989 ASHRAE Fundamentals, 24.6 Table 1: Climatic Conditions for the United States: Connecticut: Hartford, Brainard Field.
- [5] McQuiston, Faye C.; Jerald D. Parker; Jeffrey D. Spitler. Heating, Ventilating, and Air Conditioning: Analysis and Design, Fifth Edition, Chapter 7: Space Heating Load, page 192. ISBN 0-471-35098-2.

Notes

- [1] The federal minimum standard for heat pumps is HSPF 7.7, as of Jan 23, 2006
- [2] In 1992, the federal government established the minimum heating efficiency standard for new heat pumps at 6.8 HSPF.
- [3] Equivalent Full Load Hours estimated as follows:

$$EFLH_{H} = \left(\frac{24 \times HDD \times AF}{T_{OC} - T_{IC}}\right) = \left(\frac{24 \times 5885 \times 0.62}{70^{\circ}F - 3^{\circ}F}\right) = 1307 \frac{hours}{yr}$$

Where

24 = conversion between degree-days to degree-hours

HDD = 5885 = 30-year average annual degree days, data from Ref [2] for CT, Jan 1979 to Dec 2008

AF = 0.62 = ASHRAE degree day correction factor to account for occupant behavior from Ref [3]

 $T_{OC} = 3^{\circ} F$ = outdoor heating design temperature for Hartford, Brainard Field at 99% level from Ref [4]

 $T_{OC} = 70^{\circ} F = \text{indoor heating design temperature, Ref [5]}$

[4] WKW = 0; Demand savings are not claimed for this measure since backup resistance heat on the heat pump would most likely be used during winter seasonal peak periods

4.2.3 GEOTHERMAL HEAT PUMP

Description of Measure

Version Date: 10/30/2012

Installation and commissioning of a high efficiency closed loop or Buried DX Geothermal Heat Pump system.

Savings Methodology

Savings are determined using the results of "HVAC Systems in an ENERGY STAR Home: Owning & Operating Costs (Update 2008)" (Reference [1]) as a basis for the calculation. The report analyzed the annual consumption of geothermal heat pumps. To calculate savings for this measure, the results from the study are adjusted based on size (in tons) and efficiencies (COP and EER). Note: the savings baseline is an ENERGY STAR Tier 1 geothermal system.

Inputs

| Symbol | Description | Units |
|------------------|---|-------------|
| | Type of Geothermal system (closed loop/DX) Water to water or Water to air | |
| CAPi | Installed Cooling Capacity | Tons |
| EER _i | EER - Installed | Btu/Watt-hr |
| COPi | COP - Installed | |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|------------------|--|-------------|---------|--------------------|
| AH_{CDH} | Annual heating energy usage per ton | kWh/ton/yr | | Ref [1] |
| AH_b | Annual heating energy usage, Baseline | kWh/yr | | |
| AH_i | Annual heating energy usage, Installed | kWh/yr | | |
| AC_{CDH} | Annual cooling energy usage per ton | kWh/ton/yr | | Ref [1] |
| AC_b | Annual cooling energy usage, Baseline | kWh/yr | | |
| AC_i | Annual cooling energy usage, Installed | kWh/yr | | |
| CAP_i | Installed Cooling Capacity in Tons | Tons | | Input |
| CF_C | Coincidence Factor, residential cooling | | | Appendix 1 |
| CF_H | Coincidence Factor, residential heating | | | Appendix 1 |
| COP_b | COP - Baseline | | Table 1 | ENERGY STAR Tier 3 |
| COP_{CDH} | EER used to model consumption in the CDH study | | 3.9 | Ref [1] |
| COP_i | COP - Installed | | | Input |
| EER_{CDH} | EER used to model consumption in the CDH study | Btu/Watt-hr | 17.2 | Ref [1] |
| EER _b | EER - Baseline | Btu/Watt-hr | Table 1 | ENERGY STAR Tier 1 |
| EER _i | EER - Installed | Btu/Watt-hr | | Input |
| SKW_C | Summer Seasonal Demand Savings | kW | | |
| SKW_{CDH} | Summer kW per ton | kW/ton | | Ref [1] |
| WKW _H | Winter Seasonal Demand Savings | kW | | |

Lost Opportunity Gross Energy Savings, Electric

The annual consumption per ton and efficiencies per cooling capacity (tons) are as follows (Ref [1]):

 $AH_{CDH} = 1,569 \text{ kWh/Ton at } 3.9 \text{ COP}$ $AC_{CDH} = 326 \text{ kWh/ton at } 17.2 \text{ EER}$

 $SKW_{CDH} = 0.71 \text{ kW/ton}$

Table 1: Baseline Efficiencies (ENERGY STAR Tier 1) Reference [2]

| System Type | EER _b | COP _b |
|----------------------------|------------------|------------------|
| Closed Loop Water to Air | 14.1 | 3.3 |
| Closed Loop Water to Water | 15.1 | 3.0 |
| DGX | 15.0 | 3.5 |

$$AKWH_{C} = (AC_{b} - AC_{i})$$

$$AKWH_{C} = CAP_{i} \times AC_{CDH} \times \left(\frac{EER_{CDH}}{EER_{b}} - \frac{EER_{CDH}}{EER_{i}}\right)$$

$$AKWH_{C} = CAP_{i} \times 326 \times \left(\frac{17.2}{EER_{b}} - \frac{17.2}{EER_{i}}\right)$$

$$AKWH_{H} = (AH_{b} - AH_{i})$$

$$AKWH_{H} = CAP_{i} \times AH_{CDH} \times \left(\frac{COP_{CDH}}{COP_{b}} - \frac{COP_{CDH}}{COP_{i}}\right)$$

$$AKWH_{H} = CAP_{i} \times 1,569 \times \left(\frac{3.9}{COP_{b}} - \frac{3.9}{COP_{i}}\right)$$

$$AKWH = AKWH_C + AKWH_H$$

Lost Opportunity Gross Energy Savings, Example

A 3 ton closed loop geothermal heat pump is installed with an EER of 20.2 and COP of 4.2. What are the energy savings?

$$AKWH_{C} = CAP_{i} \times AC_{CDH} \times \left(\frac{EER_{CDH}}{EER_{b}} - \frac{EER_{CDH}}{EER_{i}}\right)$$

$$AKWH_{c} = 3 \times 326 \times \left(\frac{17.2}{14.1} - \frac{17.2}{20.2}\right) = 360kWh$$

$$AKWH_{H} = 3 \times 1,569 \times \left(\frac{3.9}{3.3} - \frac{3.9}{4.2}\right) = 1,192kWh$$

$$AKWH = 360 + 1{,}192 = 1{,}552kWh$$

Lost Opportunity Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

$$SKW_C = CAP_i \times SKW_{CDH} \times \left(\frac{EER_{CDH}}{EER_b} - \frac{EER_{CDH}}{EER_i}\right) \times CF_C$$

$$SKW_C = CAP_i \times 0.71 \times \left(\frac{17.2}{EER_b} - \frac{17.2}{EER_i}\right) \times CF_C$$

$$WKW_{H} = CAP_{i} \times \left(\frac{12,000Btus}{Ton}\right) \times \left(\frac{kW}{3,412Btus}\right) \times \left(\frac{1}{COP_{b}} - \frac{1}{COP_{i}}\right) \times CF_{H}$$

References

- [1] HVAC Systems in an ENERGY STAR Home: Owning & Operating Costs (Update 2008), CDH Energy Corp, 2008, Tables 3 and 4.
- [2] ENERGY STAR Tier 1 Geothermal Heat Pumps Key Product Criteria. http://www.energystar.gov/index.cfm?c=geo_heat.pr_crit_geo_heat_pumps. Last accessed on June 20, 2012.

4.2.6 ELECTRONICALLY COMMUTATED MOTOR

Description of Measure

Version Date: 10/30/2012

Installation of an electronically commutated motor (ECM) or brushless permanent magnet motor (BPM) when installed as part of a new high efficiency HVAC system or as a new ECM replacement on an existing HVAC system.

Savings Methodology

Savings for this measure are calculated based on a typical home. The savings are based on the metering study "Electricity Use by New Furnaces – A Wisconsin Field Study, Energy Center of Wisconsin," Ref [1], which compared actual furnace fan annual consumption of units with ECMs to units with permanent split capacitor motors. The annual savings (kWh) of the Wisconsin-based study were adjusted to Connecticut by applying the appropriate cooling degree day (CDD) and heating degree day (HDD) adjustments. The study identified small amount of standby losses from the ECM controls. These losses were allocated proportionally to heating and cooling savings before the results were adjusted for Connecticut. Because reducing the fan energy increases heating and reduces cooling energy usage, the calculation also quantifies interactive effects.

Inputs

| Symbol | Description | Units |
|--------|--|-------|
| | Number of systems with ECMs installed. | |
| | Heating fuel type | |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|-----------|--|--------|---------|----------|
| $ABTU_H$ | Annual BTU Savings | Btu/yr | | |
| ACCF | Annual natural gas savings | Ccf/yr | | |
| AFUE | Annual Fuel Utilization Efficiency | % | 90% | Note [4] |
| $AKWH_H$ | Annual Electric Energy Savings during heating season | kWh/yr | | |
| AKWHc | Annual Electric Energy Savings during cooling season | kWh/yr | | |
| AOG | Annual oil savings | Gal/yr | | |
| APG | Annual propane savings | Gal/yr | | |
| CDD | Cooling Degree Days for CT | | 603 | Note [2] |
| CF_C | Coincidence Factor cooling | | 0.75 | |
| CF_H | Coincidence Factor heating | | 0.50 | |
| HDD | Heating Degree Days for CT | | 5,885 | Note [2] |
| PD_{H} | Peak Day heating savings | Ccf | | |
| PDF_{H} | Peak Day factor heating | | 0.00977 | |
| PkW_C | kW savings – Cooling mode | kW | 0.16 | Ref [1] |
| PkW_H | kW savings –Heating mode | kW | 0.18 | Ref [1] |
| SEER | Seasonal Energy Efficiency Ratio | | 15 | Note [4] |
| SKW | Summer Demand Savings | kW | | |
| WCS | Electric energy savings for Wisconsin during cooling season. | kWh | 65 | Note [1] |
| WHS | Electric energy savings for Wisconsin during heating season. | kWh | 375 | Note [1] |
| WICDD | Cooling Degree Days for WI | | 524 | Note [3] |
| WIHDD | Heating Degree Days for WI | | 7,521 | Note [3] |
| WKW | Winter Demand Savings | kW | | |

Lost Opportunity Gross Energy Savings, Electric

Version Date: 10/30/2012

$$AKWH_{H} = WHS \times \left(\frac{HDD}{WIHDD}\right)$$

 $AKWH_{H} = 375 \times \left(\frac{5,885}{7,521}\right) = 293 \, kWh$

$$AKWH_{C} = WCS \times \left(\frac{CDD}{WICDD}\right) \times \left(1 + \frac{3.412}{SEER}\right)$$
$$AKWH_{C} = 65 \times \left(\frac{603}{524}\right) \times \left(1 + \frac{3.412}{15}\right) = 92 \ kWh$$

Lost Opportunity Gross Energy Savings, Fossil Fuel

Interactive savings are from the reduction of fan energy. They are negative since they increase the heating consumption.

$$ABTU_{H} = -AKWH_{H} \times \frac{3,412Btu/kWh}{AFUE}$$

$$ABTU_{H} = -293 \times \frac{3,412Btu/kWh}{0.9} = -1,110,796Btu$$

Savings by fuel type:

$$\begin{split} ACCF_{H} &= \frac{ABTU_{H}}{102,900Btu/ccf} = \frac{-1,110,796}{102,900Btu/ccf} = -10.8ccf \\ AOG_{H} &= \frac{ABTU_{H}}{138,690Btu/Gal} = \frac{-1,110,796}{138,690Btu/Gal} = -8.0Gal \\ APG_{H} &= \frac{ABTU_{H}}{91,330Btu/Gal} = \frac{-1,110,796}{91,330Btu/Gal} = -12.2Gal \end{split}$$

Lost Opportunity Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

$$WKW_{H} = PkW_{H} \times CF_{H}$$

$$WKW_{H} = 0.18 \times 0.50 = 0.09kW$$

$$SKW_{C} = PkW_{C} \times CF_{C}$$

$$SKW_{C} = 0.16 \times 0.75 = 0.12kW$$

Lost Opportunity Gross Peak Day Savings, Natural Gas

$$PD_{H} = ACCF \times PDF_{H}$$

$$PD_{H} = -10.8 \times 0.00977 = -0.106ccf$$

Changes from Last Version

Heating fuel type now listed as input.

References

Version Date: 10/30/2012

[1] Electricity Use by New Furnaces – A Wisconsin Field Study, Energy Center of Wisconsin, October 2003.

Notes

- [1] The Wisconsin study savings while heating (400 kWh, page 9), Cooling (70 kWh, page 10) and Standby losses of (30 kWh, page 11). The standby losses were allocated to heating (25 kWh) and cooling (5 kWh) before the values were adjusted based on CT.
- [2] Degree Day data from the National Climatic Data Center, Divisional Data, CT state, Jan 1979 to Dec 2008, 30 year average. http://www7.ncdc.noaa.gov/CDO/CDODivisionalSelect.jsp
- [3] Degree Day data from the National Climatic Data Center, Divisional Data, WI state, Jan 1979 to Dec 2008, 30 year average. http://www7.ncdc.noaa.gov/CDO/CDODivisionalSelect.jsp
- [4] The efficiencies assumed on an average qualifying unit's efficiency.

4.2.9 DUCT SEALING

Description of Measure

Duct sealing to improve efficiency of air distribution from HVAC systems. Savings are verified by measuring outside duct leakage at 25 Pascal using standard duct blaster testing procedures and blower door; other advanced sealing techniques can be used to achieve 2009 IECC duct sealing requirements.

Savings Methodology

Duct improvements (sealing) should be verified with duct blaster test at 25 Pa using an approved test method. Note that a blower door is required as part of this test to maintain 25 Pa in the house in order to isolate duct leakage to the outside. Alternative test methods (i.e. subtraction method, flow hood method, delta Q, etc) will generally yield inconsistent results and therefore are not permitted. Duct infiltration reduction was simulated using REM/Rate, a residential energy analysis and rating software (Ref [1]).

Advanced Duct Sealing (ADS) is a special case of duct sealing that satisfies IECC 2009 requirements of 8 CFM per 100 square feet of heated space, air flow to the outside (Ref [3]). One of the methods approved in IECC 2009 for verification of performance must be used following ADS and documented well (See Notes [1], [2]).

Reminder: Heating savings may not be claimed if ducts are not used for heating distribution. For instance, a home with electric baseboard resistance heating or a fossil fuel boiler which has ducts used only for the Central Air Conditioner may only claim cooling savings.

Inputs

| Symbol | Description |
|---------------------|---|
| A | Heated area served by system (required only for ADS measures) |
| CFM_{Pre} | Verified air flow rate at 25 Pa before duct sealing |
| CFM _{Post} | Verified air flow rate after duct sealing at 25 Pa (not required for ADS savings) |
| | Heating Fuel Type (Electric Resistive, HP, Gas, Oil, Propane, etc) |
| | Heating System Distribution Type (Forced air with fan, heat pump, resistive, radiator, etc) |

<u>Nomenclature</u>

| Symbol | Description | Units | Values | Comments |
|--------------|--|---------|---------|------------|
| A | Heated area served by system | Sq ft | Actual | |
| ACCF | Annual Natural Gas Savings | Ccf/yr | | |
| $AKWH_H$ | Annual Electric Energy Savings, Heating | kWh/yr | | |
| $AKWH_C$ | Annual Electric Energy Savings, Cooling | kWh/yr | | |
| AOG | Annual Oil Savings | Gal/yr | | |
| APG | Annual Propane Savings | Gal/yr | | |
| CFM_{Pre} | Air flow rate before duct sealing at 25Pa | CFM | Actual | Note [1] |
| CFM_{Post} | Air flow rate after duct sealing at 25 Pa | CFM | Actual | Note [2] |
| SKW | Summer Demand Savings | kW | | |
| WKW | Winter Demand Savings | kW | | |
| PD_{H} | Natural gas peak day savings - heating | Ccf | | |
| PDF_{H} | Natural gas peak day factor -heating | | 0.00977 | Appendix 1 |
| REM | Savings modeled using Residential Energy Modeling software | per cfm | | Ref [1] |

Retrofit Gross Energy Savings, Electric

Table 1: Electric Duct Blaster Savings, kWh per CFM Reduction at 25 Pa (Note [3])

| | REM _{Heating} for Heating | | | REM _{AH} | REM _{Cooling} |
|---------------------------|------------------------------------|-------|------------|-------------------|------------------------|
| | Electric Heat | | | Heating Fan | Central AC |
| | Forced Air | Pumps | Geothermal | (Note [3]) | Cooling |
| Savings per CFM Reduction | 7.693 | 3.847 | 2.564 | 1.100 | 1.059 |

For Electric (Forced Air), Heat Pump or Geothermal Heating Systems,

$$AKWH_H = REM_{Heating} \times (CFM_{Pre} - CFM_{Post})$$

For Fossil Fuel heating with air handler unit,

$$AKWH_H = REM_{AH} \times (CFM_{Pre} - CFM_{Post})$$

Home with Central AC,

$$AKWH_{H} = REM_{Cooling} \times (CFM_{Pre} - CFM_{Post})$$

Retrofit Gross Energy Savings, Fossil Fuel

Table 2: Fossil Fuel Duct Blaster Savings per CFM Reduction at 25 Pa (Note [4])

| | Heating | Gallons Oil – | Natural Gas – Ccf | Gallons Propane – Gallons |
|---------------------------|---------|---------------------------------------|----------------------|---------------------------|
| | (MMBtu) | Gallons (REM _{Oil}) | (REM _{NG}) | (REM _{Propane}) |
| Savings per CFM Reduction | 0.035 | 0.252 | 0.340 | 0.383 |

For homes with natural gas heating system,

$$ACCF_H = REM_{NG} \times (CFM_{Pre} - CFM_{Post})$$

For homes with oil heating system,

$$AOG_H = REM_{Oil} \times (CFM_{Pre} - CFM_{Post})$$

For homes with propane heating system,

$$APG_H = REM_{\text{Pr}opane} \times (CFM_{\text{Pr}e} - CFM_{Post})$$

Retrofit Gross Energy Savings, Example

Duct sealing at 25 Pa was performed in a 2400 sq ft 1960's ranch style home in Hartford. The home is primarily heated by a natural gas furnace and cooled by Central AC. The outside duct leakage readings at 25 Pa showed CFM_{Pre} of 850 and CFM_{Post} of 775. What are the energy savings for this home?

This home has fossil fuel, air handler (fan), and cooling savings.

Using the equation for gas heating savings:

$$ACCF_{H} = REM_{NG} \times (CFM_{Pre} - CFM_{Post})$$
$$ACCF_{H} = 0.340 \times (850 - 775)$$
$$ACCF_{H} = 25.5 Ccf$$

Using the equation for electric heating fan savings,

$$AKWH_{H} = REM_{AH} \times (CFM_{Pre} - CFM_{Post})$$
$$AKWH_{H} = 1.100 \times (850 - 775)$$

$$AKWH_{H} = 82.5 \, kWh$$

Using the equation for Central AC savings,

$$AKWH_{C} = REM_{Cooling} \times (CFM_{Pre} - CFM_{Post})$$

$$AKWH_C = 1.059 \times (850 - 775)$$

$$AKWH_C = 79.4 \, kWh$$

Retrofit Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

Table 3: Electric Duct Blaster Savings, kW per CFM Reduction at 25 Pa (Note [3])

| | REM _{WKW} fo | REM _{WKW} for Heating | | | |
|---------------------------|-----------------------|--------------------------------|------------|------------|------------|
| | Electric | Heat | | Everything | Central AC |
| | Forced Air | Pump | Geothermal | Else | Cooling |
| Savings per CFM Reduction | 0.0158 | 0.0158 | 0.0053 | 0 | 0.0023 |

$$WKW_{H} = REM_{WKW} \times (CFM_{Pre} - CFM_{Post})$$

$$SKW_{C} = REM_{SKW} \times (CFM_{Pre} - CFM_{Post})$$

Reminder: Demand savings are based on design load calculation in REM software; there is no need to use coincidence factors

Retrofit Gross Seasonal Peak Demand Savings, Natural Gas

$$PD_H = ACCF_H \times PDF_H$$

Retrofit Gross Peak Demand Savings, Example

Duct sealing at 25 Pa was performed in a 2400 sq ft 1960's ranch style home in Hartford. The home is primarily heated by heat pump and cooled by Central AC. The outside duct leakage readings at 25 Pa showed CFM_{Pre} of 850 and CFM_{Post} of 775. What are the peak demand savings for this home?

Using the equation for heat pump winter demand (REM_{WKW} = 0.0158 kW per CFM),

$$WKW_H = REM_{WKW} \times (CFM_{Pre} - CFM_{Post})$$

$$WKW_H = 0.0158 \times (850 - 775)$$

$$WKW_{H} = 1.19 \, kW$$

Using the equation for summer demand savings (REM_{SKW} = 0.0023 kW per CFM),

$$SKW_C = REM_{SKW} \times (CFM_{Pre} - CFM_{Post})$$

$$SKW_C = 0.0023 \times (850 - 775)$$

$$SKW_{c} = 0.173 \, kW$$

If the home in this example has a Natural Gas furnace instead of a heat pump, what are the natural gas peak day savings?

Using the formula for Peak Day Natural Gas,

$$PD_{H} = ACCF_{H} \times PDF_{H}$$

$$PD_H = 25.5 \times 0.00977 = 0.249 \ Ccf$$

$$PD_{H} = 0.249 \ Ccf$$

Changes from Last Version

In Table 2, changed the REM_{Oil} from 0.250 to 0.252, REM_{Gas} from 0.359 to 0.340

References

- [1] REM/Rate™ version 12.99 is a residential energy analysis, code compliance and rating software developed by Architectural Energy Corporation. This software calculates heating, cooling, hot water, lighting, and appliance energy loads, consumption and costs for new and existing single and multi-family homes. Duct blaster energy savings analysis using REM was performed by C&LM Planning team, Northeast Utilities & United Illuminating, August 2010
- [2] Residential Central AC Regional Evaluation, ADM Associates, Inc., Final Report, November 2009.
- [3] 2009 IEEC 403.2.2 Duct sealing. pages 30 & 31 ISBN978-1-5800-742-8

Notes

- [1] If the duct leakage to the outside has been measured and verified prior to performing ADS (such as CFM_{post} from a recent duct blaster test), this value shall be used for CFM_{pre}. If this value is not available, use the following: $CFM_{pre} = 0.195 \frac{CFM}{sqft} \times A$, based on the average CFM_{pre} from all Home Energy Solutions duct sealing projects in 2011.
- [2] Actual measured air flow CFM to outside shall be used for CFM_{post} whenever possible. In the case of ADS, if air flow to the outside is unavailable but the 2009 IECC specification has been met, CFM_{post} may be calculated based on the heated area served by the system: $CFM_{post} = 0.080 \frac{CFM}{saft} \times A$
- [3] Fan energy savings are only to be captured for forced-air systems with an air handling unit (fan).
- [4] Fossil fuel savings include estimated expected system efficiency of 75% including combustion and distribution.

4.2.12 HEAT PUMP - DUCTLESS

Description of Measure

Version Date: 10/30/2012

Installation of energy efficient Ductless Heat Pump or Mini-Split Heat Pump.

Savings Methodology

Savings methodology is based on the impact evaluation of Ductless Heat Pump (DHP) pilot performed by KEMA (Ref [1]) Energy savings for DHP are determined using savings factors from the pilot study adjusted for installed efficiencies or by performing a custom analysis such as DOE-2 or Billing analysis [PRISM] (Note [2] & [3]) for a specific project. If a custom analysis is done, the savings will be capped at 50% of the heating portion of the billing history. Heating savings are calculated on the basis of either Hartford or Bridgeport climate data. Savings for actual projects are calculated using the closest location on heating degree-day (HDD) basis.

DHP installed in an existing home with Electric Resistive heating system is considered to have Retrofit savings. DHP installed in a home with fossil fuel heating system is considered to have Lost Opportunity savings (or new construction).

Note: The savings here are not to be applied to a heat pump with ducting. Only systems without ducts are addressed by this measure.

Inputs

| Symbol | Description | |
|-----------------------------------|--|--|
| $HSPF_{I}$ | Heating Season Performance Factor, Installed | |
| SEERI | Seasonal Energy Efficiency Ratio, Installed | |
| CAP_C | Cooling Capacity | |
| CAP _H Heating capacity | | |
| | Primary existing heating fuel type | |

Nomenclature

| Symbol | Description | Units | Value | Comments |
|----------------------------|--|--------------|------------------------|------------|
| 1 Ton | Capacity, Tonnage | Tons | 12,000 Btu/hr | Unit |
| | | | | conversion |
| AA_C | Hartford kWh cooling savings factor from pilot | kWh/1000 Btu | 3.1 | Ref [1] |
| AA_H | Hartford kWh heating savings factor from pilot | kWh/1000 Btu | 130 | Ref [1] |
| AKWH | Annual Electric Energy Savings | kWh | | |
| BB_C | Hartford kW cooling savings factor from pilot | kW/1000 Btu | 0.0017 | Ref [1] |
| BB_H | Hartford kW heating savings factor from pilot | kW/1000 Btu | 0.019 | Ref [1] |
| CAP_C | Nominal Cooling Capacity | Btu/hr | | Input |
| CAP_H | Nominal Heating capacity | Btu/hr | | Input |
| CC_C | Bridgeport kWh cooling savings factor from pilot | kWh/1000 Btu | 3.2 | Ref [1] |
| CC _H | Bridgeport kWh heating savings factor from pilot | kWh/1000 Btu | 140 | Ref [1] |
| DD_{C} | Bridgeport kW cooling savings factor from pilot | kW/1000 Btu | 0.0014 | Ref [1] |
| DD_{H} | Bridgeport kW heating savings factor from pilot | kW/1000 Btu | 0.032 | Ref [1] |
| EE _C | Efficiency conversion factor, cooling | | 0.037 | Ref [1] |
| EE _H | Efficiency conversion factor, heating | | 0.171 | Ref [1] |
| HSPF _B | Heating Season Performance Factor, Baseline | Btu/Watt-hr | 7.7 – Lost Opportunity | Note [1] |
| HSPF _E | Heating Season Performance Factor, Existing | Btu/Watt-hr | 3.4 – Retrofit | Note [1] |
| HSPF _I | Heating Season Performance Factor, Installed | Btu/Watt-hr | | Input |
| SEER _B | Seasonal Energy Efficiency Ratio, Baseline | Btu/Watt-hr | 13.0 – Lost | Note [1] |
| | | | Opportunity | |

| Symbol | Description | Units | Value | Comments |
|-------------------|---|-------------|-----------------|----------|
| SEER _E | Seasonal Energy Efficiency Ratio, Existing | Btu/Watt-hr | 10.1 – Retrofit | Note [1] |
| SEERI | Seasonal Energy Efficiency Ratio, Installed | Btu/Watt-hr | | Input |
| SKW | Summer Demand Savings | kW | | |
| WKW | Winter Demand Savings | kW | | |

Retrofit Gross Energy Savings, Electric

Version Date: 10/30/2012

Heating

For Hartford:
$$AKWH_H = CAP_H \times \left(\frac{1}{HSPF_E} - \frac{1}{HSPF_L}\right) \times \frac{1}{EE_H} \times AA_H \times \frac{1}{1000}$$

For Bridgeport:
$$AKWH_H = CAP_H \times \left(\frac{1}{HSPF_E} - \frac{1}{HSPF_I}\right) \times \frac{1}{EE_H} \times CC_H \times \frac{1}{1000}$$

Cooling

For Hartford:
$$AKWH_C = CAP_C \times \left(\frac{1}{SEER_E} - \frac{1}{SEER_L}\right) \times \frac{1}{EE_C} \times AA_C \times \frac{1}{1000}$$

For Bridgeport:
$$AKWH_C = CAP_C \times \left(\frac{1}{SEER_E} - \frac{1}{SEER_I}\right) \times \frac{1}{EE_C} \times CC_C \times \frac{1}{1000}$$

Retrofit Gross Energy Savings, Example

A high energy efficient ductless heat pump (DHP) is installed in an existing home with electric resistance heat in Hartford. The nominal heating capacity is 24,000 BTU, and the nominal cooling capacity is 28,000 BTU, installed HSPF is 11 and the installed SEER is 22. What are the annual electric heating and cooling savings?

Using the equation for annual electric heating savings,

$$AKWH_{H} = CAP_{H} \times \left(\frac{1}{HSPF_{E}} - \frac{1}{HSPF_{I}}\right) \times \frac{1}{EE_{H}} \times AA_{H} \times \frac{1}{1000}$$

$$AKWH_{H} = 24,000 \times \left(\frac{1}{3.413} - \frac{1}{11}\right) \times \frac{1}{0.171} \times 130 \times \frac{1}{1000} = 3,687 \text{ kWh}$$

Using the equation for annual electric cooling savings,

$$AKWH_{C} = CAP_{C} \times \left(\frac{1}{SEER_{E}} - \frac{1}{SEER_{I}}\right) \times \frac{1}{EE_{C}} \times AA_{C} \times \frac{1}{1000}$$

$$AKWH_{C} = 28,000 \times \left(\frac{1}{10.1} - \frac{1}{22}\right) \times \frac{1}{0.037} \times 3.1 \times \frac{1}{1000} = 126 \text{ kWh}$$

Retrofit Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

Winter Demand Savings:

For Hartford:
$$WKW = CAP_H \times \left(\frac{1}{HSPF_E} - \frac{1}{HSPF_L}\right) \times \frac{1}{EE_H} \times BB_H \times \frac{1}{1000}$$

For Bridgeport:
$$WKW = CAP_H \times \left(\frac{1}{HSPF_E} - \frac{1}{HSPF_I}\right) \times \frac{1}{EE_H} \times DD_H \times \frac{1}{1000}$$

Summer Demand Savings:

For Hartford:
$$SKW = CAP_C \times \left(\frac{1}{SEER_E} - \frac{1}{SEER_I}\right) \times \frac{1}{EE_C} \times BB_C \times \frac{1}{1000}$$

For Bridgeport:
$$SKW = CAP_C \times \left(\frac{1}{SEER_E} - \frac{1}{SEER_I}\right) \times \frac{1}{EE_C} \times DD_C \times \frac{1}{1000}$$

Retrofit Gross Peak Demand Savings, Example

A high energy efficient ductless heat pump (DHP) is installed in an existing home with electric resistive heat in Hartford. The rated heating capacity is 24,000 BTU, rated cooling capacity is 28,000 BTU, installed HSPF is 11 and the installed SEER is 22. What are the annual summer and winter demand savings?

Using the equation for summer demand savings,

$$SKW = CAP_{C} \times \left(\frac{1}{SEER_{E}} - \frac{1}{SEER_{I}}\right) \times \frac{1}{EE_{C}} \times BB_{C} \times \frac{1}{1000}$$

$$SKW = 28,000 \times \left(\frac{1}{10.1} - \frac{1}{22}\right) \times \frac{1}{0.037} \times 0.0017 \times \frac{1}{1000} = 0.069 \ kW$$

Using the equation for winter demand savings,

$$WKW = CAP_{H} \times \left(\frac{1}{HSPF_{E}} - \frac{1}{HSPF_{I}}\right) \times \frac{1}{EE_{H}} \times BB_{H} \times \frac{1}{1000}$$

$$WKW = 24,000 \times \left(\frac{1}{3.413} - \frac{1}{11}\right) \times \frac{1}{0.171} \times 0.019 \times \frac{1}{1000} = 0.539 \text{ kW}$$

Lost Opportunity Gross Energy Savings, Electric

Heating

For Hartford:
$$AKWH_H = CAP_H \times \left(\frac{1}{HSPF_B} - \frac{1}{HSPF_I}\right) \times \frac{1}{EE_H} \times AA_H \times \frac{1}{1000}$$

For Bridgeport:
$$AKWH_H = CAP_H \times \left(\frac{1}{HSPF_R} - \frac{1}{HSPF_I}\right) \times \frac{1}{EE_H} \times CC_H \times \frac{1}{1000}$$

Cooling

For Hartford:
$$AKWH_C = CAP_C \times \left(\frac{1}{SEER_B} - \frac{1}{SEER_I}\right) \times \frac{1}{EE_C} \times AA_C \times \frac{1}{1000}$$

For Bridgeport:
$$AKWH_C = CAP_C \times \left(\frac{1}{SEER_B} - \frac{1}{SEER_I}\right) \times \frac{1}{EE_C} \times CC_C \times \frac{1}{1000}$$

Lost Opportunity Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

Winter Demand Savings:

For Hartford:
$$WKW = CAP_H \times \left(\frac{1}{HSPF_B} - \frac{1}{HSPF_I}\right) \times \frac{1}{EE_H} \times BB_H \times \frac{1}{1000}$$

For Bridgeport:
$$WKW = CAP_H \times \left(\frac{1}{HSPF_B} - \frac{1}{HSPF_I}\right) \times \frac{1}{EE_H} \times DD_H \times \frac{1}{1000}$$

Summer Demand Savings:

For Hartford:
$$SKW = CAP_C \times \left(\frac{1}{SEER_B} - \frac{1}{SEER_L}\right) \times \frac{1}{EE_C} \times BB_C \times \frac{1}{1000}$$

For Bridgeport:
$$SKW = CAP_C \times \left(\frac{1}{SEER_B} - \frac{1}{SEER_I}\right) \times \frac{1}{EE_C} \times DD_C \times \frac{1}{1000}$$

Non Energy Benefits

Ductless Heat Pump customers have reported high levels of satisfaction. Ref [1]

Changes from Last Version

Clarified measure pertains only to non-ducted systems.

References

[1] Ductless Mini Pilot Study, Final Report, KEMA, June 2009, Pages vi, vii, 4-15 and 4-18.

Notes

- [1] The minimum heating efficiency standard, set by federal government in 2006 for ductless heat pumps is 10.1 HSPF and cooling efficiency is 13.0 SEER. The minimum efficiency standard for electric resistive heating system is 3.4 HSPF.
- [2] PRISM is an established statistical procedure for measuring energy conservation in residential housing. The PRISM software package was developed by the Center for Energy and Environmental Studies, Princeton University. The tool is used for estimating energy savings from billing data.

 http://www.princeton.edu/~marean/
- [3] DOE-2 is a widely used and accepted building energy analysis program that can predict the energy use and cost for all types of buildings. DOE-2 uses a description of the building layout, constructions, operating schedules, conditioning systems (such as lighting & HVAC) and utility rates provided by the user, along with weather data, to perform an hourly simulation of the building and to estimate utility bills. http://www.doe2.com/>

4.2.13 PACKAGE TERMINAL HEAT PUMP

Description of Measure

Version Date: 10/30/2012

Installation of new energy efficient packaged terminal heat pump

Savings Methodology

The savings methodology for a package terminal heat pump (PTHP) is calculated from baseline efficiencies in Ref [1].

Lost Opportunity Measure:

• Lost Opportunity savings are the difference in energy use between a baseline new model and the chosen high efficiency new model, continuing for the Effective Useful Life (EUL) from Appendix 4.

Retrofit Measure:

- Uses the same methodology as a Lost Opportunity measure;
- In the case of early retirement of a working unit where the unit would have otherwise been installed until failure, lifetime "Retirement" savings are claimed additional to the lifetime "Lost Opportunity" savings (see Section 1.4).
- Retirement savings are the difference in energy use between the older unit and a baseline new model, continuing for the Remaining Useful Life (RUL) from Appendix 4.

Inputs

| Symbol | Description | Units |
|--|---|-------------|
| EER _i | EER _i Energy Efficiency Ratio, Installed | |
| CAP_C | Cooling Capacity | Btu/hr |
| EER _E | Energy Efficiency Ratio, Existing | Btu/Watt-hr |
| EER _B Energy Efficiency Ratio, Base line | | Btu/Watt-hr |
| COP_B | Coefficient of Performance Base line | Btu/Watt-hr |
| COP _E Coefficient of Performance Existing | | Watt/Watt |
| COP_I | Coefficient of Performance Installed | Watt/Watt |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|-------------------|--|-------------|--------|------------|
| 1 Ton | Capacity, Tonnage | Tons | 12,000 | Unit |
| | | | Btu/hr | conversion |
| AKWH | Annual Electric Energy Savings | kWh | | |
| CAP_C | Cooling Capacity | Btu/hr | | Input |
| COP_B | Coefficient of Performance, Base line | Watt/Watt | | Ref [1] |
| COP_E | Coefficient of Performance, Existing | Watt/Watt | | Input |
| EER _B | Energy Efficiency Ratio, Baseline | Btu/Watt-hr | | Ref [1] |
| EERE | Energy Efficiency Ratio, Existing | Btu/Watt-hr | | Input |
| EER_{I} | Energy Efficiency Ratio, Installed | Btu/Watt-hr | | Input |
| EFLH _H | Heating Equivalent Full-load Hours | hours | 1307 | Ref [3] |
| HR | Percent heating when Heat pump is not in electric resistance back up | | 60% | Note[1] |
| PTHP | Packaged Heat Pump Terminal | | | |
| S_{kWh} | Average Cooling kWh Savings per unit size | kWh/Ton | 357.6 | Ref [2] |
| S_{kW} | Average Peak kW Savings per unit size | kW/Ton | 0.591 | Ref [2] |
| SA | Seasonal Efficiency Adjustment for heating | | 80% | Note[2] |
| SKW | Summer Demand Savings | kW | | |
| WKW | Winter Demand Savings | kW | 0 | Note[3] |

Retrofit Gross Energy Savings, Electric

Version Date: 10/30/2012

Heating

a) For replacement of old PTHP, use the following equations

$$AKWH_{H} = HR \times EFLH_{H} \times CAP_{C} \times \left(\frac{1}{COP_{E}} - \frac{1}{COP_{B}}\right) \times \frac{1}{3412}$$
Where, $COP_{B} = 2.9 - \left(0.026 \times CAP_{C} \times \frac{1}{1,000}\right)$

b) For replacement of electric resistive system, use the following equation

$$AKWH_{H} = HR \times EFLH_{H} \times CAP_{C} \times \left(1 - \frac{1}{SA \times COP_{B}}\right) \times \frac{1}{3412}$$

$$Where, COP_{B} = 2.9 - \left(0.026 \times CAP_{C} \times \frac{1}{1,000}\right)$$

Cooling

$$AKWH_{C} = S_{kWh} \times CAP_{C} \times \left(\frac{EER_{B}}{EER_{E}} - 1\right) \times \frac{1}{12,000}$$

$$AKWH_{C} = 357.6 \times CAP_{C} \times \left(\frac{EER_{B}}{EER_{E}} - 1\right) \times \frac{1}{12,000}$$

$$Where, EER_{B} = 10.8 - \left(0.213 \times CAP_{C} \times \frac{1}{1,000}\right)$$

Reminder: For working unit, claim additional lost opportunity savings.

Retrofit Gross Energy Savings, Example

A new Package Terminal Heat Pump with cooling capacity of 12,000Btu/hr, $EER_I=12.5$, and $COP_I=3.6$ is installed in an existing home equipped with old working PTHP with cooling capacity of 12,000 Btu/hr, $EER_E=7.8$, and $COP_E=2.5$.

Heating

$$AKWH_{H} = HR \times EFLH_{H} \times CAP_{C} \times \left(\frac{1}{COP_{E}} - \frac{1}{COP_{B}}\right) \times \frac{1}{3412}$$

$$Where, COP_{B} = 2.9 - \left(0.026 \times 12,000 \times \frac{1}{1,000}\right) = 2.59$$

$$AKWH_{H} = 0.6 \times 1307 \times 12,000 \times \left(\frac{1}{2.5} - \frac{1}{2.59}\right) \times \frac{1}{3,412} = 38.32 \ kWh$$

Cooling

$$AKWH_{C} = 357.6 \times CAP_{C} \times \left(\frac{EER_{B}}{EER_{E}} - 1\right) \times \frac{1}{12,000}$$

Where, EER_B =
$$10.8 - \left(0.213 \times \text{CAP}_{\text{C}} \times \frac{1}{1,000}\right)$$

EER_B =
$$10.8 - \left(0.213 \times 12,000 \times \frac{1}{1,000}\right) = 8.24$$

AKWH_C = 357.6×12,000×
$$\left(\frac{8.24}{7.8} - 1\right)$$
× $\frac{1}{12,000}$ = 20.17*kWh*

Reminder: For working unit, claim additional lost opportunity savings.

Retrofit Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

WKW = 0; Note [3]

$$SKW_C = S_{kW} \times CAP_C \times \left(\frac{EER_B}{EER_E} - 1\right) \times \frac{1}{12,000}$$

$$SKW_C = 0.591 \times CAP_C \times \left(\frac{EER_B}{EER_E} - 1\right) \times \frac{1}{12,000}$$

Where, EER_B =
$$10.8 - \left(0.213 \times \text{CAP}_{\text{C}} \times \frac{1}{1,000}\right)$$

Retrofit Gross Peak Demand Savings, Example

A new Package Terminal Heat Pump with cooling capacity of 1Ton/hr, $EER_I=12.5$, and $COP_I=3.6$ is installed in an existing home equipped with old working PTHP with cooling capacity of 1Ton/hr, $EER_E=7.8$, and $COP_E=2.5$.

$$WKW = 0$$

$$SKW_{C} = 0.591 \times CAP_{C} \times \left(\frac{EER_{B}}{EER_{E}} - 1\right) \times \frac{1}{12,000}$$

Where, EER_B =
$$10.8 - \left(0.213 \times 12,000 \times \frac{1}{1,000}\right) = 8.24$$

$$SKW_C = 0.591 \times 12,000 \times \left(\frac{8.24}{7.8} - 1\right) \times \frac{1}{12,000} = 0.033kW$$

Lost Opportunity Gross Energy Savings, Electric

Heating

AKWH_H = HR×EFLH_H×CAP_C×
$$\left(\frac{1}{COP_B} - \frac{1}{COP_I}\right)$$
× $\frac{1}{3412}$
Where, COP_B = 3.2 - $\left(0.026 \times CAP_C \times \frac{1}{1,000}\right)$

Cooling

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AKWH_C = 357.6×
$$CAP_C$$
 × $\left(\frac{EER_I}{EER_B} - 1\right)$ × $\frac{1}{12,000}$
Where, EER_B = 12.3 - $\left(0.213 \times CAP_C \times \frac{1}{1,000}\right)$

Lost Opportunity Gross Energy Savings, Example

A Package Terminal Heat Pump is installed in a new construction project; the cooling capacity 12,000 Btu/hr, $EER_I = 12.5$, and $COP_I = 3.6$.

Heating

$$AKWH_{H} = HR \times EFLH_{H} \times CAP_{C} \times \left(\frac{1}{COP_{B}} - \frac{1}{COP_{I}}\right) \times \frac{1}{3412}$$

$$Where, COP_{B} = 3.2 - \left(0.026 \times 12,000 \times \frac{1}{1,000}\right) = 2.88$$

$$AKWH_{H} = 0.6 \times 1307 \times 12,000 \times \left(\frac{1}{2.88} - \frac{1}{3.6}\right) \times \frac{1}{3412} = 191.5kWh$$
Cooking

Cooling

AKWH_C = 357.6×
$$CAP_C$$
 × $\left(\frac{EER_I}{EER_B} - 1\right)$ × $\frac{1}{12,000}$
Where, EER_B = 12.3 - $\left(0.213 \times 12,000 \times \frac{1}{1,000}\right)$ = 9.74
AKWH_C = 357.6×12,000× $\left(\frac{12.5}{9.74} - 1\right)$ × $\frac{1}{12,000}$ = 101.3 kWh

Lost Opportunity Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

WKW = 0

SKW_C = 0.591×
$$CAP_C$$
× $\left(\frac{EER_I}{EER_B} - 1\right)$ × $\frac{1}{12,000}$
Where, EER_B = 12.3 - $\left(0.213$ × CAP_C × $\frac{1}{1,000}\right)$

Lost Opportunity Gross Peak Demand Savings, Example

A Package Terminal Heat Pump is installed in a new construction project; the cooling capacity 12,000 Btu/hr, $EER_I = 12.5$, and $COP_I = 3.6$.

WKW = 0

$$SKW_{C} = 0.591 \times CAP_{C} \times \left(\frac{EER_{I}}{EER_{B}} - 1\right) \times \frac{1}{12,000}$$

Where, EER_B = 12.3 -
$$\left(0.213 \times \text{CAP}_{\text{C}} \times \frac{1}{1,000}\right)$$

EER_B = 12.3 - $\left(0.213 \times 12,000 \times \frac{1}{1,000}\right)$ = 9.74
SKW_C = 0.591×12,000 Btu/hr × $\left(\frac{12.5}{9.74} - 1\right) \times \frac{1}{12,000}$ = 0.167 kW

References

- [1] "Technical Support Document (TSD): Energy Efficiency Program for Commercial and Industrial Equipment: Efficiency Standards for Commercial Heating, Air Conditioning and Water heating Equipment," Table 1, Chapter 2, page 4.
- [2] Average Cooling kWh Savings per unit size = 357.6 kWh/ton, Average peak kW Savings per unit size = 0.591 kW/ton and based on "Residential Central AC Regional Evaluation, ADM Associates Inc.," Table 4-7 and table 4-8, page 4-9
- [3] EFLH_H =1,307 hours; Based on Heating degree day data (HDD) and ASHRAE adjustment factor.

Notes

- [1] HR = 60%, is Percent heating when the Heat pump is not in electric resistance back up, based on Hartford data bin analysis
- [2] SA = 80%, is COP adjustment factor for temperatures below $47^{\circ}F$, based on Hartford bin analysis
- [3] Winter demand savings are not claimed for this measure since backup resistance heat on the heat pump would most likely be used during winter seasonal peak periods

4.2.14 QUALITY INSTALLATION VERIFICATION

Description of Measure

Version Date: 10/30/2012

Perform quality installation and verification (QIV) of a residential central air ducted system as described by ENERGY STAR. Note: QIV does not apply to Ground Source Heat Pump (GSHP) and hydro air systems.

Savings Methodology

ENERGY STAR Quality Installation Guidelines, are based on the Air Conditioning Contractors of America's (ACCA) HVAC Quality Installation Specification (Ref [2] & [3]), and is recognized as an American National Standard. For new homes, ENERGY STAR Inspection Checklist for National Programs Requirements V3.0 would be used (Ref [4] & [5]).

These industry best practices help ensure that HVAC equipment is:

- 1. Correctly sized to meet customer home's needs
- 2. Connected to a well-sealed duct system
- 3. Operating with sufficient airflow in the system
- 4. Installed with the proper amount of refrigerant

Estimated savings potential (Table 1) with Quality Installation ranges from 18% to 36% for air conditioners and heat pumps and 11% to 18% for furnaces (Ref [6]). A new residential central air conditioner uses 357.6 kWh per ton annually (Ref [1]). The cooling and heating savings are a percentage of total cooling and heating energy consumption.

Table 1: QIV, Performed with New Residential Air Conditioning System Installation, ENERGY STAR Savings Potential

| | Cooling | Heating |
|--------------------|---------|---------|
| Refrigerant Charge | 2-6% | |
| Airflow | 2-5% | |
| Sizing | 3-7% | |
| Duct Sealing | 11-18% | 11-18% |
| Total | 18-36% | 11-18% |

Due to these variations, the savings being estimated for this measure (Table 2) are based on the low-end of the range.

Table 2: Estimated QIV Savings

| | Cooling | Heating |
|--------------------|---------|---------|
| Refrigerant Charge | 2% | |
| Airflow | 2% | |
| Sizing | 3% | |
| Duct Sealing | 11% | 11% |
| Total | 18% | 11% |

Inputs

| Symbol | Description |
|---------|---|
| CAP_C | Nominal cooling capacity, Btu |
| Ton | Capacity of the equipment converted to tons |

Nomenclature

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| Symbol | Description | Units | Values | Comments |
|-------------------|---|-------|---------|------------|
| ACCF _H | Annual Natural Gas Savings, Heating | Ccf | | |
| $AKWH_C$ | Annual Electric Cooling Savings | kWh | | |
| $AKWH_H$ | Annual Electric Heating Savings | kWh | | |
| AOG_H | Annual Oil Savings, Heating | Gal | | |
| APG_H | Annual Propane Savings, Heating | Gal | | |
| CAP_C | Cooling capacity | Btu | | Input |
| PDF_{H} | Natural gas peak day factor -heating | | 0.00977 | Appendix 2 |
| PD_{H} | Natural gas peak day savings – heating | Ccf | | |
| SKW | Summer Demand Savings | kW | | |
| Ton | Capacity of the equipment converted to tons | tons | | Input |
| WKW | Winter Demand Savings | kW | | |

Retrofit Gross Peak Day Savings, Electric

Cooling

The average new residential central air conditioners use 357.6 kWh per ton annually (Ref [1]).

Therefore;

Annual cooling kWh savings = Percent savings x 357.6 x Tons

Where:

Annual cooling savings (Refrigerant Charge) = $2\% \times 357.6 \times \text{tons} = 7.15 \times \text{tons}$ Annual cooling savings (Airflow) = $2\% \times 357.6 \times \text{tons} = 7.15 \times \text{tons}$ Annual cooling savings (Sizing) = $3\% \times 357.6 \times \text{tons} = 10.73 \times \text{tons}$ Annual cooling savings (Duct Sealing) = $11\% \times 357.6 \times \text{tons} = 39.34 \times \text{tons}$

Where:

$$Ton = \frac{CAP_C}{12,000 \, {}_{BTU/ton}}$$

$$AKWH_C = 64.37 \times \frac{CAP_C}{12,000 \, {}_{BTU/ton}}$$

Heating

Using the results of 39.34 kWh duct sealing savings from the above equation and the relationship of savings from table in PSD Measure 4.2.9. Duct Sealing, the CFM reduction can be calculated as follows:

From Measure 4.2.9, for every CFM reduction the cooling savings is 1.059 kWh. Therefore, for 39.34 kWh savings, there is 37.15 CFM reduction.

$$CFMSavings = \frac{39.34}{1.059}$$

$$CFMSavings = 37.15^{CFM}/_{ton}$$

The heat pump and fan savings can be calculated using Duct Sealing, Measure 4.2.9

Heat Pump only:

$$AKWH_{H} = 142.9 \times \frac{CAP_{C}}{12,000^{BTU}/_{ton}}$$

Fan energy for fossil fuel systems only:

$$AKWH_{H} = 40.86 \times \frac{CAP_{C}}{12,000^{BTU}_{ton}}$$

Lost Opportunity Gross Energy Savings, Fossil Fuel

$$ACCF_{H} = 13.3 \times \frac{CAP_{C}}{12,000}$$

 $AOG_{H} = 9.3 \times \frac{CAP_{C}}{12,000}$
 $APG_{H} = 14.2 \times \frac{CAP_{C}}{12,000}$

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Lost Opportunity Gross Energy Savings, Example

A 1980's home has a combination natural gas furnace with a 36,000 Btu (3 tons) central air conditioning system. Quality installation and verification is performed on the systems. What are the energy savings?

Using the equation for cooling savings,

$$AKWH_{C} = 64.37 \times \frac{CAP_{C}}{12,000}$$

 $AKWH_{C} = 64.37 \times \frac{36,000}{12,000} = 193.1kWh$

Using the equation for heating fan energy,

$$AKWH_{H} = 41.25 \times \frac{CAP_{C}}{12,000}$$
$$AKWH_{H} = 41.25 \times \frac{36,000}{12,000} = 123.75kWh$$

Using the equation for natural gas heating,

$$ACCF_{H} = 13.3 \times \frac{CAP_{C}}{12,000}$$

 $ACCF_{H} = 13.3 \times \frac{36,000}{12,000} = 39.9ccf$

Lost Opportunity Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

The new residential central air conditioners use 0.591 kW per ton (Ref [1]).

Therefore, Annual summer kW savings = Percent savings x 0.591 x Tons

$$SKW = 0.106 \times \frac{CAP_C}{12,000}$$

Using the CFM savings from Section 5 and peak savings per CFM from PSD Measure 4.2.9, the winter demand savings for heat pumps only are as follows:

$$WKW = 0.587 \times \frac{CAP_C}{12,000}$$

Lost Opportunity Gross Peak Day Savings, Natural Gas

$$PD_H = ACCF_H \times PDF_H$$

Lost Opportunity Gross Peak Demand Savings, Example

A 1980's home has a 36,000 Btu (3 tons) heat pump system. Quality installation and verification is performed on the systems. What are the summer and winter demand savings?

For cooling savings:

$$SKW = 0.106 \times \frac{CAP_C}{12,000}$$
$$SKW = 0.106 \times \frac{36,000}{12,000} = 0.32kW$$

For heat pump savings:

$$WKW = 0.587 \times \frac{CAP_C}{12,000}$$
$$WKW = 0.587 \times \frac{36,000}{12,000} = 1.76kW$$

References

- [1] Residential Central AC Regional Evaluation, ADM Associates, Inc., November 2009, page 4-9 and page ES-4.
- [2] ACCA. 2010. HVAC Quality Installation Specification Standard 5. Air Conditioning Contractors of America, Arlington, VA.
- [3] ACCA. 2009. HVAC Quality Installation Verification Protocols Standard 9. Air Conditioning Contractors of America, Arlington, VA.
- [4] ENERGY STAR Homes National Programs Requirement V3.0, www.energystar.gov
- [5] ENERGY STAR Homes Inspection Checklist, www.energystar.gov
- [6] ENERGY STAR Quality Installation, http://www.energystar.gov/index.cfm?c=hvac install.hvac install index, last accessed May 23, 2011.

Version Date: 10/30/2012 4.2.15 DUCT INSULATION

4.2.15 DUCT INSULATION

Description of Measure

Installation of insulation with an R-value greater than or equal to 6 on un-insulated heating or cooling ducts in unconditioned space (i.e. attic, unconditioned basement) in order to reduce heating and cooling losses.

Savings Methodology

Heating and cooling savings per square foot of insulated duct were modeled using "3E Plus Insulation" software (Ref [2]) under four different scenarios of duct location (supply basement, return basement, supply attic, return attic), under typical conditions listed in Note [1].

Cooling savings should be reported for homes equipped with central AC using the same duct being insulated.

Note: A duct insulation project should be custom if the actual conditions vary significantly from the typical case presented in this measure (temperature conditions in Note [1], R-value about 6). In such a situation, the 3E Plus tool (Ref [2]) and a similar methodology should be used to develop estimates of the appropriate energy savings.

Reminder: Heating savings may not be claimed if ducts are not used for heating distribution; for instance, a home with electric baseboard resistance heating or a fossil fuel boiler which has ducts used only for the Central Air Conditioner

Inputs

| Symbol | Description | Units |
|--------|--|--------|
| A | Surface area of duct area being insulated | ft^2 |
| | System/Fuel type (Heat pump, Gas Furnace, Oil Furnace, Central AC, etc) | |
| | Duct location: | |
| | - Supply duct in unconditioned basement | |
| | - Return duct in unconditioned basement | |
| | - Supply duct in attic | |
| | - Return duct in attic | |
| | Heating System Distribution Type (Forced air with fan, heat pump, resistance, radiator, etc) | |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|-----------|--|-----------------|--------------|------------|
| A | Surface area of duct being insulated | ft ² | | Input |
| ACCF | Annual Natural Gas Savings | Ccf | | |
| AKWH | Annual Electric Energy Savings | kWh | | |
| AOG | Annual Oil Savings | Gal | | |
| APG | Annual Propane Savings | Gal | | |
| DI_H | Annual Heating Savings per square foot | various | Tables 2 & 3 | Ref [2] |
| DI_C | Annual Cooling Savings per square foot | various | Tables 2 & 3 | Ref [2] |
| PD_{H} | Natural gas peak day savings - heating | Ccf | | |
| PDF_{H} | Natural gas peak day factor -heating | | 0.00977 | Appendix 2 |
| SKW | Summer Demand Savings | kW | | |
| SPF | Summer Peak Factor | W/kWh | 0.017 | Ref [1] |
| WKW | Winter Demand Savings | kW | | |
| WPF | Winter Peak Factor | W/kWh | 0.570 | Ref [1] |

Retrofit Gross Energy Savings, Electric

Table 1: Annual Savings per square foot for homes with Heat Pump or Central AC

| Duct location | Heating | | Cooling | |
|----------------------|---------|---------------------|---------|---------------------|
| | DI_H | Unit | DI_C | Unit |
| Supply basement | 13.05 | kWh/ft ² | 0.7721 | kWh/ft ² |
| Return basement | 3.150 | kWh/ft ² | 0.2327 | kWh/ft ² |
| Supply Attic | 14.46 | kWh/ft ² | 1.425 | kWh/ft ² |
| Return Attic | 4.194 | kWh/ft ² | 0.8209 | kWh/ft ² |

Heating savings, Electric Heat Pumps:

$$AKWH_H = DI_H \times A$$

If Central A/C or Heat Pump providing cooling:

$$AKWH_C = DI_C \times A$$

Retrofit Gross Energy Savings, Fossil Fuel

Table 2: Annual Savings per square foot for homes with fossil fuel

| Duct location | Heating Savings per square foot | | |
|----------------------|---------------------------------|------------------------|--|
| | DI _H Unit | | |
| Supply basement | 0.1187 | MMbtu/ ft ² | |
| Return basement | 0.02866 | MMbtu/ ft ² | |
| Supply Attic | 0.1316 | MMbtu/ ft ² | |
| Return Attic | 0.03816 | MMbtu/ ft ² | |

For homes with a natural gas furnace,

$$ACCF_H = \frac{DI_H \times A}{0.10290}$$

For homes with an oil furnace,

$$AOG_H = \frac{DI_H \times A}{0.13869}$$

For homes with a propane furnace,

$$APG_H = \frac{DI_H \times A}{0.09133}$$

Reminder: cooling savings can be claimed for homes equipped with central AC

Retrofit Gross Energy Savings, Example

A Cape Cod style home has a gas furnace. It is also equipped with a central AC system for cooling. 50 ft² of insulation was installed on the supply duct in the unconditioned basement. What are the annual energy savings?

$$ACCF_{H} = \frac{DI_{H} \times A}{0.10290}$$

$$ACCF_{H} = \frac{0.1187 \times 50 \text{ ft}^{2}}{0.10290} = 57.68 \text{ Ccf}$$

Since the house is equipped with central AC, there are cooling savings too:

$$AKWH_C = DI_C \times A$$

$$AKWH_C = 0.7721 \times 50 \text{ft}^2 = 38.61 \text{ kWh}$$

Version Date: 10/30/2012 4.2.15 DUCT INSULATION

Retrofit Gross Seasonal Peak Day Savings, Electric (Winter and Summer)

Winter seasonal peak demand (kW) will be claimed for homes equipped with a Heat Pump:

$$WKW = \frac{WPF \times DI_H \times A}{1,000 \, \text{W/}_{kW}}$$

Summer seasonal peak demand (kW) will be claimed for homes equipped with Central AC:

$$SKW = \frac{SPF \times DI_C \times A}{1,000 \, \text{W/}_{kW}}$$

Retrofit Gross Peak Day Savings, Natural Gas

For homes with a natural gas furnace,

$$PD_H = ACCF_H \times PDF_H$$

Retrofit Gross Peak Demand Savings, Example

What are the peak demand savings for the above retrofit example? Using the formula for Peak Day Natural Gas:

$$PD_{H} = ACCF_{H} \times PDF_{H}$$

$$PD_{H} = 57.68 \times 0.00977 = 0.564 Ccf$$

Cooling demand savings may also be claimed:

$$SKW = \frac{SPF \times DI_C \times A}{1,000 \frac{W}{kW}}$$

$$SKW = \frac{0.017 \times 0.7721 \times 50 \text{ ft}^2}{1,000 \frac{W}{kW}} = 0.000656 \text{ kW}$$

Changes from Last Version

Table 1 and Table 2 constants used in the calculations were refined based on an updated analysis. Corrected cooling calculation and addressed custom situations.

References

- [1] Evaluation of the Weatherization Residential Assistance Partnership (WRAP) and Helps Programs, conducted by KEMA, table ES-6 page 1-8.
- [2] NAIMA, 3E Plus software tool, Version 4.0, Released 2005

Notes

[1] Assumed Temperature Conditions

| Duct Location | Season | Ambient Temp | Supply Air | Return Air |
|----------------------|---------|---------------|------------|------------|
| | | (° F) | Temp (°F) | Temp (°F) |
| Attic | Heating | 30 | 130 | 65 |
| | Cooling | 120 | 50 | 80 |
| Basement | Heating | 50 | 130 | 65 |
| | Cooling | 70 | 50 | 80 |

Version Date: 10/30/2012 4.2.17 BOILER

4.2.17 BOILER

Description of Measure

Installation of an Energy-efficient boiler

Savings Methodology

The fossil fuel savings for this measure are calculated using the same methodology as the ENERGY STAR Boiler calculator, which is located on the ENERGY STAR Website (Ref [1]). The calculator uses the home's year of construction, location, and area to determine the home's annual heating load. The age on the boiler is used to determine the efficiency. When a boiler is also used for domestic hot water, hot water savings are also estimated. Hot water savings are calculated based on the hot water load used in the water heater Measure 4.5.7.

Energy savings resulting from the removal of units in working condition are calculated as follows:

Lost Opportunity Measure:

• Lost Opportunity savings are the difference in energy use between a baseline new model (Note [1]) and the chosen high efficiency new model, continuing for the Effective Useful Life (EUL) from Appendix 4.

Retrofit Measure:

- Uses the same methodology as a Lost Opportunity measure;
- In the case of early retirement of a working unit, where the unit would have otherwise been installed until failure, lifetime "Retirement" savings are claimed additional to the lifetime "Lost Opportunity" savings (see Section 1.4).
- Retirement savings are the difference in energy use between the older unit and a baseline new model (Note [1]), continuing for the Remaining Useful Life (RUL) from Appendix 4.

Inputs

| Symbol | Description | Units |
|-------------------|--|-------|
| | Heating Fuel (Natural gas, oil, propane) | |
| YR_h | Year of home construction | Year |
| YR _e | Year existing boiler installed | Year |
| SF | Heated area served by boiler | SF |
| AFUE _I | AFUE-installed | % |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|-------------------|---|-----------------|----------------------|-------------------|
| A | Heated area served by boiler | ft ² | | Input |
| $ABTU_H$ | Annual Btu savings - heating | Btu/yr | | |
| ACCF | Annual natural gas savings | Ccf/yr | | |
| $ACCF_H$ | Annual natural gas savings -heating | Ccf/yr | | |
| $ACCF_W$ | Annual natural gas savings - water heating | Ccf/yr | | |
| ADHW | Annual domestic water heating load | Btu/yr | 11,197,132 | From water heater |
| | | | | (Measure 4.5.7) |
| $AFUE_{B}$ | Annual Fuel Utilization Efficiency, Baseline | % | 80% - Gas or Propane | Note [1] |
| | | | 80% - Oil | |
| $AFUE_{E}$ | Annual Fuel Utilization Efficiency, Existing | % | Table 2 (if known) | Ref [1] |
| AFUE _I | Annual Fuel Utilization Efficiency, Installed | % | | Input |
| EUL | Effective Useful Life | | | Appendix 4 |

Version Date: 10/30/2012 **4.2.17 BOILER**

| Symbol | Description | Units | Values | Comments |
|-----------------|--|----------|---------|------------|
| HF | Heating Factor based on age of home | Btu/ft²/ | Table 1 | Ref [1] |
| | | Yr | | |
| PD | Natural gas peak day savings | Ccf/yr | | |
| PD_{H} | Natural gas peak day savings - heating | Ccf/yr | | |
| PD_{W} | Natural gas peak day savings - water heating | Ccf/yr | | |
| PDF_{H} | Natural gas peak day factor - heating | | 0.00977 | Appendix 1 |
| PDF_{W} | Natural gas peak day factor - water heating | | 0.00321 | Appendix 1 |
| RUL | Remaining Useful Life | | | Appendix 4 |
| YR_h | Year of home construction | Years | | Input |
| YR _e | Year existing boiler installed | Years | | Input |

Lost Opportunity Gross Energy Savings, Fossil Fuel

Table 1: Residential Heating Factor (Ref [1])

| Year of home Construction (YR _h) | HF (BTU/SF/year) | | | |
|--|------------------|--|--|--|
| Before 1940 | 45,000 | | | |
| 1940 to 1949 | 41,400 | | | |
| 1950 to 1959 | 38,700 | | | |
| 1960 to 1969 | 36,000 | | | |
| 1970 to 1979 | 33,300 | | | |
| 1980 to 1989 | 30,600 | | | |
| 1990 to 1999 | 27,900 | | | |
| 2000 to present | 26,100 | | | |

Table 2: Existing AFUE (Ref [1])

| - 1110 - 1 - 1110 - 1 - 1 - 1 - 1 - 1 - | | | | |
|---|----------|----------|--|--|
| Year existing Boiler installed (YR _e) | Gas AFUE | Oil AFUE | | |
| Before 1960 | 60% | 60% | | |
| 1960 to 1969 | 60% | 65% | | |
| 1970 to 1974 | 65% | 75% | | |
| 1975 to 1983 | 65% | 75% | | |
| 1984 to 1987 | 70% | 80% | | |
| 1988 to 1991 | 77% | 80% | | |
| 1992 to present (baseline) | 80% | 80% | | |

Savings by heating fuel:

Savings by heating fuel:
$$ABTU_{H} = SF \times HF \times \left(\frac{1}{AFUE_{b}} - \frac{1}{AFUE_{i}}\right)$$

$$ACCF_{H} = \frac{ABTU_{H}}{102,900 \frac{Btu}{Ccf}}$$

$$AOG_{H} = \frac{ABTU_{H}}{138,690 \frac{Btu}{Gal}}$$

$$APG_{H} = \frac{ABTU_{H}}{91,330 \frac{Btu}{Gal}}$$

Water Heating Savings by water heating fuel:

$$ABTU_{W} = ADHW \times \left(\frac{1}{AFUE_{b}} - \frac{1}{AFUE_{i}}\right)$$

$$ACCF_{W} = \frac{ABTU_{W}}{102,900^{Btu}/c_{cf}}$$

$$ACCF_{W} = \frac{ABTU_{W}}{138,690^{Btu}/c_{cf}}$$

$$ACCF_{W} = \frac{ABTU_{W}}{91,330^{Btu}/c_{cf}}$$

Lost Opportunity Gross Energy Savings, Example

A boiler is installed in a natural gas heated home. The boiler is used to heat domestic hot water in addition to heating the home which is 2,000 square feet. The home was built in 1974 and the existing boiler was installed in 1985. The installed boiler has efficiency (AFUE) of 83 percent.

From Tables 1 and 2 above:

HF = 33,300

 $AFUE_{I} = 83\% \text{ or } 0.83$

 $AFUE_B = 80\% \text{ or } 0.80$

$$ABTU_{H} = 2,000 \times 33,300 \times \left(\frac{1}{0.80} - \frac{1}{0.83}\right)$$

$$ABTU_{H} = 3,008,988 \ Btu$$

$$ACCF_{H} = \frac{3,008,988 \ Btu}{102,900 \ ^{Btu}/_{Ccf}}$$

$$ACCF_{H} = 29.2 \ Ccf$$

Water Heating:

$$ABTU_{W} = 11,197,132 \times \left(\frac{1}{0.80} - \frac{1}{0.83}\right)$$

$$ABTU_{W} = 505,886 Btu$$

$$ACCF_{W} = \frac{505,886 Btu}{102,900 \frac{Btu}{Ccf}}$$

$$ACCF_{W} = 4.9 Ccf$$

Total:

$$ACCF = ACCF_{H} + ACCF_{W}$$

$$ACCF = 29.2 \frac{\text{Cef}}{\text{yr}} + 4.9 \frac{\text{Cef}}{\text{yr}}$$

$$ACCF = 34.1 \frac{\text{Cef}}{\text{yr}}$$

Lost Opportunity Gross Seasonal Peak Demand Savings, Natural Gas

$$PD_H = ACCF_H \times PDF_H$$

 $PD_W = ACCF_W \times PDF_W$

Lost Opportunity Gross Peak Demand Savings, Example

For the same example as above:

$$PD_H = 29.2 \times 0.00977$$

$$PD_{H} = 0.28 \ Ccf$$

$$PD_{w} = 4.9 \times 0.00321$$

$$PD_{w} = 0.0157 \ Ccf$$

Total:

$$PD = PD_H + PD_W$$

$$PD = 0.28 + 0.0157$$

$$PD = 0.296 \ Ccf$$

Retrofit Gross Energy Savings, Fossil Fuel

Reminder: Retrofit savings are the sum of Retirement savings and Lost Opportunity savings. This section presents the Retirement portion of savings.

Tables 1 and 2 are used to estimate the heating load and existing boiler efficiency of the home, based on age.

$$ABTU_{H} = A \times HF \times \left(\frac{1}{AFUE_{E}} - \frac{1}{AFUE_{B}}\right)$$

Savings by heating fuel:

$$ACCF_H = \frac{ABTU_H}{102,900^{Btu}/_{Ccf}}$$

$$AOG_H = \frac{ABTU_H}{138,690^{Btu}/_{Gal}}$$

$$APG_H = \frac{ABTU_H}{91,330^{Btu}/_{Gal}}$$

If Boiler also provides DHW:

$$ABTU_{W} = ADHW \times \left(\frac{1}{AFUE_{e}} - \frac{1}{AFUE_{b}}\right)$$

$$ABTU_{W} = 11,197,132 \times \left(\frac{1}{AFUE_{e}} - \frac{1}{AFUE_{b}}\right)$$

Water Heating Savings by water heating fuel:

$$ACCF_{W} = \frac{ABTU_{W}}{102,900 \frac{Btu}{Ccf}}$$

$$AOG_{W} = \frac{ABTU_{W}}{138,690 \frac{Btu}{Gal}}$$

$$APG_{W} = \frac{ABTU_{W}}{91,330 \frac{Btu}{Gal}}$$

Retrofit Gross Energy Savings, Example

A boiler is installed in a natural gas heated home. The boiler is used to heat domestic hot water in addition to heating the home which is 2,000 square feet. The home was built in 1974 and the existing boiler was installed in 1985.

From Tables 1 and 2: HF = 33,300 $AFUE_E = 70\%$ or 0.70 $AFUE_B = 80\%$ or 0.80

Reminder: Retrofit savings do not depend on the efficiency of the new installed unit.

$$ABTU_{H} = 2,000 \times 33,300 \times \left(\frac{1}{0.70} - \frac{1}{0.80}\right)$$

 $ABTU_{H} = 11,892,857 \ Btu$

$$ACCF_{H} = \frac{11,892,857}{102,900 \frac{Bnu}{Ccf}}$$

 $ACCF_{H} = 116 \frac{Ccf}{Ccf}$

Water Heating:

$$ABTU_{W} = 11,197,132 \times \left(\frac{1}{0.70} - \frac{1}{0.80}\right)$$

$$ABTU_{H} = 1,999,488 \ Btu$$

$$ACCF_{W} = \frac{1,999,488 \ Btu}{102,900^{Btu}/_{Ccf}}$$

$$ACCF_{W} = 19 \ Ccf$$

Total:

$$ACCF = ACCF_H + ACCF_W$$

 $ACCF = 116 + 19$
 $ACCF = 135 Ccf$

Retrofit Gross Peak Day Savings, Natural Gas

$$PD_H = ACCF_H \times PDF_H$$

If Boiler also provides DHW:

$$PD_{W} = ACCF_{W} \times PDF_{W}$$

Retrofit Gross Peak Demand Savings, Example

For same example as above:

$$PD_H = 144 \times 0.00977$$

$$PD_H = 1.4 \ Ccf$$

$$PD_w = 19 \times 0.00321$$

$$PD_w = 0.1 \, Ccf$$

$$PD = PD_H + PD_W$$

$$PD = 1.5 Ccf$$

References

[1] ENERGY STAR Microsoft Excel tool, "Life Cycle Cost Estimate for an ENERGY STAR Residential Furnace," http://www.energystar.gov/ia/business/bulk_purchasing/bpsavings_calc/Calc_Furnaces.xls, last updated July, 2009, last accessed August 6, 2012.

Notes

[1] The baseline values are based in reference [1] efficiencies for 2011.

4.2.18 FURNACE

Description of Measure

Installation of a warm air or forced-air energy efficient furnace

Savings Methodology

The fossil fuel savings for this measure are calculated using the same methodology as the ENERGY STAR furnace calculator, located on the ENERGY STAR Website (Ref [1]) with the exception of heating factor (Note [2]). The calculator uses the home's year of construction, location, and area to determine the home's annual heating load. The age on the furnace is used to determine the efficiency. This measure can be either lost opportunity or early retirement.

To account for the estimated remaining life of an existing furnace and the additional lost opportunity savings from a new installed unit, energy savings resulting from the removal of units in working condition are calculated as follows:

Lost Opportunity Measure:

• Lost Opportunity savings are the difference in energy use between a baseline new model and the chosen high-efficiency new model, continuing for the Effective Useful Life (EUL) from Appendix 4.

Retrofit Measure:

- Uses the same methodology as a Lost Opportunity measure;
- In the case of early retirement of a working unit where the unit would have otherwise been installed until failure, lifetime "Retirement" savings are claimed additional to the lifetime "Lost Opportunity" savings (see Section 1.4).
- Retirement savings are the difference in energy use between the older unit and a baseline new model, continuing for the Remaining Useful Life (RUL) from Appendix 4.

In addition to the fossil fuel savings, this measure can include electric savings if the furnace is installed with an energy efficient fan motor. For these savings, see Measure 4.2.6, Electrically Commutated Motor (ECM).

Inputs

| Symbol | Description | Units |
|-------------------|--|--------|
| | Heating Fuel (Natural gas, oil, propane) | |
| YR_h | Year of home construction | Year |
| YR _e | Year existing furnace installed | Year |
| A | Heated area served by furnace | ft^2 |
| AFUE _E | AFUE –existing (if available) | % |
| AFUE _I | AFUE -installed | % |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|-------------------|-------------------------------------|---------|-----------------------|---------------|
| A | Heated area served by furnace | ft^2 | | Input |
| $ABTU_H$ | Annual Btu savings – heating | Btu | | |
| $ACCF_H$ | Annual natural gas savings –heating | Ccf | 102,900 Btu | |
| AFUE _B | AFUE of baseline furnace | | 0.78 (Gas or Propane) | Table 2, Note |
| | | | 0.80 (Oil) | [1] |
| $AFUE_{E}$ | AFUE of existing furnace | | Table 2 if unknown | |
| AOG _H | Annual oil savings – heating | Gallons | 138,690 Btu | |
| APG _H | Annual propane savings –heating | Gallons | 91,330 Btu | |

| Symbol | Description | Units | Values | Comments |
|-----------------|--|---------------------|---------|------------|
| EUL | Effective Useful Life | | | Appendix 4 |
| HF | Heating Factor based on age of home | Btu/ft ² | Table 1 | Note [2] |
| PD_{H} | Natural gas peak day savings – heating | Ccf | | |
| PDF_{H} | Natural gas peak day factor –heating | | 0.00977 | Appendix 2 |
| RUL | Remaining Useful Life | | | Appendix 4 |
| YR_h | Year of home construction | Years | | Input |
| YR _e | Year existing furnace installed | Years | | Input |

Lost Opportunity Gross Energy Savings, Fossil Fuel

Table 1: Residential Heating Factor (Ref [1])

| Year of home Construction (YR _h) | HF (BTU/SF/year) |
|--|------------------|
| Before 1940 | 52,900 |
| 1940 to 1949 | 48,700 |
| 1950 to 1959 | 45,500 |
| 1960 to 1969 | 42,400 |
| 1970 to 1979 | 39,200 |
| 1980 to 1989 | 36,000 |
| 1990 to 1999 | 32,800 |
| 2000 to present | 30,700 |

Table 2: Existing AFUE (Ref [1])

| Year existing furnace installed (YRe) | Gas/Propane AFUE | Oil AFUE |
|---------------------------------------|------------------|----------|
| Before 1960 | 60% | 60% |
| 1960 to 1969 | 60% | 65% |
| 1970 to 1974 | 65% | 72% |
| 1975 to 1983 | 68% | 75% |
| 1984 to 1987 | 68% | 80% |
| 1988 to 1991 | 76% | 80% |
| 1992 to present (baseline) | 78% | 80% |

$$ABTU_{H} = A \times HF \times \left(\frac{1}{AFUE_{B}} - \frac{1}{AFUE_{I}}\right)$$

Savings by heating fuel:

$$ACCF_{H} = \frac{ABTU_{H}}{102,900 \frac{Btu}{Cef}}$$

$$AOG_{H} = \frac{ABTU_{H}}{138,690 \frac{Btu}{Gal}}$$

$$APG_{H} = \frac{ABTU_{H}}{91,330 \frac{Btu}{Gal}}$$

Lost Opportunity Gross Energy Savings, Example

A 2,000 sq ft home is built in 1974. The home is heated by a natural gas Furnace. The existing natural gas furnace was installed in 1985. A new natural gas furnace with an AFUE of 95% is installed. What are the annual fossil fuel savings?

From Tables 1 and 2: HF = 39,200

 $AFUE_{I} = 95\% \text{ or } 0.95$

 $AFUE_{B} = 78\% \text{ or } 0.78$

$$ABTU_{H} = 2,000 \times 39,200 \times \left(\frac{1}{0.78} - \frac{1}{0.95}\right)$$

$$ABTU_{H} = 17,986,505 \ Btu$$

$$ACCF_{H} = \frac{16,211,745 \ Btu}{102,900 \ Btu/Ccf}$$

$$ACCF_{H} = 175 \ Ccf$$

Lost Opportunity Gross Peak Day Savings, Natural Gas

$$PD_H = ACCF_H \times PDF_H$$

Lost Opportunity Gross Peak Demand Savings, Example

A 2,000 sq ft home is built in 1974. The home is heated by a natural gas Furnace. The existing natural gas furnace was installed in 1985. A new natural gas furnace with an AFUE of 95% is installed. What are the Peak Day Natural Gas savings?

$$PD_H = 175 \times 0.00977$$

$$PD_H = 1.7 \ CCF$$

Retrofit Gross Energy Savings, Fossil Fuel

Reminder: Retrofit savings are the sum of Retirement savings and Lost Opportunity savings. This section presents the Retirement portion of savings.

Using the Tables 1 and 2, the home's heating load and existing furnace efficiency can be estimated.

$$ABTU_{H} = A \times HF \times \left(\frac{1}{AFUE_{E}} - \frac{1}{AFUE_{B}}\right)$$

Savings by heating fuel:

$$ACCF_{H} = \frac{ABTU_{H}}{102,900^{Btu}/c_{cf}}$$

$$AOG_{H} = \frac{ABTU_{H}}{138,690^{Btu}/G_{al}}$$

$$APG_{H} = \frac{ABTU_{H}}{91,330^{Btu}/G_{al}}$$

Reminder: For electric savings for energy efficient fan motors, see measure 4.2.6 (ECM).

Retrofit Gross Energy Savings, Example

A 2,000 square foot home is built in 1974. The home is heated by a natural gas furnace. The existing natural gas furnace was installed in 1985. What are the annual fossil fuel savings for the replacement of this furnace?

Reminder: Retrofit savings do not depend on the efficiency of the new installed unit.

From Tables: HF = 39,200 $AFUE_E = 68\%$ or 0.68 $AFUE_B = 78\%$ or 0.78

$$ABTU_{H} = 2,000 \times 39,200 \times \left(\frac{1}{0.68} - \frac{1}{0.78}\right)$$

$$ABTU_{H} = 14,781,297 \ Btu$$

$$ACCF_{H} = \frac{14,781,297}{102,900 \ Btu/Ccf}$$

$$ACCF_{H} = 144 \ Ccf$$

Retrofit Gross Peak Day Savings, Natural Gas

$$PD_H = ACCF_H \times PDF_H$$

Retrofit Gross Peak Demand Savings, Example

A 2,000 sq ft home is built in 1974. The home is heated by a natural gas Furnace. The existing natural gas furnace was installed in 1985. What are the Peak Day Natural Gas savings?

$$PD_{H} = 144 \times 0.00977$$

 $PD_{H} = 1.4 \ Ccf$

References

[1] ENERGY STAR Microsoft Excel tool, "Life Cycle Cost Estimate for an ENERGY STAR Residential Furnace," http://www.energystar.gov/ia/business/bulk-purchasing/bpsavings-calc/Calc Furnaces.xls, last updated July, 2009, last accessed Mar 23, 2011.

Notes

- [1] The baseline values are based in reference [1] efficiencies for 2011.
- [2] The Heating Factor from reference [1] was increased by 15% to account for Duct losses. The 15% is based on the ENERGY STAR Quality Installation and Verification Potential (QIV) Savings. These are outlined in Measure 4.2.14, QIV.

4.3 APPLIANCES AND CONSUMER GOODS

4.3.6 ROOM AIR CONDITIONER

Description of Measure

Version Date: 10/30/2012

Savings detailed below cover the purchase of a high efficiency room air conditioner and the replacement of an inefficient room air conditioner in working condition.

Savings Methodology

Lost Opportunity Measure:

- Lost Opportunity savings are the difference in energy use between a baseline new model (Note [2]), and the chosen high efficiency new model, continuing for the Effective Useful Life (EUL) from Appendix 4.
- The Retail measure is a Lost Opportunity-only methodology, as the existing unit is not verified.

Retrofit Measure:

- Uses the same methodology as a Lost Opportunity measure.
- In the case of early retirement of a working unit where the unit would have otherwise been installed until failure, lifetime "Retirement" savings are claimed additional to the lifetime "Lost Opportunity" savings (see Section 1.4).
- Retirement savings are the difference in energy use between the older unit (Note [1]) and a baseline new model (Note [2]), continuing for the Remaining Useful Life (RUL) from Appendix 4.

Table 1: Energy Specifications (Note [3])

| Product Size in CAP _C (Btu/hr) | 2000 Federal Standard (Ref [3]) | | |
|--|---------------------------------|--------|--|
| Type: | Window | Sleeve | |
| <8,000 | 9.7 | 9.0 | |
| 8,000 - 13,999 | 9.8 | 8.5 | |
| 14,000 - 19,999 | 9.7 | | |
| >20,000 | 8.5 | | |

Inputs

| Symbol | Description | Required For |
|------------------|--|------------------|
| EER _e | Energy Efficiency Ratio of existing unit | Retirement |
| EER _i | Energy Efficiency Ratio of new unit | Lost Opportunity |
| $CAP_{C,e}$ | Rated cooling capacity of existing unit, in Btu/hr | Retirement |
| $CAP_{C,i}$ | Rated cooling capacity of new unit, in Btu/hr | Lost Opportunity |
| | Brand and Model of existing unit | Retirement |
| | Brand and Model of new installed unit | Lost Opportunity |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|-----------------|---|----------|-------------------------------|----------|
| $AKWH_C$ | Annual electric energy savings - cooling | kWh/yr | Calculated | |
| $CAP_{C,i}$ | Rated cooling capacity of new installed unit | Btu/hr | | |
| $CAP_{C,e}$ | Rated cooling capacity of (old) existing unit | Btu/hr | Actual as rated; Use | |
| | | | CAP _{C,i} if unknown | |
| CF _S | Summer Seasonal Peak Coincidence Factor | unitless | Appendix 1 | |

| Symbol | Description | Units | Values | Comments |
|-------------------|--|--------------|-----------------------|----------|
| EER _b | Energy Efficiency Ratio, representing baseline new | Btu/ Watt-hr | 2000 Federal Standard | Note [2] |
| | model | | level from Table 1 | |
| EER _i | Energy Efficiency Ratio of new installed unit | Btu/ Watt-hr | Actual as rated | |
| EER _e | Energy Efficiency Ratio of existing unit | Btu/ Watt-hr | Actual as rated (use | Note [1] |
| | | | 8.86 if unknown) | |
| EUL | Effective Useful Life: Measure life of the new unit | years | Appendix 4 | |
| EFLH | Annual Equivalent Full Load Hours | hr/yr | 272 | Ref [1] |
| LKWH _C | Lifetime electric energy savings - cooling | kWh | Calculated | |
| RUL | Remaining Useful Life: remaining number of years | years | Appendix 4 | |
| | the existing unit would have operated until failure. | | | |
| SKW _C | Summer Seasonal Demand savings-cooling | kW | Calculated | |
| Sleeve | Unit without louvered sides | | | Note [4] |
| Window | Unit with louvered sides | | | |
| Retire | Associated with Retirement | | | |

Lost Opportunity Gross Energy Savings, Electric

Associated with Lost Opportunity

Version Date: 10/30/2012

$$AKWH_{C,LostOpp} = EFLH \times CAP_{C,i} \times \left(\frac{1}{EER_b} - \frac{1}{EER_i}\right) \div 1000_{kW}^{W}$$
 (Note [2])

Lost Opportunity Gross Energy Savings, Example

Example 1. A 6,000 Btu/hr window AC unit at 11.7 EER is purchased through a retail promotion; what are the savings?

Use size and EER of the installed unit, and the federal standard EER for the installed unit's size (Table 1):

$$AKWH_{C,LostOpp} = 272 \, {}^{hrs}/_{yr} \times 6,000 \, {}^{Btu}/_{yr} \times \left(\frac{1}{9.7 \, {}^{Btu}/_{W \cdot \bullet hr}} - \frac{1}{11.7 \, {}^{Btu}/_{W \cdot \bullet hr}}\right) \div 1000 \, {}^{W}/_{kW}$$

$$AKWH_{C,LostOpp} = 28.8 \, kWh$$

Lost Opportunity Gross Seasonal Peak Demand Savings, Electric, Winter and Summer

$$SKW_{C,LostOpp} = CF_s \times CAP_{C,i} \times \left(\frac{1}{EER_b} - \frac{1}{EER_i}\right) \div 1000 \,\text{W/kW}$$

Lost Opportunity Gross Peak Demand Savings, Example

Example 2. A 6,000 Btu/hr window AC unit at 11.7 EER is purchased through a retail promotion; what are the demand savings?

Use size and EER of the installed unit, and the federal standard EER for the installed unit's size (Table 1):

$$SKW_{LostOpp} = 0.303 \times 6,000 \, {}^{Btu/_{yr}} \times \left(\frac{1}{9.7 \, {}^{Btu/_{W \cdot \bullet hr}}} - \frac{1}{11.7 \, {}^{Btu/_{W \cdot \bullet hr}}}\right) \div 1000 \, {}^{W/_{kW}}$$
$$SKW_{LostOpp} = 0.0320 \, kW$$

Retrofit Gross Energy Savings, Electric

Reminder: Retrofit savings are the sum of Retirement savings and Lost Opportunity savings. This section presents the Retirement portion of savings.

Retirement Component:

$$AKWH_{C,Retire} = EFLH \times CAP_{C,e} \times \left(\frac{1}{EER_e} - \frac{1}{EER_b}\right) \div 1000 \text{W/kW}$$

Retrofit Gross Energy Savings, Example

Example 3. An existing window air conditioner rated 5,900 Btu/hr 8 EER and verified to be in working condition is replaced with a 6,000 Btu/hr unit at 11.7 EER. What are the energy savings?

Lost Opportunity: using the size and EER of the installed (new) unit as well as the federal standard EER for the rated size (from Table 1) yields:

$$AKWH_{C,LostOpp} = 272 \frac{hrs}{yr} \times 6,000 \frac{Btu}{yr} \times \left(\frac{1}{9.7 \frac{Btu}{W \cdot \bullet hr}} - \frac{1}{11.7 \frac{Btu}{W \cdot \bullet hr}}\right) \div 1000 \frac{W}{kW}$$
$$AKWH_{C,LostOpp} = 28.8 \frac{kWh}{M}$$

Retirement: using the size and EER of the existing (old) unit as well as the federal standard EER for the existing unit's rated size (from Table 1) yields:

$$AKWH_{C,Retire} = 272 \, \frac{hrs}{yr} \times 5,900 \, \frac{Btu}{yr} \times \left(\frac{1}{8.0 \, \frac{Btu}{W \cdot \bullet_{hr}}} - \frac{1}{9.7 \, \frac{Btu}{W \cdot \bullet_{hr}}} \right) \div 1000 \, \frac{W}{kW}$$

$$AKWH_{C,Retire} = 35.2 \, kWh$$

Retrofit Gross Seasonal Peak Demand Savings, Electric, Winter and Summer

Reminder: Retrofit savings are the sum of Retirement savings and Lost Opportunity savings. This section presents the Retirement portion of savings.

Retirement Component:

$$SKW_{C,Retire} = CF_s \times CAP_{C,e} \times \left(\frac{1}{EER_e} - \frac{1}{EER_b}\right) \div 1000 \%_{kW}$$

Retrofit Gross Peak Demand, Example

Example 4. An existing window air conditioner rated 5,900 Btu/hr 8 EER and verified to be in working condition is replaced with a 6,000 Btu/hr unit at 11.7 EER. What are the energy savings?

Lost Opportunity: using the size and EER of the installed (new) unit as well as the federal standard EER for the rated size (from Table 1) yields:

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$$SKW_{LostOpp} = 0.303 \times 6,000 \, \frac{Btu}{yr} \times \left(\frac{1}{9.7 \, \frac{Btu}{W \cdot \bullet hr}} - \frac{1}{11.7 \, \frac{Btu}{W \cdot \bullet hr}} \right) \div 1000 \, \frac{W}{kW}$$
$$SKW_{LostOpp} = 0.0320 \, kW$$

Retirement: using the size and EER of the existing (old) unit as well as the federal standard EER for the existing unit's rated size (from Table 1) yields:

$$SKW_{Retire} = 0.303 \times 5,900 \, \frac{Btu}{y_r} \times \left(\frac{1}{8.0 \, \frac{Btu}{W \cdot \bullet_{hr}}} - \frac{1}{9.7 \, \frac{Btu}{W \cdot \bullet_{hr}}} \right) \div 1000 \, \frac{W}{kW}$$
$$SKW_{Retire} = 0.0392 \, kW$$

Changes from Last Version

Retrofit measure is more clearly presented as two-part savings that may be added together if qualified. A default efficiency level has been defined for the existing unit. Examples have been refreshed.

References

- [1] LW Coincidence Factor Study: Room Air Conditioners, Prepared for: Northeast Energy Efficiency Partnerships' New England Evaluation and State Program Working Group, June 23, 2008, page iv.
- [2] Consortium for Energy Efficiency. CEE Super-Efficient Appliances Initiative: High Efficiency Specifications for Room Air Conditioners, Effective January 1, 2003. ©2003.
- [3] ENERGY STAR Program Requirements for Room Air Conditioners, Version 2.1. Effective November 16, 2005. Revised on December 17, 2010.
- [4] ENERGY STAR Program Requirements Product Specification for Room Air Conditioners, Version 3.0. Effective October 1, 2012. Draft 2: May 17, 2011.
- [5] KEMA, Inc. Ductless Mini Pilot Study: Final Report. June, 2009, page vi.

Notes

- [1] The EER and capacity of the existing unit should be looked up in the CEC database or equivalent source by brand and model number. If the EER of the old air conditioner is unknown, use 8.86 EER, based on Ref [5], page vi, which identified baseline efficiencies for room ACs replaced with ductless heat pumps.
- [2] The EER of the baseline unit is at the 2000 Federal Standard level (Table 1); Lost Opportunity at the installed unit's size, and Retirement at the existing unit's size. **Note:** A Federal Standard is anticipated to be effective June 1, 2014.
- [3] ENERGY STAR Version 3.0 criteria (Ref [4]) will be effective Oct 1, 2013, but as of June 22, 2012, manufacturers may have products certified to V3.0. Table 2 below is an expanded version of Table 1, and lists all relevant standards for this measure (in addition to the 2000 Federal Standard in Table 1):

Version Date: 10/30/2012

Table 2: Energy Specifications (Enhanced)

| Tuble 20 Energy Specifications (Emittineed) | | | | | | | | |
|--|------------------------------|---------|------------------------------|--------|-----------------|-----------|------------|------------|
| Product Size in | Product Size in 2000 Federal | | 2005 ENERGY Oct | | Oct 2013 ENERGY | | CEE Tier 1 | CEE Tier 2 |
| CAP _C (Btu/hr) Standard (Ref [3]) | | STAR V2 | AR V2.1 (Ref STAR V3.0 (Note | | (Ref [2]) | (Ref [2]) | | |
| | | | [3]) | [3]) | | | | |
| Type: | Window | Sleeve | Window | Sleeve | Window | Sleeve | Window | Window |
| <8,000 | 9.7 | 9.0 | 10.7 | 9.9 | 11.2 | 10.4 | 11.2 | 11.6 |
| 8,000 - 13,999 | 9.8 | 8.5 | 10.8 | 9.4 | 11.3 | 9.8 | 11.3 | 11.8 |
| 14,000 - 19,999 | 9.7 | | 10.7 | | 11.2 | | 11.2 | 11.6 |
| >20,000 | 8.5 | | 9.4 | | 9.8 | 1 | 9.8 | 10.2 |

[4] ENERGY STAR defines a "Through the Wall (TTW)" unit as "A RAC [Room Air Conditioner] without louvered sides," also referred to as a "built-in" or sleeve unit. "Window" units in this measure are defined as those with louvered sides. This measure does not explicitly cover Casement (width-constrained) or Reverse Cycle (i.e. heat pump) units.

Version Date: 10/30/2012 4.3.7 CLOTHES WASHER

4.3.7 CLOTHES WASHER

Description of Measure

Savings detailed below cover the purchase of a standard size high efficiency clothes washer and the replacement of an inefficient clothes washer in working condition.

Savings Methodology

Lost Opportunity Measure:

- Lost Opportunity savings are the difference in energy use between a baseline new model (Note [1]), and the chosen high efficiency new model, continuing for the Effective Useful Life (EUL) from Appendix 4.
- The Retail measure is a Lost Opportunity-only methodology only, as the existing unit is not verified, and savings are claimed for a mix of fuels when the hot water/dryer fuel type combinations are not known as shown in Note [5].
- The ENERGY STAR New Home measure is a special Lost-Opportunity-only measure, where the hot water/dryer fuel type is known but the current ENERGY STAR level is used as the baseline.

Retrofit Measure:

- Uses the same methodology as a Lost Opportunity measure.
- In the case of early retirement of a working unit where the unit would have otherwise been installed until failure, lifetime "Retirement" savings are claimed additional to the lifetime "Lost Opportunity" savings (See Section 1.4).
- Retirement savings are the difference in energy use between the older unit (Note [4]) and a baseline new model (Note [1]), continuing for the Remaining Useful Life (RUL) from Appendix 4. See exception in Note [2].

Energy savings for clothes washers come from three sources (see Note [3]):

- 1. Machine energy savings (electricity used to run the washer itself): always electric energy.
- 2. Water Heater savings, due to the reduction in hot water use: for the fuel that is used in the home's water heater.
- 3. Dryer savings, due to the shorter drying times needed because high spin speeds leave less water in the clothes: claimed for the fuel that is used in the dryer that is to be used in conjunction with the washer; if there is no dryer, no dryer savings can be claimed.

No demand savings have been identified for this measure.

Inputs

| Symbol | Description | Required for: |
|-------------|--|------------------------|
| Axis | Existing unit's configuration: Front Loading (Horizontal Axis) or Top | Note [2]; not used for |
| Orientation | Loading (Vertical Axis) | savings |
| Dryer Type | Type of dryer to be used with the new installed unit: Electric, Gas, or None | All except Retail |
| MEF_{i} | Modified Energy Factor of new installed unit | Lost Opportunity |
| Cape | Compartment Capacity of existing unit in Cubic ft. | Retirement |
| Capi | Compartment Capacity of new installed unit in Cubic ft. | Lost Opportunity |
| WF_i | Water Factor of new installed unit (Used for calculating water savings) | Lost Opportunity |
| WH Fuel | Water heating fuel | All except Retail |
| | Brand and Model of existing unit | Retirement |
| | Brand and Model of new installed unit | Lost Opportunity |

Version Date: 10/30/2012 4.3.7 CLOTHES WASHER

Nomenclature

| Symbol | Description | Units | Values | Comments |
|------------------|---|-----------------------------|---|--|
| ACCF | Annual natural gas energy savings | Ccf/yr | Calculated | |
| AKWH | Annual electric energy savings | kWh/yr | Calculated | |
| AOG_W | Annual energy savings for oil Water Heater | Gal Oil/yr | Calculated | |
| APG_W | Annual energy savings for propane Water Heater | Gal Propane/yr | Calculated | |
| AWG | Annual Gallons of water saved | Gal/Year | Calculated | |
| Cape | Compartment capacity of existing clothes washer | cubic feet, ft ³ | Actual; use Cap _i if unknown | |
| Cap _i | Compartment capacity of new installed clothes washer | cubic feet, ft ³ | Actual as found | |
| Cycles/yr | Average number of loads of laundry per year | Cycles/yr | Residential: 392 | Ref [4] |
| EAKWH | Equivalent total annual electric equivalent energy reduction calculated directly from a model's MEF: the sum of Machine, Water Heater, and Clothes Dryer components | kWh/yr | Calculated | Definition of MEF. Used in derivation only |
| EF | Water Heating Efficiency for fossil fuel water heaters | unitless | 0.62 | Ref [6] |
| EUL | Effective Useful Life: Measure life of installed unit. | years | Appendix 4 | |
| Ltotal | Total gross lifetime energy or water savings | various | Calculated | |
| MEF _b | Modified Energy Factor (MEF) of baseline new model | ft ³ /kWh/cycle | New Home: 2.0 All Others: 1.8 | Note [1] |
| MEF _e | Modified Energy Factor (MEF) of existing unit | ft ³ /kWh/cycle | 1.26 | Note [4] |
| MEF_i | Modified Energy Factor (MEF) of new installed unit | ft ³ /kWh/cycle | Actual as rated | |
| RUL | Remaining Useful Life: remaining number of years the existing unit would have operated until failure | years | Appendix 4 | |
| WF _b | Water Factor (WF): gallons of water needed per ft ³ of laundry, baseline new model | gal/ft ³ · cycle | New Home: 6.0 All others: 7.5 | Note [1] |
| WF _e | Water Factor for existing unit | gal/ft ³ · cycle | 9.5 | Note [4] |
| WFi | Water Factor for installed unit | gal/ft ³ · cycle | Actual as found | |
| р | Associated with Clothes Dryer energy component | | Fuel-specific | |
| · · · lost opp | Associated with Lost Opportunity | | | |
| •••М | Associated with Machine energy component | | Fuel-specific | |
| ···retire | Associated with Retirement | | | |
| · · · turn-in | Associated with Turn-in Program | | | |
| ···W | Associated with Water Heating component | | Fuel-specific | |

Lost Opportunity Gross Energy Savings, Electric

Savings are based on the capacity of the existing unit and are the sum of three components (discussed previously):

- 1. *Machine energy savings*: always electric energy.
- 2. *Water Heater savings*: for the fuel that is used in the home's water heater.
- 3. *Dryer savings*: claimed for the fuel that is used in the dryer.

Table 1: Lost Opportunity Savings Summary by Savings Component, Electric Fuel (Note [3])

| Savings Component | Known Fuel Type | Unknown Fuel Type † |
|----------------------|---|--|
| Machine Energy | $AKWH_{M,LostOpp} = 20.78 \times Cap_i \times \left(\frac{1}{MEF_b} - \frac{1}{MEF_i}\right)$ | |
| Water Heater | $AKWH_{M,LostOpp} = 49 \times Cap_i \times \left(\frac{1}{MEF_b} - \frac{1}{MEF_i}\right)$ | $AKWH_{Lost Opp} = 321.3 \times Cap_i \times \left(\frac{1}{1.8} - \frac{1}{MEF_i}\right)$ |
| Clothes Dryer | $AKWH_{M,LostOpp} = 322.2 \times Cap_i \times \left(\frac{1}{MEF_b} - \frac{1}{MEF_i}\right)$ | |

[†]When the fuel is unknown (as in a retail purchase), this equation is used to calculate electric savings in conjunction with the equations for fossil fuels from Table 2. See Note [5] for details

Lost Opportunity Gross Energy Savings, Fossil Fuel

Savings are based on the capacity of the existing unit and are the sum of three components (discussed previously):

- 1. Machine energy savings: always electric energy.
- 2. Water Heater savings: for the fuel that is used in the home's water heater.
- 3. *Dryer savings*: claimed for the fuel that is used in the dryer.

Table 2: Lost Opportunity Savings Summary by Savings Component and Fossil Fuel (Note [3])

| Savings Component | Known Fuel Type | Unknown Fuel Type ††† |
|---------------------------------------|---|---|
| Machine Energy | $AKWH_{M,LostOpp} = 20.78 \times Cap_i \times \left(\frac{1}{MEF_b} - \frac{1}{MEF_i}\right)$ | Already accounted for by equation in Table 1 |
| Water Heater: Natural Gas †† | $ACCF_{W,LostOpp} = 2.621 \times Cap_i \times \left(\frac{1}{MEF_b} - \frac{1}{MEF_i}\right)$ | $ACCF_{Lost\ Opp} = 1.630 \times Cap_i \times \left(\frac{1}{1.8} - \frac{1}{MEF_i}\right)$ |
| Water Heater: Oil | $AOG_{W,LostOpp} = 1.944 \times Cap_i \times \left(\frac{1}{MEF_b} - \frac{1}{MEF_i}\right)$ | $AOG_{Lost Opp} = 0.9914 \times Cap_i \times \left(\frac{1}{1.8} - \frac{1}{MEF_i}\right)$ |
| Water Heater: Propane | $APG_{W,LostOpp} = 2.953 \times Cap_i \times \left(\frac{1}{MEF_b} - \frac{1}{MEF_i}\right)$ | $APG_{Lost Opp} = 0.2510 \times Cap_i \times \left(\frac{1}{1.8} - \frac{1}{MEF_i}\right)$ |
| Clothes Dryer (Gas Only) | $ACCF_{W,LostOpp} = 10.68 \times Cap_i \times \left(\frac{1}{MEF_b} - \frac{1}{MEF_i}\right)$ | Already accounted for by equation in Table 1 |

^{††} Existing Water heater efficiency is assumed to be 62%

Non Energy Benefits

Lost Opportunity Water Savings: these savings are also applicable to unknown fuel conditions:

$$AWG_{Lost\ Opp} = Cap_i \times 392^{cycles}/_{yr} \times (WF_b - WF_i)^{gal}/_{fi^3 \cdot cycle}$$

Retirement Water Savings: (Note [6])

$$AWG_{Re\,tire} = 784 \frac{Gal}{vr} \times Cap_e$$

^{†††} When the fuel is unknown (as in a retail purchase), this equation is used to calculate fossil fuel savings in conjunction with the equations for electric savings from Table 1. See Note [5] for details

Lost Opportunity Gross Energy Savings, Example

Example 1. Calculate the savings for a 3.00 ft³ capacity Clothes Washer purchased through a Retail promotion. The unit has an MEF of 2.22 and a WF of 4.2.

As this is a retail purchase, fuel type is unknown and the unknown fuel condition equations are used to calculate savings. Note that the baseline is 1.8 MEF and 7.5 WF.

Machine Energy: Use the equation for electric retail savings (Table 1) and use MEF_b = 1.8, MEF_i = 2.22, and Cap_i=3:

$$AKWH_{LostOpp} = 321.3 \times 3.00 \, ft^3 \times \left(\frac{1}{1.8} - \frac{1}{2.22}\right)$$

 $AKWH_{LostOpp} = 101.3 \, kWh/yr$

To calculate the fossil fuel savings, use the equations for unknown fuel conditions from Table 2:

$$ACCF_{LostOpp} = 1.630 \times 3.00 \, ft^3 \times \left(\frac{1}{1.8} - \frac{1}{2.22}\right)$$

 $ACCF_{LostOpp} = 0.5140^{Ccf}/_{vr}$

Oil:

$$AOG_{LostOpp} = .9914 \times 3.00 \, ft^3 \times \left(\frac{1}{1.8} - \frac{1}{2.22}\right)$$
$$ACCF_{LostOpp} = 0.3126 \, \frac{Gal}{v_{YF}}$$

Propane.

$$APG_{LostOpp} = 0.2510 \times 3.00 \, ft^3 \times \left(\frac{1}{1.8} - \frac{1}{2.22}\right)$$

 $APG_{LostOpp} = 0.0791^{Gal}/_{vr}$

In addition, water savings are calculated as a Non Electric Benefit:

$$\begin{split} AWG_{Lost\ Opp} &= Cap_i \times 392^{cycles}/_{yr} \times (WF_b - WF_i)^{gal}/_{ft^3 \cdot cycle} \\ AWG_{Lost\ Opp} &= 3ft^3 \times 392^{cycles}/_{yr} \times (7.5^{gal}/_{ft^3 \cdot cycle} - 4.2^{gal}/_{ft^3 \cdot cycle}) \\ AWG_{Lost\ Opp} &= 3,881^{Gal}/_{yr} \end{split}$$

Example 2. What are the energy savings from installing a new 3.81 ft³ clothes washer with MEF of 3.21 and WF of 2.9 in an ENERGY STAR New Home? The home has a gas hot water heater and a gas clothes dryer.

Machine Energy: Using the equations with MEF_b=2.0, MEF_i=3.21, and WF_b=6.0, and WF_i=2.9, and Cap_i=3.81:

$$AKWH_{LostOpp} = 20.78 \times 3.81 ft^{3} \times \left(\frac{1}{2.0} - \frac{1}{3.21}\right)$$

 $AKWH_{LostOpp} = 14.92 \frac{kWh}{vr}$

Water Heater: In this example, gas is the fuel used for water heating:

$$ACCF_{LostOpp} = 2.621 \times 3.81 ft^{3} \times \left(\frac{1}{2.0} - \frac{1}{3.21}\right)$$

 $ACCF_{LostOpp} = 1.88^{Ccf}/_{vr}$

Clothes Dryer: In this example, gas is the fuel used for the clothes dryer:

$$ACCF_{LostOpp} = 10.68 \times 3.81 ft^{3} \times \left(\frac{1}{2.0} - \frac{1}{3.21}\right)$$
$$ACCF_{LostOpp} = 7.67 \frac{Ccf}{v_{r}}$$

In addition, water savings are calculated as a Non-Electric benefit:

$$\begin{split} AWG_{Lost\ Opp} &= Cap_i \times 392^{\ cycles}/_{yr} \times (WF_b - WF_i)^{\ gal}/_{ft^3 \cdot cycle} \\ AWG_{Lost\ Opp} &= 3.81ft^3 \times 392^{\ cycles}/_{yr} \times (6.0^{\ gal}/_{ft^3 \cdot cycle} - 2.9^{\ gal}/_{ft^3 \cdot cycle}) \\ AWG_{Lost\ Opp} &= 4,630^{\ Gal}/_{yr} \end{split}$$

Retrofit Gross Energy Savings, Electric

Reminder: Retrofit savings are the sum of Retirement savings and Lost Opportunity savings. This section presents the Retirement portion of savings.

Retirement Component: Savings are based on the capacity of the existing unit and are the sum of the previously discussed three components:

- 1. Machine energy savings: always electric energy.
- 2. *Water Heater savings*: for the fuel that is used in the home's water heater.
- 3. *Dryer savings*: claimed for the fuel that is used in the dryer.

Table 3: Retirement Savings; Summary by Fuel Type and Savings Component (Note [3])

| Fuel Type | Savings Component | | | |
|-----------|--|--|---|--|
| | Machine Energy | Water Heater | Clothes Dryer | |
| Electric | $AKWH_{M,retire} = 5.227 \times Cap_e$ | $AKWH_{W, retire} = 16.43 \times Cap_e$ | $AKWH_{D, retire} = 71.68 \times Cap_e$ | |
| Gas | | $ACCF_{W, Retire} = 0.8785 \times Cap_e$ | $ACCF_{D, Retire} = 2.377 \times Cap_e$ | |
| Oil | | $AOG_{W, Retire} = 0.6518 \times Cap_e$ | | |
| Propane | | $APG_{W, Retire} = 0.9898 \times Cap_e$ | | |

Retrofit Gross Energy Savings, Fossil Fuel

Reminder: Retrofit savings are the sum of Retirement savings and Lost Opportunity savings. This section presents the Retirement portion of savings.

Retirement Component: Savings are based on the capacity of the existing unit and are the sum of the previously discussed three components:

- 1. Machine energy savings: always electric energy.
- 2. *Water Heater savings*: for the fuel that is used in the home's water heater.
- 3. *Dryer savings*: claimed for the fuel that is used in the dryer.

Refer to Table 4 for the equation to calculate savings, depending on the fossil fuel of each component.

Retrofit Gross Energy Savings, Example

Example 3. In an existing home, a 3.00 ft³ capacity unit is installed with an MEF of 2.22 and a WF of 4.2. The home uses an electric dryer and a gas water heater. The existing unit is the same size as the new unit and is top-loading (unknown existing efficiency, but verified to be in working condition). What are the total savings?

Lost Opportunity: use $Cap_i = 3$, $MEF_b = 1.8$, $MEF_i = 2.22$, $WF_b = 7.5$, $WF_i = 4.2$, and equations from Tables 1 and 2 to calculate savings for each savings component and fuel type:

Machine Energy:

$$AKWH_{LostOpp} = 20.78 \times 3 ft^{3} \times \left(\frac{1}{1.8} - \frac{1}{2.22}\right)$$
$$AKWH_{LostOpp} = 6.55 \frac{kWh}{yr}$$

Water Heater: In this example, gas is the fuel used for water heating:

$$ACCF_{LostOpp} = 2.621 \times 3 ft^{3} \times \left(\frac{1}{1.8} - \frac{1}{2.22}\right)$$
$$ACCF_{LostOpp} = 0.82 \frac{Ccf}{vr}$$

Clothes Dryer: In this example, electricity is the fuel used for the clothes dryer:

$$AKWH_{LostOpp} = 322.2 \times 3 ft^{3} \times \left(\frac{1}{1.8} - \frac{1}{2.22}\right)$$
$$AKWH_{LostOpp} = 101.6 \frac{kWh}{yr}$$

In addition, water savings are calculated as a Non Electric Benefit:

$$\begin{split} AWG_{Lost\ Opp} &= Cap_i \times 392^{\ cycles}/_{yr} \times (WF_b - WF_i)^{\ gal}/_{fi^3 \cdot cycle} \\ AWG_{Lost\ Opp} &= 3ft^3 \times 392^{\ cycles}/_{yr} \times (7.5^{\ gal}/_{fi^3 \cdot cycle} - 4.22^{\ gal}/_{fi^3 \cdot cycle}) \\ AWG_{Lost\ Opp} &= 3,857^{\ Gal}/_{yr} \end{split}$$

Retirement: use Cap_i=3 to calculate savings and equations from Table 2 for each savings component and fuel type:

Machine Energy:

$$AKWH_{M,Retire} = 5.227 \times Cap_e$$

 $AKWH_{M,Retire} = 5.227 \times 3.00 \text{ ft}^3$
 $AKWH_{M,Retire} = 15.68 \frac{kWh}{yr}$

Water Heater: From the example, the fuel source for the water heater is natural gas

$$ACCF_{W,Retire} = 0.8785 \times Cap_e$$

 $ACCF_{W,Retire} = 0.8785 \times 3.00 ft^3$
 $ACCF_{W,Retire} = 2.64 \frac{ccf}{v}$

Clothes Dryer: From the example, the fuel source for the clothes dryer is electric

$$AKWH_{D,Retire} = 71.68 \times Cap_e$$

 $AKWH_{D,Retire} = 71.68 \times 3.00 \, ft^3$
 $AKWH_{D,Retire} = 215.0 \, kWh/yr$

Non Electric Benefit: Water Savings may also be calculated

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$$AWG_{Retire} = 784 \frac{Gal}{ft^3 \cdot yr} \times Cap_e$$

$$AWG_{Retire} = 784 \times 3.00 ft^3$$

$$AWG_{Retire} = 2,352 \frac{Gal}{yr}$$

Non Energy Benefits

New units may have additional useful features and controls, do a better job cleaning, use less detergent, and leave less water weight remaining in the clean items.

Changes from Last Version

Equations were simplified wherever possible. Lost Opportunity calculations moved to the Lost Opportunity sections from Retrofit sections. Retail is no longer deemed, allowing custom calculation of specific super-efficient models. Listed water heater and dryer fuel mix (Note [5]). Examples have been refreshed. Savings calculations were added for New Homes. Notes [6] added, and Note [3] expanded to include derivation of equations.

References

- [1] ENERGY STAR Program Requirements Product Specification for Clothes Washers: Eligibility Criteria, Version 5.1. Effective January 1, 2011. Tier 1 effective July 1, 2009, Tier 2 effective January 1, 2011.
- [2] U.S. D.O.E. Energy Conservation Standards Rulemaking Framework Document for Residential Clothes Washers, August 21, 2009.
- [3] ENERGY STAR Consumer Clothes Washer Calculator, Excel Spreadsheet Tool, updated October 2009 by Cadmus Group, Available Online at http://www.energystar.gov/ia/business/bulk-purchasing/bpsavings-calc/CalculatorConsumerClothesWasher.xls, last accessed June 13, 2011.
- [4] DOE Federal Test Procedure 10 CFR 430, Appendix J1, as of June 14, 2011.
- [5] Consortium for Energy Efficiency (CEE) Super Efficient Home Appliances Initiative (SEHA): High efficiency specification for residential clothes washers. January 1, 2011.
- [6] Federal Register Part III, DOE Energy Conservation Program: Energy Conservation standards for Residential Water Heaters, Direct Heating Equipment, Pool Heater; (Final Rule, Table I.2). April 16, 2010.
- [7] ENERGY STAR Program Requirements Product Specification for Clothes Washers: Eligibility Criteria, Version 6.0. Effective February 1, 2013

Notes

- [1] The MEF and WF of the baseline unit are at 2009 ENERGY STAR Version 5.1 Tier 1 level, which does not depend on any categories. New Construction is a special case, where the baseline must be current ENERGY STAR level (Ref [7]).
- [2] According to the Engineering Analysis section of Ref [2], "a survey of frontloading clothes washers in the CEC [California Energy Commission] appliance database shows that there are no frontloading washers with efficiencies at the existing Federal standards level, or, for that matter, any below the [January 2007] ENERGY STAR level (1.72 MEF/8.00 WF)." (Italicized text within brackets was added for clarification and is not part of the original document.). Therefore, if the existing unit is front-loading, the "retirement" portion may not be claimed (Note [2]).

[3] The ENERGY STAR Calculator tool (Ref [3]) gives average energy consumption based on all qualified models and the same average for all non-qualified models. While manufacturers are permitted to achieve the MEF by varying any blend of the three energy areas, the energy proportion values below are derived from those average consumptions and reflect the average weight each component contributes to total energy use:

Table 4: Proportions for Equivalent Energy Proportions

| Measure | Machine Proportion | Water Heater Proportion | Clothes Dryer Proportion |
|------------------|---------------------------|-------------------------|---------------------------------|
| Lost Opportunity | 5.3% | 12.5% | 82.2% |
| Retirement | 5.6% | 17.6% | 76.8% |

To derive the equations in Tables 2-4, calculate the difference in equivalent total electric energy between two units using MEF. For non-electric equations, the equivalent total kWh is split into its components according to the proportions in Table 5, then converted from electricity into each fuel, including assumed water heater efficiency of 62%:

Deriving the Lost Opportunity Portion (Table 1)

First calculate the difference in equivalent total electric energy from one model to another, based on MEF:

$$EAKWH_{Lost Opp} = Cap_{i} \times 392^{cycles} /_{yr} \times \left(\frac{1}{MEF_{b}} - \frac{1}{MEF_{i}}\right)$$

The equivalent total kWh is split into its components according to the proportions in Note [3]: *Machine Energy (All):*

$$AKWH_{M,Lost\,Opp} = 5.3\% \times EAKWH_{Lost\,Opp} = AKWH_{M,LostOpp} = 20.78 \times Cap_i \times \left(\frac{1}{MEF_b} - \frac{1}{MEF_i}\right)$$

Electric Water Heater:

$$AKWH_{W, Lost Opp} = 12.5\% \times EAKWH_{Lost Opp} = AKWH_{M, LostOpp} = 49 \times Cap_i \times \left(\frac{1}{MEF_b} - \frac{1}{MEF_i}\right)$$

Electric Clothes Dryer:

$$AKWH_{D,Lost\ Opp} = 82.2\% \times EAKWH_{Lost\ Opp} = AKWH_{M,LostOpp} = 322.2 \times Cap_i \times \left(\frac{1}{MEF_b} - \frac{1}{MEF_i}\right)$$

For Fossil Fuels, a conversion from kWh is required:

Gas Water Heater:

$$ACCF_{W,Lost\,Opp} = \frac{12.5\% \times 3412^{Btu}/_{kWh} \times EAKWH_{Lost\,Opp}}{102,900^{Btu}/_{Cof} \times 0.62} = ACCF_{W,LostOpp} = 2.621 \times Cap_i \times \left(\frac{1}{MEF_b} - \frac{1}{MEF_i}\right)$$

Oil Water Heater:

$$AOG_{W,LostOpp} = \frac{12.5\% \times 3412^{Btu}/_{kWh} \times EAKWH_{LostOpp}}{138,690^{Btu}/_{Gal} \times 62\%} = AOG_{W,LostOpp} = 1.944 \times Cap_i \times \left(\frac{1}{MEF_b} - \frac{1}{MEF_i}\right)$$

Propane Water Heater:

$$AOG_{W,Lost\ Opp} = \frac{12.5\% \times 3412^{Btu}/_{kWh} \times EAKWH_{Lost\ Opp}}{91,330^{Btu}/_{Gal} \times 62\%} = APG_{W,LostOpp} = 2.953 \times Cap_{i} \times \left(\frac{1}{MEF_{b}} - \frac{1}{MEF_{i}}\right)$$

Gas Clothes Dryer:

$$ACCF_{D,Lost\ Opp} = \frac{82.2\% \times 3412^{Btu}/_{kWh} \times EAKWH_{Lost\ Opp}}{102,900^{Btu}/_{Gal}} = ACCF_{W,LostOpp} = 10.68 \times Cap_i \times \left(\frac{1}{MEF_b} - \frac{1}{MEF_i}\right)$$

Deriving the Retirement Portion: (Table 2)

First, the equivalent total annual kWh is calculated, using baseline and standard values:

$$EAKWH_{Lost\ Opp} = 392 \frac{cycles}{y_r} \times \left(\frac{1}{MEF_e} - \frac{1}{MEF_b}\right) \times Cap_i$$

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$$EAKWH_{Lost Opp} = 392 \times \left(\frac{1}{1.26} - \frac{1}{1.8}\right) \times Cap_i = 93.333 \times Cap_i$$

The equivalent total kWh is split into its components according to values in Table 5:

Machine Energy (All Fuels): $AKWH_{M, retire} = 5.6\% \times EAKWH_{retire} = AKWH_{M, retire} = 5.227 \times Cap_e$

Electric Water Heater: $AKWH_{W, retire} = 17.6\% \times EAKWH_{retire} = AKWH_{W, retire} = 16.43 \times Cap_e$

Electric Clothes Dryer: $AKWH_{D.retire} = 76.8\% \times EAKWH_{retire} = AKWH_{D.retire} = 71.68 \times Cap_e$

For Fossil Fuels, a conversion from kWh is required:

Gas Water Heater:

$$ACCF_{W,Retire} = \frac{17.6\% \times 3412^{Btu}/_{kWh} \times EAKWH_{Retire}}{102,900^{Btu}/_{Ccf} \times 62\%} = ACCF_{W,Retire} = 0.8785 \times Cap_e$$

Oil Water Heater:

$$AOG_{W,Retire} = \frac{17.6\% \times 3412 \frac{Btu}_{kWh} \times EAKWH_{Retire}}{138,690 \frac{Btu}{Gal} \times 62\%} = AOG_{W,Retire} = 0.6518 \times Cap_{e}$$

Propane Water Heater:

$$AOG_{W,Retire} = \frac{17.6\% \times 3412^{Btu}/_{kWh} \times EAKWH_{Retire}}{91,330^{Btu}/_{Gal} \times 62\%} = APG_{W,Retire} = 0.9898 \times Cap_{e}$$

Gas Clothes Dryer:

$$ACCF_{D,Retire} = \frac{76.8\% \times 3412 \frac{Btu}{kWh} \times EAKWH_{retire}}{102,900 \frac{Btu}{Gal}} = ACCF_{D,Retire} = 2.377 \times Cap_{e}$$

[4] For early retirement cases where the MEF and WF of the existing unit is unknown, the existing unit efficiency is estimated to be at the level of the 2010 Federal Standard: 1.26 MEF and 9.5 WF (Ref [6]). Listed below are MEF and WF values for relevant standards:

| ia vii values for relevant standards. | | | | | | |
|---------------------------------------|------|-----|---------------|--|--|--|
| Level | MEF | WF | Reference | | | |
| 2010 Federal Standard | 1.26 | 9.5 | [6] | | | |
| 2009 ENERGY STAR | 1.8 | 7.5 | [1] | | | |
| CEE Tier 1 / 2011 ENERGY STAR / 2013 | 2.0 | 6.0 | [5], [1], [7] | | | |
| ENERGY STAR | | | | | | |
| CEE Tier 2 | 2.2 | 4.5 | [5] | | | |
| CEE Tier 3 | 2.4 | 4.0 | [5] | | | |

[5] When the hot water and dryer fuels are both unknown, the following fuel mix is estimated typical for Connecticut. Savings are claimed for all fuel types according to the following percentages; this weighting has been done by multiplying every individual Lost Opportunity component of every fuel by its respective percentage and only the resultant equations have been listed in the body of the measure:

| Water Heater Fuel | | | | Clothes D | ryer Fuel |
|--------------------------|-------|-----|------|-----------|-----------|
| Electric Gas Oil Propane | | | | Electric | Gas |
| 15% | 25.5% | 51% | 8.5% | 91% | 9% |

[6] Non Energy benefits for the retirement component simplifies as follows:

$$\begin{aligned} AWG_{Retire} &= Cap_e \times 392^{cycles}/_{yr} \times \left(WF_e - WF_b\right) \\ AWG_{Retire} &= Cap_e \times 392^{cycles}/_{yr} \times \left(9.5^{Gal}/_{ft^3} - 7.5^{Gal}/_{ft^3}\right) = 784 \times Cap_e \end{aligned}$$

4.3.8 DISHWASHER

Description of Measure

Savings detailed below cover the purchase of a high efficiency standard size residential dishwasher and the replacement of an inefficient dishwasher in working condition.

Savings Methodology

Lost Opportunity Measure:

- Lost Opportunity savings are the difference in energy use between a baseline new model (Note [3]), and the chosen high efficiency new model, continuing for the Effective Useful Life (EUL) from Appendix 4.
- The Retail measure is a Lost Opportunity-only methodology, as the existing unit is not verified, and savings are claimed for a mix of fuels when the hot water fuel type is not known (Note [1]).
- The Energy Star New Home measure is a special Lost-Opportunity-only measure, where the hot water fuel type is known.

Retrofit Measure:

- Uses the same methodology as a Lost Opportunity measure.
- In the case of early retirement of a working unit where the unit would have otherwise been installed until failure, lifetime "Retirement" savings are claimed additional to the lifetime "Lost Opportunity" savings (see Section 1.4).
- Retirement savings are the difference in energy use between the older unit (Note [4]) and a baseline new model (Note [3]), a deemed value, continuing for the Remaining Useful Life (RUL) from Appendix 4.

Dishwashers are rated for the kWh energy use per year, and hot water usage per cycle. Savings, based on equations derived in Note [2], come from two sources:

- 1. Machine energy savings (electricity used to run the machine and during standby mode): always electric energy.
- 2. Water Heater savings, due to the reduction in hot water use: may only be claimed for the fuel that is used in the home's water heater.

Inputs

| Symbol | Description | Required for |
|---------|--|---|
| WH Fuel | Water Heater fuel type | All (When unknown, use fuel mix, Note [1]) |
| Ei | Rated kWh/yr of new unit | Lost Opportunity |
| GPC | Rated gallons of water per cycle of new unit | Lost Opportunity |
| | Brand and Model of existing unit | Verification purposes only (not used for savings) |
| | Brand and Model of new installed unit | Lost Opportunity |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|----------------|--|-----------|------------------|----------------|
| $AKWH_{M}$ | Annual gross Machine electric savings, including motor, | kWh/yr | calculated | Notes [1], [3] |
| | heater, and dryer energy as well as standby energy. | | | |
| $AKWH_W$ | Annual gross energy savings for an electric water heater | kWh/yr | calculated | Notes [1], [3] |
| AKWH | Annual gross electric savings | kWh/yr | | |
| AOG | Annual gross energy savings for an oil water heater. | Gal/yr | calculated | Notes [1],[3] |
| APG | Annual gross energy savings for a propane water heater. | Gal/yr | calculated | Notes [1],[3] |
| Cycles/yr | Average number of loads of dishes per year | Cycles/yr | Residential: 215 | Ref [1] |
| E_b | Annual Rated kWh usage of baseline unit | kWh/yr | 307 | Ref [6] |
| E _e | Annual Rated kWh usage of existing unit | kWh/yr | 371 | Note [4] |

| Symbol | Description | Units | Values | Comments |
|------------------|---|-----------|----------|-------------------|
| E_{i} | Annual Rated kWh usage of new installed unit | kWh/yr | Actual | |
| EF | Efficiency for fossil fuel Water Heaters | Unitless | | Ref [5] |
| GPC_b | Estimated Gallons of Water per cycle of baseline unit | Gal/cycle | 5.0 | Ref [6], Note [4] |
| GPC _i | Rated Gallons of Water per cycle of installed unit | Gal/cycle | As found | |
| ···retire | Associated with Retirement component. | | | |
| · · · lost opp | Associated with Lost Opportunity component. | | | |

Lost Opportunity Gross Energy Savings, Electric

Savings shown in Tables 1 and 2 are the sum of two components (discussed previously):

- 1. *Machine energy savings*: always electric energy.
- 2. *Water Heater savings*: for the fuel that is used in the home's water heater.

Table 1a: Lost Opportunity Savings When Fuel Type is Known (using baseline level shown in Table 3)

| Savings Component | Fuel Type | Equation |
|-------------------|-----------|--|
| Machine Energy | All units | $AKWH_{M,lost opp} = 126 \frac{kWh}{y_r} - \left[E_i - \left(36.17 \times GPC_i \right) \right]$ |
| | Electric | $AKWH_{W,lost opp} = 181^{kWh}/_{yr} - (36.17 \times GPC_i)$ |
| Water Heater | Gas | $ACCF_{lost opp} = 9.670^{Ccf}/_{yr} - (1.934 \times GPC_i)$ |
| (claim only one) | Oil | $AOG_{lost opp} = 7.175 \frac{Gal}{yr} - (1.435 \times GPC_i)$ |
| | Propane | $APG_{lost opp} = 10.90^{Gal}/_{yr} - (2.179 \times GPC_i)$ |

Table 1b: Lost Opportunity Savings When Fuel Type is Unknown (Note [1])

| | Fuel Type | Equation (Derived using Table 1a equations, Note [1] methodology) |
|------------------------------|-----------|--|
| Total energy | Electric | $AKWH_{lost opp, fuel mix} = 153^{kWh}/_{yr} - [E_i - (30.74 \times GPC_i)]$ |
| savings for a | Gas | $ACCF_{lost opp, fuel mix} = 2.466 \frac{ccf}{y_r} - (0.4932 \times GPC_i)$ |
| mix of fuels per Note [1] | Oil | $AOG_{lost opp, fuel mix} = 3.659^{Gal Oil}/_{yr} - (0.7319 \times GPC_i)$ |
| (claim all) | Propane | $APG_{lost opp, fuel mix} = 0.9265^{Gal}/_{yr} - (0.1852 \times GPC_i)$ |

Lost Opportunity Gross Energy Savings, Fossil Fuel

Use equations in Table 1a to calculate savings. If water heater fuel is unknown, use Table 1b.

Lost Opportunity Gross Energy Savings, Example

A new unit is purchased through a retail promotion, rated for total energy of 190 kWh/yr and total water use of 2.9 Gallons/cycle. The water heater fuel is unknown. What savings may be claimed?

Because the water heating fuel type is not known, a mix of fuels is claimed per the equations in Table 1b:

$$AKWH_{lost opp, fuel mix} = 153 \, \frac{kWh}{yr} - \left[E_i - \left(30.74 \times GPC_i \right) \right]$$

$$AKWH_{lost opp, fuel mix} = 153 \, \frac{kWh}{yr} - \left[190 \, \frac{kWh}{yr} - \left(30.74 \times 2.9 \right) \right] = 52.1 \, \frac{kWh}{yr}$$

$$ACCF_{lost opp, fuel mix} = 2.466 \frac{ccf}{yr} - (0.4932 \times GPC_i)$$

$$ACCF_{lost opp, fuel mix} = 2.466 \frac{ccf}{yr} - (0.4932 \times 2.9) = 1.036 \frac{ccf}{yr}$$

$$AOG_{lost\;opp} = 3.659^{\,Gal\;Oil}/_{yr} - \left(0.7319 \times GPC_i\right)$$

$$AOG_{lost opp} = 3.659 \frac{Gal Oil}{yr} - (0.7319 \times 2.9) = 1.54 \frac{Gal Oil}{yr}$$

$$APG_{lost opp} = 0.9265 \frac{Gal}{yr} - (0.1852 \times GPC_i)$$

$$APG_{lost opp} = 0.9265 \frac{Gal}{yr} - (0.1852 \times 2.9) = 0.389 \frac{Gal Propane}{yr}$$

$$AWG_{lost opp} = (5.0 \frac{Gal}{cycle} - GPC_i) \times 215 \frac{cycles}{yr}$$

$$AWG_{lost opp} = (5.0 \frac{Gal}{cycle} - 2.9) \times 215 \frac{cycles}{yr} = 452 \frac{Gal Water}{yr}$$

Retrofit Gross Energy Savings, Electric

Reminder: Retrofit savings are the sum of Retirement savings and Lost Opportunity savings. This section presents the Retirement portion of savings while the Lost Opportunity portion of the savings is presented further on in this measure. To obtain the lifetime savings, the following formula should be used:

$$LKWH_{Total} = (AKWH_{Retire} \times RUL) + (AKWH_{Lost\ Opp} \times EUL)$$

Retirement Component:

Table 2a: Retirement Savings When Fuel Type is Known (using baseline level shown in Table 3)

| Savings Component | Fuel Type | Derivation | Deemed Savings |
|-------------------|-----------|--|----------------|
| Machine Energy | All units | $AKWH_{M,lost opp} = [371 \frac{kWh}{yr} - (36.17 \times 5.8)] - 126 \frac{kWh}{yr}$ | 35 kWh/yr |
| | Electric | $AKWH_{W,lost opp} = (36.17 \times 5.8) - 181^{kWh}/_{yr}$ | 29 kWh/yr |
| Water Heater | Gas | $ACCF_{lost opp} = (1.934 \times 5.8) - 9.670 \frac{Ccf}{y_r}$ | 1.547 Ccf/yr |
| (claim only one) | Oil | $AOG_{lost \ opp} = (1.435 \times 5.8) - 7.175^{Gal}/_{yr}$ | 1.148 Gal/yr |
| | Propane | $APG_{lost opp} = (2.179 \times 5.8) - 10.90 \frac{Gal}{yr}$ | 1.738 Gal/yr |

Table 2b: Retirement Savings When Fuel Type is Unknown (Note [1])

| | Fuel Type | Derivation (using Table 2a equations, Note [1] methodology) | Deemed Savings |
|--|--------------|---|----------------|
| Total energy | Electric | $AKWH_{lost opp, fuel mix} = 35.2 \frac{kWh}{yr} + (15\% \times 28.8 \frac{kWh}{yr})$ | 39.5 kWh/yr |
| savings for a mix of fuels per Note [1] (claim all) | Gas | $ACCF_{lost opp, fuel mix} = (25.5\% \times 1.547 \frac{Ccf}{yr})$ | 0.394 Ccf/yr |
| | Oil | $AOG_{lost \ opp, \ fuel \ mix} = (51\% \times 1.148 \frac{Gal}{y_r})$ | 0.585 Gal/yr |
| | Propane | $APG_{lost opp, fuel mix} = (8.5\% \times 1.738 \frac{Gal}{yr})$ | 0.148 Gal/yr |

Retrofit Gross Energy Savings, Fossil Fuel

Reminder: Retrofit savings are the sum of Retirement savings and Lost Opportunity savings. This section presents the Retirement portion of savings while the Lost Opportunity portion of the savings is presented further on in this measure.

Retirement Component:

Use equations in Table 2a to calculate savings. If water heater fuel is unknown, use Table 2b.

Retrofit Gross Energy Savings, Example

What are the savings for a dishwasher installed in an existing home to replace a working unit? The new unit is rated for total energy of 190 kWh/yr and total water use of 2.9 Gallons/cycle. The home has a propane water heater.

Lost Opportunity (use rated Energy and water use for new installed unit):

Claim electric energy savings for the Machine component:

$$AKWH_{M,lost opp} = 126 \frac{kWh}{yr} - [E_i - (36.17 \times GPC_i)]$$

$$AKWH_{M,lost opp} = 126 \frac{kWh}{yr} - [190 - (36.17 \times 2.9)]$$

$$AKWH_{M,lost opp} = 40.89 \frac{kWh}{yr}$$

Claim propane savings for the Water Heating component:

$$APG_{lost opp} = 10.90 \frac{Gal}{yr} - (2.179 \times GPC_i)$$

$$APG_{lost opp} = 10.90 \frac{Gal}{yr} - (2.179 \times 2.9)$$

$$APG_{lost opp} = 4.58 \frac{Gal Propane}{yr}$$

Non energy water savings may be claimed for Lost Opportunity,

$$AWG_{lost opp} = (5.0 \frac{Gal}{cycle} - 2.9) \times 215 \frac{cycles}{yr} = 452 \frac{Gal Water}{yr}$$

Retirement (Deemed):

The Machine energy component is 47 kWh/yr. Propane Water Heater component may be claimed, 1.738 Gal/yr. Non energy water savings may also be claimed, 172 Gal/yr.

Non Energy Benefits (Quantified)

Lost Opportunity Water Savings (all units):

$$AWG_{lost opp} = (GPC_b - GPC_i) \times 215^{cycles} /_{yr}$$
$$AWG_{lost opp} = (5.0^{Gal} /_{cycle} - GPC_i) \times 215^{cycles} /_{yr}$$

Retirement Water Savings (all units):

$$\begin{split} AWG_{retire} &= \left(GPC_e - GPC_b\right) \times 215^{cycles}/_{yr} \\ AWG_{retire} &= \left(5.8 \frac{Gal}{cycle} - 5.0 \frac{Gal}{cycle}\right) \times 215^{cycles}/_{yr} \\ AWG_{retire} &= 172 \frac{Gal}{v_r} \end{split}$$

Changes from Last Version

Updated typical existing unit efficiency level appropriate to measure life. Lost Opportunity is no longer deemed, allowing custom calculation of super-efficient models. Updated water heating fuel mix to match the clothes washer measure. Non energy water savings added. Baseline was changed to the 2013 Federal Standard.

References

- [1] DOE Federal Test Procedure 10 CFR 430, Appendix C, as of June 20, 2011.
- [2] Consortium for Energy Efficiency (CEE) Super Efficient Home Appliances Initiative (SEHA): Dish Washer Specification August 11, 2009.
- [3] Energy Star Program Requirements Product Specification for Dish Washers: Eligibility Criteria, Version 4.1. Effective August 11, 2009.
- [4] Energy Star Program Requirements Product Specification for Dish Washers: Eligibility Criteria, Version 5.0. Effective January 20, 2012.

[5] Federal Register Part III, DOE Energy Conservation Program: Energy Conservation Standards for Residential Water Heaters, Direct Heating Equipment, Pool Heater; Final Rule, Table I.2. April 16, 2010.

- [6] Federal Register 10 CFR Parts 429 and 430, Energy Conservation Program: Energy Conservation Standards for Residential Dishwashers. Published May 30, 2012, effective May 30, 2013. Table I.1.
- [7] Market Impact Analysis on the Potential Revision of the ENERGY STAR Criteria for Dishwashers, June 10, 2005
- [8] Energy Star Criteria for Dishwashers as of March 2, 2006.

Notes

[1] Most of the savings for high efficiency dishwashers come from water heating. When the hot water fuel is unknown, water heating savings are claimed for all fuel types according to the following percentages:

| Water Heater Fuel (typical fuel mix estimated for Connecticut) | | | | | | | |
|--|--------------------------|-----|------|--|--|--|--|
| Electric | Electric Gas Oil Propane | | | | | | |
| 15% | 25.5% | 51% | 8.5% | | | | |

The total savings using this fuel mix are calculated as a percent of savings for known fuels as follows:

$$AKWH_{fuel\ mix} = (100\% \times AKWH_{M}) + (15\% \times AKWH_{W})$$

$$ACCF_{fuel\ mix} = (25.5\% \times ACCF_W)$$

$$AOG_{fuel\ mix} = (51\% \times AOG_W)$$

$$AOG_{fuel\ mix} = (8.5\% \times APG_W)$$

- [2] For E = total rated energy use, a = Water Heater component of usage, b = Machine component of usage, the energy usage is characterized by the equation E = a + b. Each usage component is derived as follows:
 - a. Water Heater Component:

| Water Heating Assumptions (Ref [1]) | | | | | | |
|-------------------------------------|-------------------|-------------|----------------|----------|-----------------------|--|
| % Hot Water | Average Cycles/yr | Temperature | Specific Heat | Water He | ater Efficiency | |
| Supplied | of Dishwasher | Rise | of Water | Electric | Fossil Fuel (Ref [5]) | |
| 100% | 215 | 70°F | 8.2 Btu/Gal-°F | 100% | 62% | |

Estimate Annual Btu energy usage to heat the hot water used by the dishwasher:

Annual Hot Water Btu Usage =
$$100\% \times 215^{Cycles}/_{vr} \times 8.2^{Btu}/_{Gal-\circ F} \times 70^{\circ}F \times GPC_W$$

Annual Hot Water Btu Usage =
$$123,410^{Btu-cycles}/Gal-vr \times GPC_W$$

Using the following equation to convert annual Hot Water energy from Btu to each fuel type:

$$Annual Water Heating Usage = \frac{Annual Hot Water Btu Usage}{Fuel Conversion \frac{Btu}{wnit} \times EF}$$

Electric Water Heater usage:

Annual Electric Water Heating Usage,
$$kWh = \frac{123,410 \times GPC_W}{3412 \frac{Btu}{kWh}}$$

Annual Electric Water Heating Usage, $kWh = 36.17 \times GPC_W$

Gas Water Heater usage:

Annual Gas Water Heating Usage =
$$\frac{123,410 \times GPC_W}{102,900^{Btu}/_{Cof} \times 0.62}$$

Annual Gas Water Heating Usage = $1.934 \times GPC_W$

Oil Water Heater usage:

Annual Oil Water Heating Usage =
$$\frac{123,410 \times GPC_W}{138,690^{Btu}/_{Gal~Oil} \times 0.62}$$

Annual Oil Water Heating Usage = $1.435 \times GPC_W$

Propane Water Heater usage:

Annual Propane Water Heating Usage =
$$\frac{123,410 \times GPC_W}{91,330^{Btu}/_{Gal\ Propane} \times 0.62}$$

Annual Propane Water Heating Usage = $2.179 \times GPC_w$

b. Machine Component:

Estimate electric Machine energy use (b) by subtracting the water heating energy in kWh (a) from the unit's total rated kWh usage (E)

Annual Machine kWh Usage =
$$E - (36.17 \, \frac{\text{kWh}}{\text{Gal-vr}} \times GPC_W)$$

- [3] The Lost Opportunity baseline unit is represented by the 2013 Federal Standard (Ref [6]). Baseline Energy usage for the Machine and Water Heater Components is shown in Table 3.
- [4] Energy Factor (EF) was not rated until the 1994 Federal Standard. The Maximum Energy and Water Use criteria replaced the EF in the 2009 Energy Star criteria, and the 2010 Federal Standard followed suit. The annual kWh energy use criterion differs from the EF in that it also includes standby energy use. The approximate relationship

between the two types of criteria is (standby power use additional to this): Annual kWh Energy Use = $\frac{215 \frac{cycles}{yr}}{EF}$

The typical existing unit is represented the 2001 Energy Star level at 0.58 EF, based on high market penetration in 2004 (Ref [7]), with equivalent energy use of 371 kWh/yr. Because there was no specification for water use prior to 2009, the typical existing unit water usage is estimated to be the same as the 2009 Energy Star (5.8 Gal/cycle) level.

Table 3: Energy Specifications and Usage Components (values in brackets are estimated)

| Level (with effective date) | EF | Total | Hot | Energy Usage Components R | | | | Ref | |
|------------------------------------|------|--------|--------|---|---------------------|-------|-------|---------|-----|
| | | Energy | Water | (Calculated from equations in Note [2]) | | | | 2]) | |
| | | Use | Use | Machine | chine Water Heating | | | | |
| | | Rating | Rating | Energy | Electric | Gas | Oil | Propane | |
| | N/A | kWh/yr | Gal/ | kWh/yr | kWh/yr | Ccf/ | Gal/ | Gal/ yr | |
| | | | Cycle | | | yr | yr | | |
| May 14, 1994 Federal Standard | 0.46 | [467] | [7.3] | 203 | 264 | 14.12 | 10.48 | 15.91 | [8] |
| Jan 1, 2001 Energy Star (existing) | 0.58 | [371] | [5.8] | 161 | 210 | 11.22 | 8.323 | 12.64 | [8] |
| 2007 Energy Star | 0.65 | [331] | [5.8] | 121 | 210 | 11.22 | 8.323 | 12.64 | [8] |
| 2010 Federal Standard | N/A | 355 | 6.5 | 120 | 235 | 12.57 | 9.328 | 14.16 | [2] |
| 2009 Energy Star | N/A | 324 | 5.8 | 114 | 210 | 11.22 | 8.323 | 12.64 | [3] |
| 2013 Federal Standard | N/A | 307 | 5.0 | 126 | 181 | 9.670 | 7.175 | 10.90 | [6] |
| 2012 Energy Star | N/A | 295 | 4.25 | 141 | 154 | 8.220 | 6.099 | 9.261 | [4] |
| 2012 CEE Tier 1 | 0.75 | 295 | 4.25 | 141 | 154 | 8.220 | 6.099 | 9.261 | [2] |

4.3.9 REFRIGERATOR

Description of Measure

Savings detailed below cover the replacement of a full size refrigerator with a new energy efficient model, the installation of an energy efficient refrigerator in a new home, and the permanent removal of a non-primary refrigerator from service

Savings Methodology

Lost Opportunity Measure:

- Lost Opportunity savings are the difference in energy use between a baseline new model (Note [4]) of the same size and category as the installed unit, and the chosen high efficiency new model, continuing for the Effective Useful Life (EUL) from Appendix 4.
- The Retail measure is a Lost Opportunity-only methodology, as the existing unit is not verified.
- The Energy Star New Home measure is a special Lost-Opportunity-only measure, where the 2008 Energy Star level is used as the baseline.

Retrofit Measure:

- Uses the same methodology as a Lost Opportunity measure.
- In the case of early retirement of a working unit where the unit would have otherwise been installed until failure, lifetime "Retirement" savings are claimed additional to the lifetime "Lost Opportunity" savings (see Section 1.4).
- Retirement savings are the difference in energy use between the older unit (Note [1]) and a baseline new model (Note [4]) of the same size and category as the older unit, continuing for the Remaining Useful Life (RUL) from Appendix 4. See Note [5] for exceptions.
- The Turn-in measure (permanent removal of a working non-primary unit that will not be replaced with a new unit) is a special case where savings are claimed as the existing unit's rated annual energy usage (Note [1]).

Only Full-Sized Refrigerators are considered in this measure (Total volume of 7.75 cubic feet or greater). The efficiency of a refrigerator model is rated on the annual energy usage in kWh, which varies according to size, configuration, and features. A "Site/Lab Factor" (Ref [1], pages 7-2 and 7-3) is applied to the consumption for each newer unit (from 2004 on) before taking the difference between energy usage levels for savings calculations.

Inputs

| Symbol | Description | Required for |
|---------------------------|--|---------------------------------------|
| AV_i | Adjusted Volume of new installed unit | Lost Opportunity |
| E_{e} | Actual unadjusted rated kWh energy usage for the existing unit | Retirement |
| $\mathbf{E}_{\mathbf{i}}$ | Actual rated kWh energy usage for the new installed unit | Lost Opportunity |
| V_{e} | Total Nominal Volume of existing unit | Retirement |
| Year _e | Year of existing (old) model | Retirement – only if usage is unknown |
| | Category of existing refrigerator (See Table 1 for options) | Retirement |
| | Category of new refrigerator (See Table 1 for options) | Lost Opportunity |
| | Brand and Model of existing refrigerator | Retirement |
| | Brand and Model of new installed refrigerator | Lost Opportunity |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|--------------------------|---------------------------------------|--------|------------|----------|
| AKWH _{retire} | Gross annual Retirement savings | kWh/yr | Calculated | |
| AKWH _{lost opp} | Gross annual Lost Opportunity savings | kWh/yr | Calculated | |
| AKWH _{turn-in} | Gross annual Turn-in savings | kWh/yr | Calculated | |

| Symbol | Description | Units | Values | Comments |
|-----------------------|--|-----------------|------------------------|--------------|
| AV_i | Adjusted Volume of new installed unit | ft ³ | Actual as rated | Note [3] |
| AV_e | Adjusted Volume of existing unit | ft ³ | | Note [2] |
| E_b | Electric energy usage of baseline new unit, | kWh/yr | New Home: | Note [4], |
| | calculated separately for 'Retirement' and 'Lost | | 2008 Energy Star | Table [2] |
| | Opportunity' | | All Others: | |
| | | | 2004 Energy Star | |
| E _e | Unadjusted electric energy usage of existing unit | | | Note [1] |
| E _{fed std} | Electric energy usage of 2001 Federal Standard | kWh/yr | Calculated separately | Note [4], |
| | unit, varies according to size and category | | for 'Retirement' and | Table 1, |
| | | | 'Lost Opportunity' | Ref [9] |
| E_{i} | Electric energy usage of new installed unit | kWh/yr | Calculated | |
| EUL | Effective Useful Life: Measure life of installed unit. | years | Appendix 4 | |
| LKWH _{total} | Total gross lifetime electric energy savings | kWh | Calculated | |
| PF_S | Summer Peak Factor | W/ kWh | 0.1834 | Ref [1] |
| PF_W | Winter Peak Factor | W/ kWh | 0.1031 | Ref [1] |
| RUL | Remaining Useful Life: remaining number of years | years | Appendix 4 | |
| | the existing unit would have operated until failure | | | |
| SKW | Summer electric demand savings | kW | | |
| SLF_{new} | Site/Lab Factor, an adjustment for DOE test lab | | 0.881 | Ref [1], Ref |
| | performance of new refrigerators to in situ | | | [2] |
| | performance | | | |
| V _e | Total Nominal Volume of existing unit | ft ³ | Actual as found | |
| WKW | Winter electric demand savings | kW | | |
| Year _e | Year of Manufacture of existing unit | Yr | Actual; if unknown, | Note [1] |
| | | | estimate based on age. | |
| ···retire | Associated with Retirement | | | |
| ···lost opp | Associated with Lost Opportunity | | | |
| · · · turn-in | Associated with Turn-in Program | | | |

Lost Opportunity Gross Energy Savings, Electric

New Home:

- Select the equation for E_{fed std} for the new installed unit's configuration from Table 1 in Note [4], and use AV_i in this equation.
- Calculate the baseline energy usage at the Energy Star 2008 level from Table 2: $E_{b, retire} = E_{fed \ std} \times 0.80$
- Use this and the rated energy usage of the new installed unit (Note [4]) in the following equation: $AKWH_{lost\,opp} = 0.881 \times \left(E_{b,\,lost\,opp} E_i\right)$

All Others:

- Select the equation for $E_{\text{fed std}}$ for the new installed unit's configuration from Table 1, and use AV_i in this equation.
- Calculate the baseline energy usage at the Energy Star 2004 level from Table 2: $E_{b, retire} = E_{fed \ std} \times 0.85$
- Use this and the rated energy usage of the new installed unit (Note [4]) in the following equation: $AKWH_{lost opp} = 0.881 \times \left(E_{b,lost opp} E_i\right)$

Note: The equation for Lost Opportunity was derived from the following difference in energy usage: $AKWH_{lost\ opp} = (SLF_{new} \times E_{b,lost\ opp}) - (SLF_{new} \times E_{i})$

Lost Opportunity Gross Energy Savings, Example

Example 1. A new 25.25 ft³ refrigerator with a side-by-side configuration, automatic defrost, and through-the-door ice service is purchased through a retail promotion. The Energy Star lists Adjusted Volume of 31.3925 ft³, and rated annual energy usage of 469 kWh/yr. What are the energy savings?

Select the appropriate equation from Table 1 and calculate $E_{\text{fed std}}$ for Lost Opportunity (Note [4]) using AV_i (Note [3]): $E_{\text{fed std,lost opp}} = (10.1 \times AV_i) + 406$

$$E_{fed\ std,lost\ opp} = \left(10.1 \times 31.3925\ ft^3\right) + 406 = 723\ kWh$$

Use this to calculate $E_{b, lost opp}$ (Note [4]):

$$E_{b,lost \ opp} = E_{fed \ std,lost \ opp} \times 0.85 = 723 \, \frac{kWh}{yr} \times 0.85 = 615 \, \frac{kWh}{yr}$$

Using the Lost Opportunity equation for annual energy savings, $AKWH_{lost\,opp} = 0.881 \times \left(E_{b,\,lost\,opp} - E_i\right)$

$$AKWH_{lost opp} = 0.881 \times (615 \, \frac{kWh}{vr} - 469 \, \frac{kWh}{vr}) = 128 \, \frac{kWh}{vr}$$

Example 2. A 25.25 ft³ refrigerator with a side-by-side configuration, automatic defrost, and through-the-door ice service is installed in an Energy Star New Home. Energy Star lists Adjusted Volume of 31.3925 ft³, and rated annual energy usage of 469 kWh/yr. What are the energy savings?

Select the appropriate equation from Table 1 and calculate $E_{\text{fed std}}$ for Lost Opportunity (Note [4]) using AV_i (Note [3]):

$$E_{fed\ std,lost\ opp} = (10.1 \times AV_i) + 406$$

$$E_{fed, std, lost, opp} = (10.1 \times 31.3925 \, ft^3) + 406 = 723 \, kWh$$

Use this to calculate $E_{b, lost opp}$ (Note [4]):

$$E_{b, lost opp} = E_{fed \ std, lost opp} \times 0.80 = 723 \, \frac{kWh}{yr} \times 0.80 = 578.4 \, \frac{kWh}{yr}$$

Using the Lost Opportunity equation for annual energy savings, $AKWH_{lost opp} = 0.881 \times (E_{b, lost opp} - E_i)$

$$AKWH_{lost opp} = 0.881 \times (578.4 \, \frac{kWh}{yr} - 469 \, \frac{kWh}{yr}) = 96 \, \frac{kWh}{yr}$$

Lost Opportunity Gross Peak Demand Savings, Electric, Winter and Summer

Use the annual energy savings calculated for lost opportunity in the following equations:

$$WKW_{lost\,opp} = AKWH_{lost\,opp} \times PF_W \left/ 1000^W \right/_{kW}$$

$$SKW_{lost \, opp} = AKWH_{lost \, opp} \times PF_S / 1000 \frac{W}{kW}$$

Lost Opportunity Gross Peak Demand Savings, Example

Example 3. A new 25.25 ft³ refrigerator with a side-by-side configuration, automatic defrost, and through-the-door ice service is purchased through a retail promotion. Energy Star lists Adjusted Volume of 31.3925 ft³, and rated annual energy usage of 469 kWh/yr. Calculate demand savings using the results of Example 1.

$$WKW_{lost \, opp} = AKWH_{lost \, opp} \times PF_W / 1000 \frac{W}{kW}$$

$$WKW_{lost opp} = 128 \, kWh/_{vr} \times 0.1031/1000 \, W/_{kW} = 0.0132 \, kW$$

$$SKW_{lost \, opp} = AKWH_{lost \, opp} \times PF_S / 1000 \frac{W}{kW}$$

$$SKW_{lost opp} = 128 \frac{kWh}{yr} \times 0.1834 / 1000 \frac{W}{kW} = 0.0235 kW$$

Example 4. A 25.25 ft³ refrigerator with a side-by-side configuration, automatic defrost, and through-the-door ice service is installed in an Energy Star New Home. Energy Star lists Adjusted Volume of 31.3925 ft³, and rated annual energy usage of 469 kWh/yr. Calculate demand savings using the results of Example 2.

$$WKW_{new home} = 96 \frac{kWh}{yr} \times 0.1031 / 1000 \frac{W}{kW} = 0.0099 \ kW$$
$$SKW_{new home} = 96 \frac{kWh}{yr} \times 0.1834 / 1000 \frac{W}{kW} = 0.0177 \ kW$$

Retrofit Gross Energy Savings, Electric

Reminder: Retrofit savings are the sum of Retirement savings and Lost Opportunity savings. This section presents the Retirement portion of savings while the Lost Opportunity portion of the savings is presented further on in this measure.

To obtain the lifetime savings, the following formula should be used:

$$LKWH_{C, Total} = AKWH_{C, Retire} \times RUL + AKWH_{C, Lost Opp} \times EUL$$

Retirement Component:

- Estimate AV_e based on the volume of the existing unit (Note [2]): $AV_e = (1.319 \times V_e) 2.491$
- Select the equation for $E_{\text{fed std}}$ for the existing unit's configuration from Table 1, and use AV_e in the equation.
- Calculate the baseline energy usage: $E_{b, retire} = E_{fed \ std} \times 0.85$
- Use this and the rated energy usage of the existing unit (Note [1]) in the following equation: $AKWH_{retire} = E_e (0.881 \times E_{b.retire})$

Note: The equation for Retirement was derived from the following difference in energy usage: $AKWH_{retire} = E_e - (SLF_{new} \times E_{b, retire})$

Turn-in measure:

$$AKWH_{turn-in} = E_e$$

Retrofit Gross Energy Savings, Example

Example 5. Calculate energy savings for replacing a 1998 model in working condition in an existing home if the rated energy usage of the existing model is known, 683 kWh/yr. The existing model has a total volume of 18.00 ft³ with a top-mount freezer and without through-the-door ice service. The new installed model is an 18.11 ft³ Refrigerator with top-mount freezer and automatic defrost without through-the-door ice service. The Energy Star website lists Adjusted Volume of 20.7686 ft³ and rated annual energy use of 311 kWh/yr.

Lost Opportunity Component:

• Select the appropriate equation from Table 1:

$$E_{fed\ std,lost\ opp} = (9.8 \times AV_i) + 276$$

• Calculate E_{fed std} using AV_i:

$$E_{fed\ std,lost\ opp} = (9.8 \times 20.7686 \, ft^3) + 276 = 480 \, kWh$$

• Use $E_{\text{fed std, lost opp}}$ to calculate baseline energy usage, $E_{\text{b, lost opp}}$: $E_{b, lost opp} = E_{\text{fed std, lost opp}} \times 0.85 = 480 \, \frac{\text{kWh}}{\text{yr}} \times 0.85 = 408 \, \frac{\text{kWh}}{\text{yr}}$

$$AKWH_{lost opp} = 0.881 \times (E_{b, lost opp} - E_i)$$

$$AKWH_{lost opp} = 0.881 \times (408 \, {}^{kWh}/_{yr} - 311 \, {}^{kWh}/_{yr}) = 85 \, {}^{kWh}/_{yr}$$

Retirement Component:

• Calculate Adjusted Volume using the total volume of the existing unit: $AV_e = (1.319 \times V_e) - 2.491$ $AV_e = (1.319 \times 18.00 \text{ ft}^3) - 2.491 = 21.251 \text{ ft}^3$

 $\bullet \quad \text{Select the appropriate equation from Table 1 and calculate } E_{\text{fed std}} \text{ for Retirement using } AV_e; \\$

$$E_{fed\ std.\ retire} = (9.8 \times AV_e) + 276 = (9.8 \times 21.251 ft^3) + 276 = 484 \, kWh$$

• Use $E_{\text{fed std, retire}}$ to calculate baseline energy usage, $E_{\text{b, retire}}$, at the 2004 Energy Star level: $E_{\text{b, retire}} = E_{\text{fed std, retire}} \times 0.85 = 484 \frac{\text{kWh}}{\text{vr}} \times 0.85 = 412 \frac{\text{kWh}}{\text{vr}}$

• Use the equation for Retirement savings input the rated existing unit usage and the calculated baseline usage: $AKWH_{retire} = E_e - (0.881 \times E_{b, retire})$ $AKWH_{retire} = 683 \frac{kWh}{v_r} - (0.881 \times 412 \frac{kWh}{v_r}) = 320 \frac{kWh}{v_r}$

Example 6. Calculate energy savings for replacing a 1998 model in working condition in an existing home if the rated energy usage of the existing model is unknown. The existing model has a total volume of 18.00 ft³ with a top-mount freezer and without through-the-door ice service. The new installed model is an 18.11 ft³ Refrigerator with top-mount freezer and automatic defrost without through-the-door ice service. The Energy Star website lists Adjusted Volume of 20.7686 ft³ and rated annual energy use of 311 kWh/yr.

Because the existing unit is verified to be in working condition, the retrofit savings are made up of both a Lost Opportunity component and an Early Retirement component.

Lost Opportunity Component:

Lost Opportunity savings are the same as Example 5, $AKWH_{lost opp} = 85 \frac{kWh}{\gamma r}$.

Retirement Component:

The Retirement calculation is the same as previous except the last step; E_e must be estimated based on the age of the existing unit (per Note [1]):

$$E_{b, retire} = 412 \, \frac{kWh}{yr}$$

$$E_e = V_e \times (4440.6 - (2.2035 \times Year_e))$$

$$E_e = 18.00 \, \text{ft}^3 \times (4440.6 - (2.2035 \times 1998)) = 684 \, \frac{kWh}{yr}$$

Input the estimated existing unit usage and the calculated baseline usage:

$$AKWH_{retire} = E_e - (0.881 \times E_{b, retire})$$

 $AKWH_{retire} = 684 \frac{kWh}{vr} - (0.881 \times 412 \frac{kWh}{vr}) = 321 \frac{kWh}{vr}$

Example 7. Calculate energy savings for removing a 1998 model in working condition from service through a Turn-in program if the rated energy usage of the existing model is known (683 kWh/yr) and the unit is a second unit that will not be replaced by a new unit. The unit has a total volume of 18.00 ft³ with a top-mount freezer and without through-the-door ice service.

Gross Annual savings for removing the unit from operation are 683 kWh/yr.

Retrofit Gross Peak Demand Savings, Electric, Winter and Summer

Reminder: Retrofit savings are the sum of Retirement savings and Lost Opportunity savings. This section presents the Retirement portion of savings while the Lost Opportunity portion of the savings is presented further on in this measure.

Retirement Component

$$WKW_{retire} = AKWH_{retire} \times PF_W / 1000 \frac{W}{kW}$$

 $SKW_{retire} = AKWH_{retire} \times PF_S / 1000 \frac{W}{kW}$

Turn-in:

$$WKW_{turn-in} = AKWH_{turn-in} \times PF_W / 1000 \frac{W}{kW}$$

 $SKW_{turn-in} = AKWH_{turn-in} \times PF_S / 1000 \frac{W}{kW}$

Retrofit Gross Peak Demand Savings, Example

Example 8. Using the results of Example 5, calculate demand savings for replacing a 1998 model in working condition in an existing home if the rated energy usage of the existing model is known, 683 kWh/yr. The existing model has a total volume of 18.00 ft³ with a top-mount freezer and without through-the-door ice service. The new installed model is an 18.11 ft³ Refrigerator with top-mount freezer and automatic defrost without through-the-door ice service. The Energy Star website lists Adjusted Volume of 20.7686 ft³ and rated annual energy use of 311 kWh/yr.

Because the existing unit is verified to be in working condition, the retrofit savings are made up of both a Lost Opportunity component and an Early Retirement component.

Lost Opportunity Component:

$$WKW_{lost opp} = AKWH_{lost opp} \times PF_W / 1000 \frac{W}{kW}$$

$$WKW_{lost opp} = 85 \frac{kWh}{y_r} \times 0.1031 / 1000 \frac{W}{kW} = 0.0088 kW$$

$$SKW_{lost opp} = AKWH_{lost opp} \times PF_S / 1000 \frac{W}{kW}$$

$$SKW_{lost opp} = 85 \frac{kWh}{y_r} \times 0.1834 / 1000 \frac{W}{kW} = 0.0156 kW$$

Retrofit Component:

$$WKW_{retire} = 320 \frac{kWh}{yr} \times 0.1031/1000 \frac{W}{kW} = 0.0330 kW$$

 $SKW_{retire} = 320 \frac{kWh}{yr} \times 0.1834/1000 \frac{W}{kW} = 0.0587 kW$

Example 9. Using the results of Example 6, calculate demand savings for replacing a 1998 model in working condition in an existing home if the rated energy usage of the existing model is unknown. The existing model has a total volume of 18.00 ft³ with a top-mount freezer and without through-the-door ice service. The new installed model is an 18.11 ft³ Refrigerator with top-mount freezer and automatic defrost without through-the-door ice service. The Energy Star website lists Adjusted Volume of 20.7686 ft³ and rated annual energy use of 311 kWh/yr. (Unknown Existing Usage)

Because the existing unit is verified to be in working condition, the retrofit savings are made up of both a Lost Opportunity component and an Early Retirement component

Lost Opportunity Component:

$$WKW_{lost opp} = 0.0088 kW$$
$$SKW_{lost opp} = 0.0156 kW$$

Retrofit Component:

$$WKW_{retire} = 321^{kWh}/_{yr} \times 0.1031/1000^{W}/_{kW} = 0.0331 \, kW$$

 $SKW_{retire} = 321^{kWh}/_{yr} \times 0.1834/1000^{W}/_{kW} = 0.0589 \, kW$

Example 10. Using the results of Example 7, calculate demand savings for removing a 1998 model in working condition from service through a Turn-in program if the rated energy usage of the existing model is known (683 kWh/yr) and the unit is a second unit that will not be replaced by a new unit. The unit has a total volume of 18.00 ft³ with a top-mount freezer and without through-the-door ice service.

$$\begin{aligned} WKW_{turn-in} &= AKWH_{turn-in} \times PF_W / 1000W_{kW} \\ WKW_{turn-in} &= 683 \, \frac{kWh}{y_T} \times 0.1031 / 1000W_{kW} = 0.0704 \, kW \\ SKW_{turn-in} &= AKWH_{turn-in} \times PF_S / 1000W_{kW} \\ SKW_{turn-in} &= 683 \, \frac{kWh}{y_T} \times 0.1834 / 1000W_{kW} = 0.1253 \, kW \end{aligned}$$

Changes from Last Version

Rearranged presentation to facilitate clear definition of lost opportunity and retrofit. Provided equations to estimate existing values in the case of unknowns; kWh is based on age and nominal size, and AV is based on nominal size. Examples have been refreshed. Turn-in program and New Home savings added.

References

- [1] KEMA, Evaluation of the Weatherization Residential Assistance Partnership and Helps Programs (WRAP/Helps), September 10, 2010
- [2] Blasnik, Michael, Proctor Engineering Group Limited, Michael Blasnik & Associates, and Conservation Services Group. Measurement and Verification of Residential Refrigerator Energy Use: Final Report, 2003-2004 Metering Study. July 29, 2004.
- [3] Energy Star Program Requirements Product Specification for Residential Refrigerators and Freezers: Eligibility Criteria, Version 4.1. Effective April 28, 2008.
- [4] Consortium for Energy Efficiency (CEE) Super-Efficient Home Appliances Initiative (SEHA) High-efficiency Specifications for Refrigerators, Effective Jan 1, 2007.
- [5] California Energy Commission (CEC) Appliance Database.

 Online historical appliance database: http://www.energy.ca.gov/appliances/database/historical_excel_files/
 Online current (meeting minimum standards) appliance database: http://www.appliances.energy.ca.gov/
- [6] Energy Star Residential Refrigerators and Freezers Specification: Website tracking proposed draft Energy Star Version 5.0 specification. http://www.energystar.gov/index.cfm?c=revisions.res_refrig_spec. Last Accessed July 25, 2012. Proposed Effective date: January 1, 2013.
- [7] Federal Register, Vol. 76, No. 179. 10 CFR Part 430. Energy Conservation Program: Energy Conservation Standards for Residential Refrigerators, Refrigerator-Freezers, and Freezers. Published September 15, 2011, Effective November 14, 2011, Compliance date September 15, 2014.
- [8] Energy Star Refrigerators Website, last accessed July 25, 2012: http://www.energystar.gov/index.cfm?fuseaction=find_a_product.showProductGroup&pgw_code=RF
- [9] Federal Register Part IX, 10 CFR Part 430, Vol. 63, No. 81, Energy Conservation Program for Consumer Products: Energy Conservation Standards for Refrigerators, Refrigerator-Freezers and Freezers; Final Rule. Published Monday, April 28, 1997. Effective July 1, 2001.

Notes

[1] The unadjusted annual energy usage of the existing unit can usually be found in the CEC database (Ref [5]) or equivalent source by brand and model number.

If the existing unit kWh usage is unknown, it may be estimated with the following equation, using the nominal total volume of the unit and the estimated year of manufacture

For units from 1978 and newer:

$$E_e = V_e \times (4440.6 - (2.2035 \times Year_e))$$

Units prior to 1978 are to be capped at:

$$E_e = V_e \times \left(82 \, \frac{kWh}{ft^3}\right)$$

This equation is based on average rated usage of full size standard refrigerators found in the CEC Database (Ref [5]) from 1978 to 2003.

- [2] The definition of Adjusted Volume is the following equation: $AV = V_{fresh} + (1.63 \times V_{frozen})$, where fresh refers to the main refrigerator compartment, and frozen refers to the freezer compartment. Adjusted Volume of the existing unit may be estimated using the following: an analysis of data from Ref [5] showed the following strong relationship between Volume and Adjusted Volume for standard size Refrigerator-Freezer units: $AV_e = (1.319 \times V_e) 2.491$. For All-Refrigerators, the Adjusted Volume (AV) is the same as the nominal volume (no freezer compartment).
- [3] Energy use and Adjusted Volume ratings for new installed Energy Star units may be obtained through the Energy Star website, Ref [8]. Because of the complexity of the 2013 Energy Star Version 5.0 specification (Ref [6]) and 2014 Federal Standard (Ref [7]), the details of these specifications are not listed here but may be obtained directly from the final reference documents.
- [4] The baseline new model is represented by the 2004 Energy Star level, using the equation in Table 2 applied to the Federal Standard found in Table 1. Because in many cases the installed energy efficient unit does not share the same size and category as the existing unit, the Federal Standard level (E_{fed std}) must be calculated separately for Lost Opportunity (using the Adjusted Volume and category of the installed unit) and Retirement (using the Adjusted Volume and category of the existing unit), using equations found in Table 1. In the special case of an Energy Star New Home, the baseline new model is represented by the 2008 Energy Star level (using the equation in Table 2) with the same Adjusted Volume and category as the installed unit.

Table 1: 2001 Federal Standard Energy Use (Based on Size), in kWh/yr, for Full-Size Refrigerators (Ref [9])

| Configuration | Defrost | Through-the-Door Ice | $\mathbf{E}_{fed\;std}$ |
|--|-------------------|----------------------|-------------------------|
| Any | Manual | Any | 8.82*AV+248.4 |
| Any | Partial Automatic | Any | 8.82*AV+248.4 |
| All-Refrigerator (No Frozen Compartment) | Automatic | Any | 9.8*AV+276 |
| Top Mount Freezer | Automatic | No | 9.8*AV+276 |
| Side Mount Freezer | Automatic | No | 4.91*AV+507.5 |
| Bottom Mount Freezer | Automatic | No | 4.6*AV+459 |
| Top Mount Freezer | Automatic | Yes | 10.2*AV+356 |
| Side Mount Freezer | Automatic | Yes | 10.1*AV+406 |
| Bottom Mount Freezer | Automatic | Yes | 5.0*AV+539.0 |

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Table 2: Energy Specifications based on 2001 Federal Standard

| Table 21 Energy Specifications waste on 2001 1 tuestar Standard | | | | |
|---|--------------------------|----------------------------------|-----------|--|
| Specification | %< 2001 Federal Standard | Maximum Energy Usage, E (kWh/yr) | Reference | |
| 2004 Energy Star | 15% | $E = E_{fed \ std} \times 0.85$ | [3] | |
| 2008 Energy Star | 20% | $E = E_{fed \ std} \times 0.80$ | [3] | |
| CEE Tier 2 | 25% | $E = E_{fed\ std} \times 0.75$ | [4] | |
| CEE Tier 3 | 30% | $E = E_{fed \ std} \times 0.70$ | [4] | |

- [5] Exceptions to standard calculations for replacement of existing units may occur in the following special situations:
 - a. If the annual kWh usage of the existing unit is already less than or equal to the baseline level $(E_e \le E_b)$, no retirement savings may be claimed.
 - b. If the annual kWh usage of existing unit is less than the baseline level but greater than the annual kWh usage of the new installed unit ($E_i < E_e < E_b$), the lost opportunity component of savings may still be claimed, but the existing unit Annual kWh usage must be used for the baseline rather than Energy Star 2004.
 - c. If new unit Annual kWh is greater than or equal to the existing unit kWh $(E_e \le E_i)$, regardless of size, no savings may be claimed.

4.3.12 FREEZER

Description of Measure

Savings detailed below cover the replacement of a full size freezer with a new energy efficient model, the installation of an energy efficient freezer in a new home, and the permanent removal of a freezer from service.

Savings Methodology

Lost Opportunity Measure:

- Lost Opportunity savings are the difference in energy use between a baseline new model (Note [2]) of the same size and category as the installed unit, and the chosen high efficiency new model (Note [4]), continuing for the Effective Useful Life (EUL) from Appendix 4.
- The Retail measure is a Lost Opportunity-only methodology, as the existing unit is not verified.
- The Energy Star New Home measure is a special Lost-Opportunity-only measure, where the current Energy Star level is used as the baseline.

Retrofit Measure:

- Uses the same methodology as a Lost Opportunity measure.
- In the case of early retirement of a working unit where the unit would have otherwise been installed until failure, lifetime "Retirement" savings are claimed additional to the lifetime "Lost Opportunity" savings (see Section 1.4).
- Retirement savings are the difference in energy use between the older unit (Note [1]) and a baseline new model (Note [2]) of the same size and category as the older unit, continuing for the Remaining Useful Life (RUL) from Appendix 4. See Note [3] for exceptions.
- The Turn-in measure (permanent removal of a working non-primary unit that will not be replaced with a new unit) is a special case where savings are claimed as the existing unit's rated annual energy usage (Note [1]).

Only Full-Sized Freezers are considered in this measure (Total volume of 7.75 cubic feet or greater). The efficiency of a freezer model is rated on the annual energy usage in kWh, which varies according to size, configuration, and features (See Note [3]). Savings are calculated as the difference in unadjusted rated annual energy usage between two levels.

Inputs

| Symbol | Description | Required for |
|-------------------|---|---------------------------------------|
| E _e | Actual (unadjusted) rated kWh consumption of (old) existing model | Retirement |
| E_{i} | Actual rated kWh consumption of new installed model | Lost Opportunity |
| V_{e} | Volume of existing (old) model | Retirement |
| Vi | Volume of new installed model | Lost Opportunity |
| Year _e | Year of existing (old) model | Retirement – only if usage is unknown |
| | Category of existing freezer (See Table 1 for options) | Retirement |
| | Category of new installed freezer (See Table 1 for options) | Lost Opportunity |
| | Brand and Model of existing freezer | Retirement |
| | Brand and Model of new installed freezer | Lost Opportunity |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|-----------------|--|-----------------|--------------------------|----------|
| AV _e | Adjusted Volume of existing model | ft ³ | $AV_e = 1.73 \times V_e$ | |
| AV_i | Adjusted Volume of new installed model | ft ³ | $AV_i = 1.73 \times V_i$ | |
| V _e | Total volume of existing model | ft^3 | Actual | |
| V_{i} | Total volume of new installed model | ft^3 | Actual | |

| Symbol | Description | Units | Values | Comments |
|----------------------|--|--------|----------------------------------|-----------|
| E _b | Annual electric energy usage of baseline new unit | kWh/yr | New Home: E _{ES 2008} | Note [2], |
| | | | All Others: E _{fed std} | Table 1 |
| E_{e} | Annual electric energy usage of existing model | kWh/yr | Actual | Note [1] |
| E _{ES 2013} | Electric energy usage of Proposed 2013 Energy Star | kWh/yr | Calculated | Table 1 |
| | Version 5.0 unit, varies according to size and | | | |
| | category | | | |
| $E_{\text{fed std}}$ | Electric energy usage of Federal Standard unit, | kWh/yr | Calculated separately | Table 1 |
| | varies according to size and category | | for "Retirement" and | |
| | | | "Lost Opportunity" | |
| E_{i} | Electric energy usage of new installed unit | kWh/yr | As rated | |
| AKWH | Gross annual electric energy savings | kWh/yr | Calculated | |
| WKW | Winter electric demand savings | kW | | |
| SKW | Summer electric demand savings | kW | | |
| PF_S | Summer Peak Factor | W/ kWh | 0.1834 | Ref [1] |
| PF _W | Winter Peak Factor | W/ kWh | 0.1031 | Ref [1] |
| · · · turn-in | Associated with Turn-in Program | | | |
| · · · lost opp | Associated with Lost Opportunity | | | |
| ···retire | Associated with Retirement | | | |

Lost Opportunity Gross Energy Savings, Electric

New Home:

- Convert installed volume (V_i) into Adjusted Volume: $AV_i = 1.73 \times V_i$.
- Select the equation for $E_{ES\ 2008}$ for the new installed unit's configuration from Table 1 in Note [2], and use AV_i in this equation. This is the baseline level, $E_{b,\ lost\ opp}$.
- Then take the energy usage difference between the baseline and installed unit: $AKWH_{lost opp} = E_{b, lost opp} E_i$

All Others:

- Convert installed volume (V_i) into Adjusted Volume: $AV_i = 1.73 \times V_i$.
- Select the $E_{\text{fed std}}$ equation for the category of the new installed unit from Table 1 in Note [2] and use AV_i in the equation. This is the baseline level, $E_{b, \text{ lost opp}}$.
- Then take the energy usage difference between the baseline and installed unit: $AKWH_{lost\ opp} = E_{b,lost\ opp} E_i$

Lost Opportunity Gross Energy Savings, Example

Example 1. Calculate savings for a 16.0 cubic foot upright freezer with manual defrost purchased through a retail promotion. Rated energy usage is 409 kWh/yr.

Convert the volume into Adjusted Volume (or obtain from Energy Star): $AV_i = 1.73 \times V_i = 27.68 \text{ ft}^3$

The Retail baseline is at the 2001 Federal Standard; select the equation for the category of the (new) installed unit from Table 1 and calculate the baseline:

$$E_{b, lost opp} = 7.55 \times AV_i + 258.3$$

 $E_{b, lost opp} = 7.55 \times 27.68 \text{ ft}^3 + 258.3 = 467 \text{ kWh/yr}$

Then calculate savings as the difference between the baseline and the installed unit:

$$AKWH_{lost opp} = E_{b,lost opp} - E_i$$

$$AKWH_{lost opp} = 467 \frac{kWh}{yr} - 409 \frac{kWh}{yr} = 58 \frac{kWh}{yr}$$

Example 2. Calculate savings for an 8.5 cubic foot upright freezer with automatic defrost installed in an Energy Star New Home. Rated energy usage is 370 kWh/yr.

Convert the volume into Adjusted Volume (or obtain from Energy Star): $AV_i = 1.73 \times V_i = 14.705 \text{ ft}^3$ Obtain rated energy usage from either label or Energy Star:

The New Home baseline is at the 2008 Energy Star level (Note [4]); select the equation for the category of the (new) installed unit from the specification and calculate the baseline:

For Upright Freezers with Automatic Defrost:

$$E_{ES\ 2008} = (11.19 \times AV) + 293.5$$

 $E_{b,lost\ opp} = (11.19 \times 14.705) + 293.5 = 458.0^{kWh}/_{vr}$

Then calculate savings as the difference between the baseline and the installed unit:

$$AKWH_{lost opp} = E_{b, lost opp} - E_{i}$$

$$AKWH_{lost opp} = 458.0 \, \frac{kWh}{yr} - 370 \, \frac{kWh}{yr} = 88 \, \frac{kWh}{yr}$$

Lost Opportunity Gross Peak Demand Savings, Electric, Winter and Summer

Use the annual energy usage calculated for lost opportunity in the following equations:

$$\begin{aligned} WKW_{lost\;opp} &= \frac{AKWH_{lost\;opp} \times PF_W}{1000 \ensuremath{W_{kW}}} \\ SKW_{lost\;opp} &= \frac{AKWH_{lost\;opp} \times PF_S}{1000 \ensuremath{W_{kW}}} \end{aligned}$$

Lost Opportunity Gross Peak Demand Savings, Example

Example 3. Using the results of Example 1, calculate demand savings for a 16.0 cubic foot upright freezer with manual defrost purchased through a retail promotion. Rated energy usage is 409 kWh/yr.

$$WKW_{lost opp} = AKWH_{lost opp} \times PF_W / 1000W_{kW}$$

$$WKW_{lost opp} = 58 \, kWh_{yr} \times 0.1031 / 1000W_{kW} = 0.0060 \, kW$$

$$SKW_{lost opp} = AKWH_{lost opp} \times PF_S / 1000W_{kW}$$

$$SKW_{lost opp} = 58 \, kWh_{yr} \times 0.1834 / 1000W_{kW} = 0.0106 \, kW$$

Example 4. Using the results of Example 2, calculate demand savings for an 8.5 cubic foot upright freezer with automatic defrost installed in an Energy Star New Home. Rated energy usage is 370 kWh/yr.

$$WKW_{lost opp} = 88 \frac{kWh}{yr} \times 0.1031/1000 \frac{W}{kW} = 0.0091 kW$$

$$SKW_{lost \, opp} = 88 \, \frac{kWh}{yr} \times 0.1834 / 1000 \, \frac{W}{kW} = 0.0161 \, kW$$

Retrofit Gross Energy Savings, Electric

Reminder: Retrofit savings are the sum of Retirement savings and Lost Opportunity savings. This section presents the Retirement portion of savings while the Lost Opportunity portion of the savings is presented further on in this measure.

To obtain the lifetime savings, the following formula should be used:

$$LKWH_{C. Total} = AKWH_{C. Retire} \times RUL + AKWH_{C. Lost Opp} \times EUL$$

Retirement Component:

- Convert volume (V) into Adjusted Volume: $AV_e = 1.73 \times V_e$
- Select the equation for $E_{\text{fed std}}$ for the existing unit's configuration from Table 1 in Note [2], and use AV_e in the equation. This is the baseline level, $E_{b, \text{ retire}}$.
- Then take the energy usage difference between the existing and baseline unit:

$$AKWH_{\it retire} = E_e - E_{b,\, retire}$$

Turn-in measure:

$$AKWH_{turn-in} = E_e$$

Retrofit Gross Energy Savings, Example

Example 5. Calculate energy savings for replacing a 1997 model manual defrost chest freezer in working condition in an existing home if the rated usage of the existing model is known, 399 kWh/yr. The old unit's volume is 12.86 ft^3 , resulting in the following adjusted volume: $AV_e = 1.73 \times V_e = 22.2478 \text{ ft}^3$.

The new model's volume is 12.9 ft³, resulting in the following adjusted volume: $AV_i = 1.73 \times V_i = 22.317 \text{ ft}^3$. The rated energy use of the new model is 326 kWh/yr.

Lost Opportunity Component:

Select the E_{fed std} equation for the category of the (new) installed unit from Table 1 for E_h:

$$E_{b, lost opp} = 9.88 \times AV_i + 143.7$$

Calculate the baseline level from AVi:

$$E_{b,lost opp} = 9.88 \times 22.317 + 143.7 = 364 \frac{kWh}{yr}$$

Then calculate Lost Opportunity savings as the difference between the baseline and the installed unit:

$$AKWH_{lost opp} = E_{b,lost opp} - E_i$$

 $AKWH_{lost opp} = 364 \ kWh - 326 \ kWh = 38^{kWh}/_{vr}$

Retirement Component:

Select the $E_{\text{fed std}}$ equation for the category of the (old) existing unit from Table 1 and calculate the baseline level from AV_e :

$$E_{b, retire} = (9.88 \times AV_e) + 143.7$$

 $E_{b, retire} = (9.88 \times 22.2478) + 143.7 = 364 \text{ kWh/yr}$

Then calculate savings as the difference between the existing and the baseline unit:

$$AKWH_{retire} = 399 \ kWh - 364 \ kWh = 35 \ kWh/_{vr}$$

Example 6. Calculate energy savings for replacing a 1997 model manual defrost chest freezer in working condition in an existing home if the rated usage of the existing model is unknown. The old unit's volume is 12.86 ft³, resulting in the following adjusted volume: $AV_e = 1.73 \times V_e = 22.2478 \text{ ft}^3$.

The new model's volume is 12.9 ft³, resulting in the following adjusted volume: $AV_i = 1.73 \times V_i = 22.317 \text{ ft}^3$. The rated energy use of the new model is 326 kWh/yr.

Lost Opportunity Component:

 $AKWH_{lost opp} = 38 \, kWh/_{vr}$ from Example 1.

Retirement Component:

The Retirement calculation is the same as Example 1 except the last step; E_e must be estimated based on the age of the existing unit (per Note [1]):

$$\begin{split} E_{b, \, retire} &= 364 \, {}^{kWh} / {}_{yr} \\ E_e &= \left(3142.6 - \left(1.5579 \times Year_e \right) \right) \times V_e \\ E_e &= \left(3142.6 - \left(1.5579 \times 1997 \right) \right) \times 12.86 \, ft^3 = 405 \, {}^{kWh} / {}_{yr} \end{split}$$

Then calculate Retirement savings as the difference between the existing and the baseline unit:

$$AKWH_{retire} = 405 \, kWh - 364 \, kWh = 41 \, kWh/_{yr}$$

Example 7. Calculate energy savings for a 1997 model manual defrost chest freezer in working condition being recycled through a turn-in program if it is a second unit which will not be replaced by a new unit. The rated usage of the existing model is known, 399 kWh/yr. The old unit's volume is 12.86 ft³, resulting in the following adjusted volume: $AV_e = 1.73 \times V_e = 22.2478 \text{ ft}^3$.

Gross annual savings (no Lost Opportunity) for removing the unit from operation are:

$$AKWH_{turn-in} = 399 \, \frac{kWh}{yr}$$

Retrofit Gross Peak Demand Savings, Electric, Winter and Summer

Reminder: Retrofit savings are the sum of Retirement savings and Lost Opportunity savings. This section presents the Retirement portion of savings while the Lost Opportunity portion of the savings is presented further on in this measure.

Retirement Component:

$$\begin{aligned} WKW_{retire} &= \frac{AKWH_{retire} \times PF_W}{1000 \, W_{kW}} \\ SKW_{retire} &= \frac{AKWH_{retire} \times PF_S}{1000 \, W_{kW}} \end{aligned}$$

Turn-in:

$$WKW_{turn-in} = AKWH_{turn-in} \times PF_W / 1000 \frac{W}{kW}$$

$$SKW_{turn-in} = AKWH_{turn-in} \times PF_S / 1000 \frac{W}{kW}$$

Retrofit Gross Peak Demand Savings, Example

Example 8. Using the results of Example 5, calculate demand savings for replacing a 1997 model manual defrost chest freezer in working condition in an existing home if the rated usage of the existing model is known, 399 kWh/yr. The old unit's volume is 12.86 ft³, resulting in the following adjusted volume:

 $AV_e = 1.73 \times V_e = 22.2478 \text{ ft}^3$. The new model's volume is 12.9 ft³, resulting in the following adjusted volume: $AV_i = 1.73 \times V_i = 22.317 \text{ ft}^3$. The rated energy use of the new model is 326 kWh/yr.

Because the existing unit is verified to be in working condition, the retrofit savings are made up of both a Lost Opportunity component and an early Retirement component.

Lost Opportunity Component:

$$WKW_{lost opp} = 38 \frac{kWh}{yr} \times 0.1031/1000 \frac{W}{kW} = 0.0039 kW$$

$$SKW_{lost opp} = 38 \times 0.1834/1000 \frac{W}{kW} = 0.0070 kW$$

Retirement Component:

$$WKW_{retire} = 35 \frac{kWh}{yr} \times 0.1031 / 1000 \frac{W}{kW} = 0.0036 kW$$
$$SKW_{retire} = 35 \times 0.1834 / 1000 \frac{W}{kW} = 0.0064 kW$$

Total Demand Savings:

Claim WKW of 0.0039 and SKW of 0.0070 kW for Lost Opportunity savings for the EUL Claim WKW of 0.0036 kW and 0.0064 kW for Retirement savings for the RUL.

Example 9. Using the results of Example 6, calculate demand savings for replacing a 1997 model manual defrost chest freezer in working condition in an existing home if the rated usage of the existing model is unknown. The old unit's volume is 12.86 ft³, resulting in the following adjusted volume: $AV_e = 1.73 \times V_e = 22.2478 \text{ ft}^3$. The new model's volume is 12.9 ft³, resulting in the following adjusted volume: $AV_i = 1.73 \times V_i = 22.317 \text{ ft}^3$. The rated energy use of the new model is 326 kWh/yr.

Lost Opportunity Component:

$$WKW_{lost \, opp} = 0.0039 \, kW \text{ from Example 1.}$$

 $SKW_{lost \, opp} = 0.0070 \, kW \text{ from Example 1.}$

Retirement Component:

$$WKW_{retire} = 41^{kWh}/_{yr} \times 0.1031/1000W/_{kW} = 0.0042 \ kW$$
$$SKW_{retire} = 41 \times 0.1834/1000W/_{kW} = 0.0075 \ kW$$

Total Demand Savings:

Claim WKW of 0.0039 and SKW of 0.0070 kW for Lost Opportunity savings for the EUL Claim WKW of 0.0042 kW and 0.0075 kW for Retirement savings for the RUL.

Example 10. Using the results of Example 7, calculate demand savings for a 1997 model manual defrost chest freezer in working condition being recycled through a turn-in program if it is a second unit which will not be replaced by a new unit. The rated usage of the existing model is known, 399 kWh/yr. The old unit's volume is 12.86 ft³, resulting in the following adjusted volume: $AV_e = 1.73 \times V_e = 22.2478 \text{ ft}^3$.

$$WKW_{turn-in} = 399 \, \frac{kWh}{yr} \times 0.1031 / 1000 \, \frac{W}{kW} = 0.0411 \, kW$$
$$SKW_{turn-in} = 399 \times 0.1834 / 1000 \, \frac{W}{kW} = 0.0732 \, kW$$

Changes from Last Version

Rearranged presentation to facilitate clear definition of lost opportunity and retrofit. Customized Lost Opportunity calculations are now found in the Lost Opportunity sections instead of in Retrofit. Provided alternate equations to estimate energy usage of existing unit in the case of unknowns. Examples have been refreshed. Recycling Turn-in program and New Homes savings added.

References

- [1] KEMA, Evaluation of the Weatherization Residential Assistance Partnership and Helps Programs (WRAP/Helps), September 10, 2010
- [2] Energy Star Program Requirements Product Specification for Residential Refrigerators and Freezers: Eligibility Criteria, Version 4.1. Effective April 28, 2008.
- [3] Energy Star Residential Refrigerators and Freezers Specification: Website tracking proposed draft Energy Star Version 5.0 specification. http://www.energystar.gov/index.cfm?c=revisions.res_refrig_spec . Last Accessed July 25, 2012. Proposed Effective date: January 1, 2013.
- [4] Federal Register Part IX, 10 CFR Part 430, Vol. 63, No. 81, Energy Conservation Program for Consumer Products: Energy Conservation Standards for Refrigerators, Refrigerator-Freezers and Freezers; Final Rule. Published Monday, April 28, 1997. Effective July 1, 2001. Last accessed online July 30, 2012: http://www1.eere.energy.gov/buildings/appliance_standards/residential/pdfs/reffrbod.pdf
- [5] California Energy Commission (CEC) Appliance Database.

 Online historical appliance database: http://www.energy.ca.gov/appliances/database/historical_excel_files/
 Online current (meeting minimum standards) appliance database: http://www.appliances.energy.ca.gov/
- [6] Energy Star Residential Refrigerators and Freezers Specification: Website tracking proposed draft Energy Star Version 5.0 specification. http://www.energystar.gov/index.cfm?c=revisions.res_refrig_spec . Last Accessed July 25, 2012. Proposed Effective date: January 1, 2013.
- [7] Federal Register, Vol. 76, No. 179. 10 CFR Part 430. Energy Conservation Program: Energy Conservation Standards for Residential Refrigerators, Refrigerator-Freezers, and Freezers. Published September 15, 2011, Effective November 14, 2011, Compliance date September 15, 2014.
- [8] Energy Star Freezers website, last accessed August 2, 2012: http://www.energystar.gov/index.cfm?fuseaction=find_a_product.showProductGroup&pgw_code=FRZ
- [9] Nexus Market Research, Inc. Impact, Process, and Market Study of the Connecticut Appliance Retirement Program: Overall Report, December 23, 2005. Table ES.4, Page 3.

Notes

[1] The unadjusted annual energy usage of the existing unit can usually be found in the CEC database (Ref [5]) or equivalent source by brand and model number.

If actual usage of the existing unit is unknown, the equations in Table 3, below, may be used to estimate the energy usage of the existing unit, based on its known volume and estimated age. The following equations are based on average rated usage of models from Ref [5] added between 1978 and 2003.

Table 3: Equations to estimate existing energy usage if unknown

| Category | Units 1978 and newer, Estimated E _e | Units prior to 1978, Estimated E _e (capped at 1978 levels) |
|---|---|---|
| Upright freezers with manual defrost | $(2797.8 - (1.382 \times Year_e)) \times V_e$ | $(64.204 \times V_e)$ |
| Upright freezers with automatic defrost | $(4562.5 - (2.295 \times Year_e)) \times V_e$ | $(22.99 \times V_e)$ |
| Chest freezers and all other freezers except compacts | $(3142.6 - (1.5579 \times Year_e)) \times V_e$ | $(61.074 \times V_e)$ |

[2] The baseline new model is represented by the 2001 NAECA Federal Standard level (Table 1). Because in many cases the installed energy efficient unit does not share the same size and category as the existing unit, the Federal Standard energy usage, $E_{\text{fed std}}$, must be calculated separately for Lost Opportunity (using the Adjusted Volume

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and category of the new installed unit) and Retirement (using the Adjusted Volume and category of the existing unit).

Note: In the special case of an Energy Star New Home, the baseline new model is represented by a 2008 Energy Star model (Table 1) using the Adjusted Volume and category specific to the installed unit. The minimum 2008 Energy Star energy usage is 90% of the Federal Standard usage.

Table 1: Energy Specifications: Maximum Energy Use (Based on Size)

| Configuration | 2001 Federal Standard, E _{fed std} (Ref [4]) | 2008 Energy Star, E _{ES 2008} (Ref [2]) |
|---|--|---|
| Upright freezers with manual defrost | $(7.55 \times AV) + 258.3$ | $(6.80 \times AV) + 232.5$ |
| Upright freezers with automatic defrost | $(12.43 \times AV) + 326.1$ | $(11.19 \times AV) + 293.5$ |
| Chest freezers and all other freezers except compacts | $(9.88 \times AV) + 143.7$ | $(8.89 \times AV) + 129.3$ |

- [3] Exceptions to standard calculations for replacement of existing units may occur in the following special situations:
 - a. If the annual kWh usage of the existing unit is already less than or equal to that of the baseline level ($E_e \le E_b$), no retirement savings may be claimed.
 - b. If the annual kWh usage of the existing unit is less than the that of the baseline level but greater than that of the new installed unit ($E_i < E_e < E_b$), the lost opportunity component of savings may still be claimed, but the existing unit Annual kWh usage must be used for the baseline rather than Energy Star 2004.
 - c. If annual kWh usage of the new installed unit greater than or equal to that of the existing unit $(E_e \le E_i)$, regardless of size, no savings may be claimed.
- [4] Energy use and Adjusted Volume ratings for new installed Energy Star units may be obtained through the Energy Star website, Ref [8]. Because of the complexity of the 2013 Energy Star Version 5.0 specification (summarized in Table 1) and 2014 Federal Standard (Ref [7]), the details of these specifications are not listed here but may be obtained directly from the final reference documents.

Version Date: 10/30/2012 4.3.13 DEHUMIDIFIER

4.3.13 DEHUMIDIFIER

Description of Measure

Savings detailed below cover the purchase of a high efficiency dehumidifier and the replacement of an inefficient dehumidifier in working condition.

Savings Methodology

Lost Opportunity Measure:

- Lost Opportunity savings are the difference in energy use between a baseline new model (Note [4]) based on the capacity of the installed unit, and the chosen high efficiency new model (Note [1]), continuing for the Effective Useful Life (EUL) from Appendix 4.
- The Retail measure is a Lost Opportunity-only methodology, as the existing unit is not verified.

Retrofit Measure:

- Uses the same methodology as a Lost Opportunity measure.
- In the case of early retirement of a working unit where the unit would have otherwise been installed until failure, lifetime "Retirement" savings are claimed additional to the lifetime "Lost Opportunity" savings (see Section 1.4).
- Retirement savings are the difference in energy use between the older unit (Note [2]) and a baseline new model (Note [4]) based on the capacity of the existing unit, continuing for the Remaining Useful Life (RUL) from Appendix 4.

Energy usage for dehumidifiers depends on the capacity and the rated Energy Factor.

Inputs

| Symbol | Description | |
|-----------------|---|--|
| Capi | Capacity of the new installed unit, in pints/day | |
| Cape | Capacity of the (old) existing unit, in pints/day | |
| EF_i | Energy Factor of the new installed unit | |
| EF _e | Energy Factor of the (old) existing unit | |
| | Make and Model of (old) existing unit | |
| · | Make and Model of new installed unit | |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|---------------------------|---|-----------|--------------|------------|
| days/yr | Equivalent Annual Days per year equaling 1620 hrs/yr | days/yr | 67.5 | Ref [4] |
| EF _{b, lost opp} | Energy Factor of baseline new unit based on size of new | L/kWh | 2012 Federal | Table 1 of |
| | unit | | Standard | Note [4] |
| EF _{b, retire} | Energy Factor of baseline new unit based on size of | L/kWh | 2012 Federal | Table 1 of |
| · | existing unit | | Standard | Note [4] |
| EF_e | Energy Factor of (old) existing unit | L/kWh | actual | Note [2] |
| EF_i | Energy Factor of new installed unit | L/kWh | actual | |
| size _e | Capacity of the (old) existing unit | pints/day | actual | |
| size _i | Capacity of the new installed unit | pints/day | actual | |

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Lost Opportunity Gross Energy Savings, Electric

Select EF_b of the 2012 Federal Standard (Table 1) for the capacity of the installed unit to use in the following equation:

$$AKWH_{lost\;opp} = Cap_{i} \times 0.473 \, {}^{Liters}/_{pint} \times 67.5 \, {}^{days}/_{yr} \times \left(\frac{1}{EF_{b,lost\;opp}} - \frac{1}{EF_{i}}\right)$$

Lost Opportunity Gross Energy Savings, Example

Example 1. A 64 pint/day unit with an energy factor of 1.9 is purchased through a retail promotion. What are the energy savings?

First, determine the EF for a 30 pint/day unit meeting 2012 Federal Standards from Table 1: $EF_{b,lost \, opp} = 1.70$. Then calculate AKWH using the equation from the Lost Opportunity section:

$$AKWH_{lost opp} = 64 \frac{pints}{day} \times 0.473 \frac{Liters}{pint} \times 67.5 \frac{days}{yr} \times \left(\frac{1}{1.7} - \frac{1}{1.9}\right) = 126.5 \frac{kWh}{yr}$$

Lost Opportunity Gross Peak Demand Savings, Electric, Winter and Summer

$$SKW_{lost opp} = \frac{AKWH_{lost opp}}{1620^{hrs}/v_r}$$

No winter demand savings shall be claimed (Note [3]).

Lost Opportunity Gross Peak Demand Savings, Example

Example 2. A 64 pint/day unit with an energy factor of 1.9 is purchased through a retail promotion. Using the results of Example 1, what are the demand savings?

$$SKW_{lost \ opp} = \frac{126.5 \,^{kWh}/_{yr}}{1620 \,^{hrs}/_{yr}} = 0.0781 \,^{kW}$$

Retrofit Gross Energy Savings, Electric

Reminder: Retrofit savings are the sum of Retirement savings and Lost Opportunity savings. This section presents the Retirement portion of savings while the Lost Opportunity portion of the savings is presented further on in this measure.

To obtain the lifetime savings, the following formula should be used:

$$LKWH_{C, Total} = AKWH_{C, Retire} \times RUL + AKWH_{C, Lost Opp} \times EUL$$

Retirement Component:

Select EF_b of the 2012 Federal Standard (Table 1) for the capacity of the existing unit to use in the following equation:

$$AKWH_{retire} = Cap_{e} \times 0.473 \, \frac{Liters}{pint} \times 67.5 \, \frac{days}{yr} \times \left(\frac{1}{EF_{e}} - \frac{1}{EF_{b, retire}} \right)$$

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Retrofit Gross Energy Savings, Example

Example 3. A 30 pint/day unit with a known EF of 1.2 Liters/kWh is replaced in an existing home with a high efficiency 30 pint/day unit with an EF of 1.85 Liters/kWh. What are the energy savings?

First, determine the EF for a 30 pint/day unit meeting 2012 Federal Standards from Table 1: $EF_{b,lost opp} = 1.35$. In this case, the size of both units is the same, therefore: $EF_{b,retire} = EF_{b,lost opp}$

Then calculate AKWH for both Lost Opportunity and Retirement components using equations from the respective sections:

$$AKWH_{lost opp} = 30^{pints} / _{day} \times 0.473^{Liters} / _{pint} \times 67.5^{days} / _{yr} \times \left(\frac{1}{1.35} - \frac{1}{1.85}\right) = 191.8^{kWh} / _{yr}$$

$$AKWH_{retire} = 30^{pints} / _{day} \times 0.473^{Liters} / _{pint} \times 67.5^{days} / _{yr} \times \left(\frac{1}{1.2} - \frac{1}{1.35}\right) = 88.7^{kWh} / _{yr}$$

Retrofit Gross Peak Demand Savings, Electric, Winter and Summer

Reminder: Retrofit savings are the sum of Retirement savings and Lost Opportunity savings. This section presents the Retirement portion of savings while the Lost Opportunity portion of the savings is presented further on in this measure.

Retirement Component:

$$SKW_{retire} = \frac{AKWH_{retire}}{1620^{hrs}/_{vr}}$$

No winter demand savings shall be claimed (Note [3]).

Retrofit Gross Peak Demand Savings, Example

Example 4. A 30 pint/day unit with a known EF of 1.2 Liters/kWh is replaced in an existing home with a high efficiency 30 pint/day unit with an EF of 1.5 Liters/kWh. Using the results of Example 3, what are the demand savings?

$$SKW_{lost opp} = \frac{191.8 \, \frac{kWh}{yr}}{1620 \, \frac{hrs}{yr}} = 0.1184 \, \frac{kWh}{yr}$$
$$SKW_{retire} = \frac{88.7 \, \frac{kWh}{yr}}{1620 \, \frac{hrs}{yr}} = 0.0547 \, \frac{kWh}{yr}$$

Changes from Last Version

Rearranged presentation to facilitate clear definition of lost opportunity and retrofit and moved Lost Opportunity to its own section. Examples have been refreshed. While methodology is the same, baseline level was previously Energy Star 2008 and is now the 2012 Federal Standard.

References

- [1] US Congress, Energy Independence and Security Act of 2007 (EISA), Title III, "ENERGY SAVINGS THROUGH IMPROVED STANDARDS FOR APPLIANCE AND LIGHTING," January 4, 2007. Section 311 (a)(1) Dehumidifiers, Effective October 1, 2012.
- [2] Energy Star Program Requirements Product Specification for Dehumidifiers: Eligibility Criteria, Version 2.1. Effective June 1, 2008.

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- [3] US Congress, Energy Policy Act of 2005 (EPACT), Title I, "ENERGY EFFICIENCY", Subtitle C, "Energy Efficient Products", January 4, 2005, Section 135 (cc), "DEHUMIDIFIERS", effective October 1, 2007.
- [4] Energy Star Dehumidifiers website, last accessed August 2, 2012. http://www.energystar.gov/index.cfm?fuseaction=find_a_product.showProductGroup&pgw_code=DE
- [5] Federal Register Volume 74, No 66, published April 8, 2009, Part II, DOE, 10 CFR Part 340, Energy Conservation Program: Energy Conservation Standards for Certain Consumer Products (Dishwashers, Dehumidifiers, Microwave Ovens, and Electric and Gas Kitchen Ranges and Ovens) and for Certain Commercial and Industrial Equipment (Commercial Clothes Washers), Final Rule, effective October 1, 2012. Page 16042, Table I.1.

Notes

- [1] The Energy Factor for new installed Energy Star units may be obtained through the Energy Star website, Ref [4].
- [2] If the Energy Factor of the existing unit is unknown, it shall be based on the 2007 Federal Standard EF listed in Table 1 for the existing unit's capacity. If the capacity of the existing unit is unknown, the capacity of the new unit shall be used.
- [3] Due to insufficient peak coincident data, the average kW savings, which is conservatively lower than the coincident peak, shall be claimed for the summer seasonal peak demand savings. No winter demand savings shall be claimed.
- [4] The baseline new model is represented by the 2012 Federal Standard level shown in Table 1, below. Because in many cases the installed energy efficient unit does not share the same capacity as the existing unit, the baseline energy usage, must be calculated separately for Lost Opportunity (using the capacity of the new installed unit) and Retirement (using the capacity of the existing unit).

Table 1: Energy Specifications: Energy Factor (EF)

| Capacity (Pints/day) | 2007 Federal Standard (Ref [3]) | 2008 Energy Star (Ref [2]) | 2012 Federal Standard (Ref [5]) | 2012 Energy Star (Ref [1]) |
|--------------------------|---------------------------------------|-------------------------------|------------------------------------|-------------------------------|
| ≤ 25 | 1.00 | 1.20 | 1.35 | |
| $> 25 \text{ to} \le 35$ | 1.20 | 1.40 | 1.33 | |
| $> 35 \text{ to} \le 45$ | 1.30 | 1.50 | 1.50 | 1.85 |
| $>$ 45 to \leq 54 | 1.30 | 1.60 | 1.60 | |
| > 54 to < 75 | 1.50 | 1.80 | 1.70 | |
| \geq 75 to \leq 185 | 2.25 | 2.50 | 2.5 | 2.80 |

Version Date: 10/30/2012 4.3.14 ELECTRONICS

4.3.14 ELECTRONICS

Description of Measure

A new ENERGY STAR qualified electronics equipment. Electronics equipment includes:

- Blu-Ray player
- Computer Monitor (Displays)
- Cordless Phones
- Desktop Computers
- DVD player
- Laptop Computers
- Set-top Boxes & Cable Boxes
- Televisions

Savings Methodology

The savings estimates in the Table 1 below are for ENERGY STAR qualified electronics equipment versus conventional equipment. (References [1] & [2]).

Note: no demand savings have been identified for this measure

Inputs

| Symbol | Description | Units |
|--------|-----------------------|-------|
| | No of units purchased | |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|--------|--------------------------------|-------|--------|----------|
| AKWH | Annual Electric Energy Savings | kWh | | Table 1 |
| SKW | Summer Demand Savings | kW | 0 | |
| WKW | Winter Demand Savings | kW | 0 | |

Lost Opportunity Gross Energy Savings, Electric

The savings estimates in the following table are for ENERGY STAR qualified electronics equipment versus conventional equipment.

| Table 1: ENERGY STAR Electronics Annual Savings | | | | |
|---|------------------------|---|--|--|
| Electronics Equipment | Energy Savings AKWH | Comments | | |
| Blu-Ray player | 8 | Reference [1] | | |
| Computer Monitor (Displays) | 14 | Reference [2] | | |
| Cordless Phones | 26 | The savings are based on the difference between a conventional cordless phone (37.1 kWh) and an ENERGY STAR rated (11.5 kWh). Reference [1] | | |
| Desktop Computers | 77 | Reference [2] | | |
| DVD player | 19 | Reference [1] | | |
| Laptop Computers | 24 | Reference [2] | | |
| Set-top Boxes & Cable Boxes | 54 | Reference [1] | | |
| Televisions | 119 | The savings are based on the difference between a 40 inch | | |

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| C | conventional TV | and an ENERGY | STAR rated. | Reference [1] |
|---|-----------------|---------------|-------------|---------------|

Lost Opportunity Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

WKW = 0SKW = 0

No demand savings are claimed for this measure.

Changes from Last Version

New measure

References

- [1] Savings Estimate for ENERGY STAR Qualified Consumer Electronics, ENERGY STAR Consumer Electronics Calculator, ENERGY STAR www.energystar.gov> Last accessed on July 25, 2012.
- [2] Savings Estimate for ENERGY STAR Qualified Office Equipment, ENERGY STAR Office Equipment Savings Calculator, ENERGY STAR www.energystar.gov> Last accessed on July 25, 2012.

Version Date: 10/30/2012 4.4.1 REM SAVINGS

4.4 ENVELOPE

4.4.1 REM SAVINGS

Description of Measure

Residential Energy Modeling (REM) Savings for ENERGY STAR certified residential new construction.

Savings Methodology

An ENERGY STAR Home must be certified through Home Energy Rating System (HERS). ENERGY STAR Homes are limited to single family homes or multi-family homes that are five stories or less. Hi-rise units do not qualify for ENERGY STAR certification and the savings methodology below does not apply to those units.

The traditional method of qualifying ENERGY STAR Homes is through a HERS rating. The rating involves inputting the key energy features into a computer program (geometry, orientation, thermal performance, mechanical systems, etc.) that will generate a HERS score and other useful information regarding the energy usage of the home. REM/RateTM (REM) is the software that is used in Connecticut (and in most jurisdictions) to generate HERS ratings (Note [1]).

A feature of REM is that it enables the user to define a base home ("user defined reference home," or UDRH) and calculate the savings of an actual home relative to the UDRH. UDRH is the same size as the "as-built" and utilizes the same type of mechanical systems and fuels. However, the thermal and mechanical efficiencies of the UDRH are set to baseline levels (Note [2]). Current UDRH values are based on the 2011 RNC study (Ref [1]).

Inputs

| Symbol | Description |
|--------|--|
| REM | REM simulation file submitted by an HERS rater |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|--------|--------------------------------|-------|---------------|------------|
| 1 Ton | Capacity, Tonnage | Tons | 12,000 Btu/hr | Conversion |
| AKWH | Annual Electric Energy Savings | kWh | | |
| SKW | Summer Demand Savings | kW | | |
| WKW | Winter Demand Savings | kW | | |

Lost Opportunity Gross Energy Savings, Electric

The UDRH report generates heating, cooling and water heating consumption for the "as-built" home and the defined "base" home (i.e. Table 1). The difference between those values is the energy savings. This savings is referred to as "REM" savings.

Table 1: Example of a Typical UDRH Report

| | UDRH Consumption (MMBtu) | As-Built Consumption (MMBtu) | Energy Savings (MMBtu) |
|---------------|---------------------------------|------------------------------|-------------------------------|
| Heating | 40.5 | 34.8 | 5.7 |
| Cooling | 4.5 | 2.3 | 2.2 |
| Water Heating | 20.6 | 17.5 | 3.1 |

The REM savings above includes the effect of installing a programmable thermostat, so additional savings should not be claimed if one (or more) is programmable thermostat is installed. Also, REM has the ability to incorporate lights and

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appliances into an "expanded" rating. Connecticut does NOT use the expanded rating. Therefore, the REM savings does not include savings for lights and appliances. These savings (if any) are calculated separately.

Since REM savings is based on a whole building approach (i.e. it includes the effects of upgraded insulation, tighter ducts, increased efficiencies, etc.), this savings methodology takes precedence over "code-plus" measures. Savings for homes that have a REM analysis done should be calculated using the UDRH Report; and no additional savings should be claimed based on code-plus measures.

There are two baselines from which savings are calculated. Of the following two options, the baseline that produces the least savings will be the baseline of the claimed savings, either:

- 1. A home based on minimum prescriptive code.
- 2. An "average" home built in Connecticut as determined by a baseline evaluation (and used as a baseline home UDRH). Note: the baseline may differ from a home built to minimum prescriptive code. While many homes fail to meet some aspects of the energy code, their performance overall exceeds minimum code performance substantially and therefore, the baseline exceeds minimum code performance as well.

Lost Opportunity Gross Energy Savings, Electric

Described above in lost opportunity gross energy savings – electric

Lost Opportunity Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

Described above in lost opportunity gross energy savings – electric

Lost Opportunity Gross Peak Day Savings, Natural Gas

Described above in lost opportunity gross energy savings – electric

Non Energy Benefits

Improves personal comfort and health. It also increases a home's durability and value.

Changes from Last Version

Note [2] added.

References

[1] http://www.ctenergyinfo.com/ConnecticutNewResidentialConstructionBaseline-10-1-12.pdf

Notes

- [1] REM/RateTM is a residential energy analysis, code compliance and rating software developed by Architectural Energy Corporation. This software calculates heating, cooling, hot water, lighting, and appliance energy loads, consumption and costs for new and existing single and multi-family homes
- [2] The UDRH is based on data collected through evaluations, and baseline levels are prescriptive code values or those established from the most recent baseline studies available and program administrator field experience.

4.4.4 INFILTRATION REDUCTION TESTING (BLOWER DOOR TEST)

Description of Measure

Version Date: 10/30/2012

Blower Door Test equipment is used to verify infiltration reduction.

Savings Methodology

REM/Rate (Ref [1]), a residential energy analysis, code compliance and rating software, was used to simulate energy use in a typical home before and after infiltration reduction (CFM air leakage at 50 Pascals pressure difference). The average energy savings in MMBtu and kWh were estimated from the results of the REM/Rate simulations, then converted to the appropriate fuels using unit conversions and assumed distribution losses. The demand savings were also based on the REM simulation.

Note: these savings are based on envelope reductions only and should not be applied to duct sealing reductions which are addressed as a separate measure (Measure 4.2.9).

Inputs

| Symbol | Description |
|---------------------|---|
| CFM_{Pre} | Infiltration before air sealing @ 50 Pa |
| CFM _{Post} | Infiltration after air sealing @ 50 Pa |
| | Heating Fuel Type (Electric Resistive, HP, Gas, Oil, Propane, etc) |
| | Heating System Distribution Type (Forced air with fan, heat pump, resistive, radiator, etc) |

Nomenclature

| Symbol | Description | Units | Value | Comments |
|-------------------|---|-------|---------|------------|
| ACCF _H | Annual Natural Gas Savings, Heating | Ccf | | |
| AKWH _H | Annual Electric Energy Savings, Heating | kWh | | |
| $AKWH_C$ | Annual Electric Energy Savings, Cooling | kWh | | |
| AOG_H | Annual Oil Savings, Heating | Gal | | |
| APG_H | Annual Propane Savings, Heating | Gal | | |
| CFM_{Pre} | Infiltration before air sealing measured with the house being | CFM | | Inputs |
| | negatively pressurized to 50 Pa relative to outdoor conditions. | | | |
| CFM_{Post} | Infiltration after air sealing measured with the house being negatively | CFM | | Inputs |
| | pressurized to 50 Pa relative to outdoor conditions. | | | |
| PD_{H} | Natural gas peak day savings, Heating | Ccf | | |
| PDF_{H} | Natural gas peak day factor – Heating | | 0.00977 | Appendix 1 |
| REM | Savings factor in energy units per CFM reduction based on REM/Rate | | | |
| | simulation | | | |
| SKW | Summer Demand Savings | kW | | |
| WKW | Winter Demand Savings | kW | | |

Retrofit Gross Energy Savings, Electric

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Table 1: Retrofit Electric Savings per CFM Reduction (at 50 Pa)

| Measure | | Energy Savings | Units |
|---|------------------------|-----------------------|-------|
| Electric Resistance Heat | REM _{Heating} | 2.638 | kWh |
| Heat Pump Heating | REM _{Heating} | 1.319 | kWh |
| Geothermal Heating | REM _{Heating} | 0.879 | kWh |
| Air Handler (fan) Heating | REM _{AH} | 0.06 | kWh |
| Cooling (Central Air Only) | REM _{Cooling} | 0.0593 | kWh |
| Cooling (Room AC: Window, Sleeve, or PTAC) (Note [1]) | REM _{Cooling} | 0.0168 | kWh |

For Electric Resistive, Heat Pump or Geothermal Heating Systems,

$$AKWH_H = REM_{Heating} \times (CFM_{Pre} - CFM_{Post})$$

For Fossil Fuel heating with air handler unit,

$$AKWH_H = REM_{AH} \times (CFM_{Pre} - CFM_{Post})$$

For homes with cooling,

$$AKWH_C = REM_{Cooling} \times (CFM_{Pre} - CFM_{Post})$$

Retrofit Gross Energy Savings, Fossil Fuel

Table 2: Retrofit Fossil Fuel Savings per CFM Reduction (at 50 Pa)

| Measure | | Energy Savings | Units |
|---------------------|------------------------|-----------------------|-------|
| Fossil Fuel Heating | | 0.012 | MMBtu |
| Natural Gas | REM_{NG} | 0.117 | Ccf |
| Propane | REM _{Propane} | 0.131 | Gal |
| Oil | REM_{Oil} | 0.087 | Gal |

For homes with natural gas heating system,

$$ACCF_H = REM_{NG} \times (CFM_{Pre} - CFM_{Post})$$

For homes with oil heating system,

$$AOG_H = REM_{Oil} \times (CFM_{Pre} - CFM_{Post})$$

For homes with propane heating system,

$$APG_H = REM_{Propage} \times (CFM_{Pre} - CFM_{Post})$$

Retrofit Gross Energy Savings, Example

A blower door test was performed in a 2400 ft², 1940's Cape Cod style home in Hartford, heated primarily by an oil boiler and cooled by Room AC. Blower Door test equipment was used to measure the infiltration of the home at 50 Pa. The readings on the test equipment showed CFM_{Pre} of 1850 and CFM_{Post} of 1575. What are the electric and fossil fuel savings for this home?

Oil Heating savings may be calculated using the following equation:

$$AOG_H = REM_{Oil} \times (CFM_{Pre} - CFM_{Post})$$

$$AOG_H = 0.086 \times (1850 - 1575) = 23.7^{Gal Oil/_{vr}}$$

Cooling savings may also be claimed as follows:

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$$AKWH_C = REM_{Cooling} \times (CFM_{Pre} - CFM_{Post})$$
$$AKWH_C = 0.0168 \times (1850 - 1575) = 4.62 \, ^{kWh}/_{vr}$$

Retrofit Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

Table 3: Demand Savings, kW per CFM Reduction

| Electric Resistance | Geothermal | Central AC | Room AC |
|---------------------|--------------------|-------------|-------------|
| and Heat Pump | - Retrofit | and HP | (Note [1]) |
| REM_{WKW} | REM _{WKW} | REM_{SKW} | REM_{SKW} |
| 0.00117 | 0.00039 | 0.00009 | 0.00002 |

$$WKW_{H} = REM_{WKW} \times (CFM_{Pre} - CFM_{Post})$$

$$SKW_{C} = REM_{SKW} \times (CFM_{Pre} - CFM_{Post})$$

Reminder: Demand savings are based on design load calculation in REM software hence there is no need to use coincidence factors

Retrofit Gross Peak Day Savings, Natural Gas

For homes with natural gas heating system,

$$PD_H = ACCF_H \times PDF_H$$

Retrofit Gross Peak Demand Savings, Example

For the above Retrofit example, what are the summer and winter demand savings for this home?

$$SKW_C = REM_{SKW} \times (CFM_{Pre} - CFM_{Post})$$

 $SKW_C = 0.00002 \times (1850 - 1575) = 0.0055 \text{ kW}$
 $WKW_H = REM_{WKW} \times (CFM_{Pre} - CFM_{Post})$
 $WKW_H = 0.00117 \times (1850 - 1575) = 0.332 \text{ kW}$

Changes from Last Version

Added cooling savings for Room AC. Updated Table 2, REM_{NG} from 0.123 to 0.117. Updated Table 2, REM_{Oil} from 0.086 to 0.087.

References

- [1] REM/RateTM is a residential energy analysis, code compliance and rating software developed by Architectural Energy Corporation. This software calculates heating, cooling, hot water, lighting, and appliance energy loads, consumption and costs for new and existing single and multi-family homes. Blower Door energy savings analysis using REM/RateTM was performed by C&LM Planning team, Northeast Utilities, August 2008.
- [2] Nexant Market Research, Inc., "Market Assessment for ENERGY STAR Room Air Conditioners in Connecticut," Cambridge, MA, 2007, pp. 17,18

- [3] RLW Analytics, "Final Report: Coincidence Factor Study: Residential Room Air Conditioners," Middletown, CT, 2008, p. iv, p. 22
- [4] ADM Associates, Inc., "Residential Central AC Regional Evaluation," Sacramento, CA, 2009, pp. 4-4

Notes

Version Date: 10/30/2012

[1] Room Air Conditioning cooling savings are derived from factors found in Ref [2,3,4].

4.4.8 WINDOW REPLACEMENT

Description of Measure

Version Date: 10/30/2012

Installation of ENERGY STAR window to replace existing single pane window that is between the conditioned space and the outdoors.

Savings Methodology

The savings for this measure are calculated using the installed area of the replacement window and usage factors develop using RESFEN (Ref [1]) to model different window types and heating fuels. The results of this analysis are shown in tables 1 & 2. The energy savings are calculated by subtracting the heating fuel specific ENERGY STAR Value single pane "tight" value and multiplying by the window area. For homes that have central cooling, the same analysis is done using the cooling energy usage.

Note: Savings may not be claimed if the window is located in an unconditioned space such as an unheated porch, basement, or hallway.

Inputs

| Symbol | Description | Units |
|---------|---|----------------------|
| | Cooling system type of home | |
| | Heating fuel of home / Heating system type | |
| D_{H} | Height of the window | Inches |
| D_{W} | Width of the window | Inches |
| U | Rated U value of window. (Not required for savings calculation) | $BTU/ft^2 x h x ^0F$ |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|------------------|---|--------------------------|---------|------------|
| A | Area of the window | ft ² | | |
| $ACCF_H$ | Annual Gas Savings - heating | Ccf/yr | | |
| AEC | Annual Electric Cooling Usage | kWh/ft²/yr | Table 1 | Note [2] |
| AEH | Annual Electric Heating Usage | kWh/ft²/yr | Table 1 | Note [2] |
| AGU | Annual Gas Usage | Ccf/ ft ² /yr | Table 2 | Note [2] |
| $AKWH_C$ | Annual Electric energy savings-Cooling | kWh/yr | | |
| $AKWH_H$ | Annual Electric energy savings-Heating | kWh/yr | | |
| AOG_H | Annual Oil Savings - heating | gal/yr | | |
| AOU | Annual Oil Usage | gal/ft²/yr | Table 2 | Note [2] |
| APG_H | Annual Propane Savings - heating | gallons/yr | | |
| APU | Annual Propane Usage | gal/ft²/yr | Table 2 | Note [2] |
| CF_S | Summer Seasonal Peak Coincidence Factor | | 0.59 | Appendix 1 |
| D_{H} | Height of the window | inch | | |
| D_{W} | Width of the window | inch | | |
| PF_W | Winter Peak Factor | W/kWh | 0.570 | Ref [2] |
| WKW | Winter coincident peak demand savings | kW | | |
| SKW | Summer coincident peak demand savings | kW | | |
| PDF_{H} | Peak Day Factor - Heating | | 0.00977 | Appendix 1 |
| PD_{H} | Peak Day savings - Heating | | | |
| •••• | Baseline | | | |
| ···es | ENERGY STAR | | | |

| Symbol | Description | Units | Values | Comments |
|--------|--------------------------------------|-------|--------|----------|
| •••НР | Heat Pump Heating Only | | | |
| ···R | Electric Resistance Heating Only | | | |
| ···RAC | Room Air Conditioners (Cooling Only) | | | Note [3] |

Retrofit Gross Energy Savings, Electric

Table 1: Annual Electric Energy Usage (Note [2])

| Window Type | AEH (kWh/ft ²) | AEC (kWh/ft ²) |
|------------------------------------|----------------------------|----------------------------|
| Single pane ("leaky") | 28.61 | 2.65 |
| Single pane ("tight") (baseline) | 22.02 | 2.57 |
| Double Pane (or single with storm) | 10.79 | 2.57 |
| ENERGY STAR | 5.66 | 1.49 |

$$A = \frac{D_H \times D_W}{144 \frac{in^2}{ft^2}}$$

Heating (Electric Resistive Heating and Heat Pump, Note [1]):

$$AKWH_{H.R} = (AEH_b - AEH_{es}) \times A$$

$$AKWH_{H,R} = (22.02 - 5.66) \times A$$

$$AKWH_{HR} = 16.36 \times A$$

$$AKWH_{H.HP} = 8.18 \times A$$

Cooling (CAC Only):

$$AKWH_{C,CAC} = (AEH_b - AEH_{es}) \times A$$

$$AKWH_{C,CAC} = (2.57 - 1.49) \times A$$

$$AKWH_{C,CAC} = 1.08 \times A$$

Cooling (Room A/C Only): (Note [3])

$$AKWH_{C,RAC} = (28.3\%) \times AKWH_{C,CAC}$$

$$AKWH_{C,RAC} = 0.305 \times A$$

Retrofit Gross Energy Savings, Fossil Fuel

Table 2: Annual Fossil Fuel Energy Usage

| Window Type | AGU (Ccf/ft ²) | AOU (gal/ft ²) | APG _H (gal/ft ²) |
|------------------------------------|----------------------------|----------------------------|---|
| Single pane ("leaky") | 1.39 | 1.03 | 1.57 |
| Single pane ("tight") (baseline) | 1.08 | 0.80 | 1.21 |
| Double Pane (or single with storm) | 0.53 | 0.39 | 0.59 |
| ENERGY STAR | 0.28 | 0.20 | 0.31 |

$$A = \frac{D_H \times D_W}{144 \, \frac{in^2}{ft^2}}$$

Savings by heating fuel:

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Natural Gas:

$$ACCF_{H} = (AGU_{b} - AGU_{es}) \times A$$
$$ACCF_{H} = (1.08 - 0.28) \times A$$
$$ACCF_{H} = 0.80 \times A$$

Oil:

$$AOG_{H} = (AOU_{b} - AOU_{es}) \times A$$

$$AOG_{H} = (0.80 - 0.20) \times A$$

$$AOG_{H} = 0.60 \times A$$

Propane:

$$APG_{H} = (APU_{b} - APU_{es}) \times A$$

$$APG_{H} = (1.21 - 0.31) \times A$$

$$APG_{H} = 0.90 \times A$$

Retrofit Gross Energy Savings, Example

A single pane 24" x 36" window is replaced by an ENERGY STAR window in a home cooled by central AC and heated by electric resistance.

$$A = \frac{24 \operatorname{in} \times 36 \operatorname{in}}{144^{\operatorname{sqin}}/\operatorname{sf}} = 6 \operatorname{sq} \operatorname{ft}$$

$$AKWH_{H} = 16.36 \, \frac{kWh}{sf} \times 6 \, sqft = 98 \, kWh$$
$$AKWH_{C} = 1.08 \, \frac{kWh}{sf} \times 6 \, sqft = 6.5 \, kWh$$

Retrofit Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

If home has electric heat or heat pump (Note [1]),

$$WKW = AKWH_{H,R} \times \frac{PFW}{1000 \frac{w}{kW}} = 16.36 \frac{kWh}{sf} \times A \times \frac{0.570 \frac{w}{kWh}}{1000 \frac{w}{kW}} = 0.0093 \frac{kW}{sf} \times A$$

If home has central air conditioning:

$$SKW_{C,CAC} = (0.0046 \, \frac{kW}{sf} - 0.0025 \, \frac{kW}{sf}) \times CF_S \times A$$

$$SKW_{C,CAC} = 0.0012 \, \frac{kW}{sf} \times A$$

If home has one or more room air conditioners: (Note [3])

$$SKW_{C,RAC} = (25.1\%) \times SKW_{C,CAC}$$

$$SKW_{C,RAC} = 0.00031^{kW}/_{sf} \times A$$

Retrofit Gross Peak Day Savings, Natural Gas

$$PD_H = ACCF_H \times PDF_H$$

Retrofit Gross Peak Demand Savings, Example

For the above example with electric resistance heat and central air, demand savings are as follows:

$$WKW = 0.0093 \, \frac{kW}{sf} \times 6 \, ft^2 = 0.056 kW$$

$$SKW_{CAC} = 0.0012 \, \frac{kW}{sf} \times 6 \, ft^2 = 0.0072 \, kW$$

Changes from Last Version

Updated equations to account for Room A/C savings (Note [3]).

References

- [1] Lawrence Berkeley National Laboratory, RESFEN 5.0 computer software, May 12, 2005. http://windows.lbl.gov/software
- [2] KEMA, Evaluation of the Weatherization Residential Assistance Partnership and Helps Programs (WRAP/Helps), September 10, 2010
- [3] Nexant Market Research, Inc., "Market Assessment for ENERGY STAR Room Air Conditioners in Connecticut," Cambridge, MA, 2007, pp. 17,18
- [4] RLW Analytics, "Final Report: Coincidence Factor Study: Residential Room Air Conditioners," Middletown, CT, 2008, p. iv, p. 22
- [5] ADM Associates, Inc., "Residential Central AC Regional Evaluation," Sacramento, CA, 2009, pp. 4-4

Notes

- [1] Heat pump energy savings are one half of electric resistance savings based on a 2.0 COP. Since heat pumps use backup resistance heat during winter peak, winter demand savings for heat pumps equals resistance heat demand savings.
- [2] The usage values were developed for different fuel types and windows using RESFEN from Ref [1]. The values from that analysis are shown in the tables.
- [3] Room Air Conditioning cooling savings are derived from factors found in Ref [3,4,5].

4.4.9 THERMAL ENCLOSURE

Description of Measure

Version Date: 10/30/2012

New homes that meet or exceed ENERGY STAR Thermal Enclosure criteria including Quality Installed Insulation criteria, Fully Aligned Air Barriers criteria, and Reduced Thermal Bridging criteria. In addition, homes must have at least R-40 ceiling insulation and R-21 above grade wall insulation and must have a mechanical ventilation system.

Savings Methodology

The R values for walls and ceilings reflect the nominal R value, not the total R value of the assembly. *Note: Thermal mass does not equate to R-value. Solid wood walls (log cabins) are not considered high performance walls and do not qualify because they do not meet the R-value or infiltration requirements. For rated homes, savings from this measure are superseded by REM savings.*

CFM reduction and energy analysis were based on a sample of actual ENERGY STAR rated homes in the existing residential new construction program

Inputs

| Symbol | Description | Units |
|--------|--|-------|
| A | Surface area above grade of conditioned space | sf |
| | System/Fuel Type (Electric Resistive, Heat Pump, air handler, Central A/C, Gas, Oil, Propane, etc) | |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|-------------|--|--------------------|---------|------------|
| A | Surface area above grade of conditioned space | sf | | Inputs |
| $ACCF_H$ | Annual Natural Gas Savings, Heating | Ccf | | |
| $AKWH_H$ | Annual Electric Energy Savings, Heating | kWh | | |
| $AKWH_C$ | Annual Electric Energy Savings, Cooling | kWh | | |
| AOG_H | Annual Oil Savings, Heating | Gal | | |
| APG_H | Annual Propane Savings, Heating | Gal | | |
| PD_{H} | Natural gas peak day savings – heating | | 0.00977 | Appendix 2 |
| REM | Savings using residential energy modeling software | | | Note [1] |
| REM_{SKW} | Modeled Summer kW per square foot | kW/ft ² | 0.00009 | Note [1] |
| REM_{WKW} | Modeled Winter kW per square foot | kW/ft ² | 0.00117 | Note [1] |
| SKW | Summer Demand Savings | kW | | |
| WKW | Winter Demand Savings | kW | | |

Lost Opportunity Gross Energy Savings, Electric

Table 1 –Electric Savings per square foot (Note [1])

| System type | Symbol | Energy Savings | Units |
|---------------------------------|------------------|-----------------------|---------------------|
| Electric Resistance Heat | REM _H | 1.32 | kWh/ft ² |
| Heat Pump Heating | REM_H | 0.66 | kWh/ft ² |
| Ground Source Heat Pump Heating | REM _H | 0.33 | kWh/ft ² |
| Air Handler (fan) Heating | REM_F | 0.03 | kWh/ft ² |
| Cooling | REM_C | 0.03 | kWh/ft ² |

For Electric Resistive, or Heat Pump Systems,

$$AKWH_{H} = REM_{H} \times A$$

For Fossil Fuel heating with air handling unit,

$$AKWH_H = REM_F \times A$$

Homes with Central AC,

$$AKWH_C = REM_C \times A$$

Lost Opportunity Gross Energy Savings, Fossil Fuel

Table 2 – Fossil Fuel Savings per square foot (Note [1])

| Heating Fuel | Symbol | Energy Savings | Units |
|---------------------|------------------|-----------------------|-----------------------|
| Fossil Fuel Heating | | 0.0045 | MMBtu/ft ² |
| Natural Gas | REM_G | 0.044 | Ccf/ft ² |
| Oil | REM _O | 0.032 | Gal/ ft ² |
| Propane | REM_P | 0.049 | Gal/ft ² |

For homes with natural gas heating system,

$$ACCF_H = REM_G \times A$$

For homes with oil heating system,

$$AOG_H = REM_O \times A$$

For homes with propane heating system,

$$APG_{H} = REM_{P} \times A$$

Lost Opportunity Gross Energy Savings, Example

Insulation was installed in a new home and the insulation meets the ENERGY STAR thermal bypass requirements. The home is equipped with a natural gas furnace and a central AC. The total floor area of conditioned space is 1,100 sf. What are the annual energy savings?

$$ACCF_{H} = REM_{G} \times A = 0.044 \times 1,100 = 54 \ Ccf$$

Additional electric savings claimed for air handling system,

$$AKWH_{H} = REM_{F} \times A = 0.03 \times 1,100 = 33 \text{ kWh}$$

Lost Opportunity Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

 $WKW_H = REM_{WKW} \times A$ (Electric Resistance and Heat Pump)

 $SKW_C = REM_{SKW} \times A$ (Central Air Conditioner or Heat Pump providing cooling)

Lost Opportunity Gross Peak Day Savings, Natural Gas

$$PD_H = ACCF_H \times PDF_H$$

Lost Opportunity Gross Peak Demand Savings, Example

Insulation was installed in a new home. The insulation meets the ENERGY STAR thermal bypass requirements. The home is equipped with a natural gas furnace and a central AC. The total floor area of conditioned space is 1,100 sf. What are the peak demand savings (electric and natural gas)?

Summer demand savings,

$$SKW_C = REM_{SKW} \times A = 0.00009 \times 1,100 = 0.099 \ kW$$

Natural gas peak day savings,

$$PD_{H} = ACCF_{H} \times PDF_{H} = 54 \times 0.00977 = 0.53 Ccf$$

Non Energy Benefits

Increased personal comfort.

Changes from Last Version

Added savings for ground source heat pump in Table 1

Notes

[1] REM/Rate[™] is a residential energy analysis, code compliance and rating software developed by Architectural Energy Corporation. This software calculates heating, cooling, hot water, lighting, and appliance energy loads, consumption and costs for new and existing single and multi-family homes

4.4.10 INSTALL STORM WINDOW

Description of Measure

Version Date: 10/30/2012

Installation of storm window to augment existing single pane window that is between the conditioned space and the outdoors.

Savings Methodology

The savings for this measure are calculated using the installed storm window area and usage factors develop using RESFEN (Ref [1]) to model different window types and heating fuels. The results of that analysis are shown in tables 1 & 2. The energy savings are calculated by subtracting the heating fuel specific Double Pane Value from the single pane "tight" value and multiplying by the storm window area. Because the cooling usage was the same for the baseline and the Double Pane the cooling savings are zero.

Note: Savings may not be claimed if the window is located in an unconditioned space such as an unheated porch, basement, or hallway.

Inputs

| Symbol | Description | Units |
|---------|------------------------------------|--------|
| | Number storm windows installed | |
| D_{H} | Height of the window | Inches |
| D_{W} | Width of the window | Inches |
| · | Primary existing heating fuel type | |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|----------|--|---------------------|---------|----------|
| A | Area of the window | ft ² | | |
| $ACCF_H$ | Annual Gas Savings - heating | Ccf | | |
| AEC | Annual Electric Cooling Usage | kWh/ft ² | Table 1 | Note [2] |
| AEH | Annual Electric Heating Usage | kWh/ft ² | Table 1 | Note [2] |
| AGU | Annual Gas Usage | Ccf/ft ² | Table 2 | Note [2] |
| $AKWH_H$ | Annual Electric energy savings-Heating | kWh | | |
| AOG_H | Annual Oil Savings - heating | gallons | | |
| AOU | Annual Oil Usage | gal/ft ² | Table 2 | Note [2] |
| APG_H | Annual Propane Savings - heating | gallons | | |
| APU | Annual Propane Usage | gal/ft ² | Table 2 | Note [2] |
| D_{H} | Height of the window | inch | | |
| D_{W} | Width of the window | inch | | |
| PFW | Winter Peak Factor | W per kWh | 0.570 | Ref [2] |
| SKW | Summer coincident peak demand savings | kW | | |
| WKW | Winter coincident peak demand savings | kW | | |
| •••ь | baseline | | | |
| ···dp | double pane | | | |
| •••НР | Heat Pump Heating | | | |
| ···R | Resistance Heating | | | |

Version Date: 10/30/2012

Retrofit Gross Energy Savings, Electric

Table 1: Annual Electric Energy Usage

| Window Type | AEH (kWh/ft ²) | AEC (kWh/ft ²) |
|------------------------------------|----------------------------|----------------------------|
| Single pane ("leaky") | 28.61 | 2.65 |
| Single pane ("tight") | 22.02 | 2.57 |
| Double Pane (or single with storm) | 10.79 | 2.57 |
| ENERGY STAR | 5.66 | 1.49 |

$$A = \frac{D_H \times D_W}{144 \, \frac{in^2}{ft^2}}$$

Heating (Electric Resistive Heating and Heat Pump, Note [1]):

$$AKWH_{H,R} = (AEH_b - AEH_{dp}) \times A$$

$$AKWH_{H,R} = (22.02 - 10.79) \times A$$

$$AKWH_{H,R} = 11.23 \times A$$

$$AKWH_{H,HP} = 5.62 \times A$$

Retrofit Gross Energy Savings, Fossil Fuel

Table 2: Annual Gas Energy Usage

| Window Type | AGU (kWh/ft ²) | AOU (gal/ft ²) | APG (gal/ft ²) |
|------------------------------------|----------------------------|----------------------------|----------------------------|
| Single pane ("leaky") | 1.39 | 1.03 | 1.57 |
| Single pane ("tight") | 1.08 | 0.80 | 1.21 |
| Double Pane (or single with storm) | 0.53 | 0.39 | 0.59 |
| ENERGY STAR | 0.28 | 0.20 | 0.31 |

$$A = \frac{D_H \times D_W}{144 \frac{in^2}{ft^2}}$$

Savings by heating fuel:

Gas:

$$ACCF_{H} = (AGU_{b} - AGU_{dp}) \times A = (1.08 - 0.53) \times A$$
$$ACCF_{H} = 0.55 \times A$$

Oil:

$$AOG_{H} = (AOU_{b} - AOU_{dp}) \times A = (0.80 - 0.39) \times A$$
$$AOG_{H} = 0.41 \times A$$

Propane

$$APG_{H} = (APU_{b} - APU_{dp}) \times A = (1.21 - 0.59) \times A$$

$$APG_{H} = 0.62 \times A$$

Retrofit Gross Energy Savings, Example

A new storm window is added to a single pane 24" x 36" window heated by electric resistance.

$$A = \frac{24 in \times 36 in}{144 \frac{in^2}{ft^2}} = 6 sq ft$$

$$AKWH_{H} = 11.25 \frac{kWh}{ft^{2}} \times 6 ft^{2} = 68 kWh$$

Retrofit Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

If home has electric heat or heat pump (Note [1]),

$$WKW = AKWH_{H} \times \frac{PFW}{1000 \, \text{W/}_{kW}} = 11.25 \, \text{kWh/}_{sf} \times A \times \frac{0.570}{1000} = 0.0064 \, \text{kW/}_{sf} \times A$$

SKW = 0

Retrofit Gross Peak Demand Savings, Example

For the above example with electric resistance heat and central air, demand savings are as follows:

$$WKW = 0.0064 \, \frac{kW}{sf} \times 6 \, sq \, ft = 0.038 \, kW$$
$$SKW = 0 \, kW$$

References

- [1] Lawrence Berkeley National Laboratory, RESFEN 5.0 computer software, May 12, 2005. http://windows.lbl.gov/software
- [2] KEMA, Evaluation of the Weatherization Residential Assistance Partnership and Helps Programs (WRAP/Helps), September 10, 2010

<u>Notes</u>

- [1] Heat pump savings are one half of electric resistance savings. Since heat pumps use backup resistance heat during winter peak, winter demand savings for heat pumps equals resistance heat demand savings.
- [2] The usage values were developed for different fuel types and windows using RESFEN from Ref [1]. The values from that analysis are shown in the tables.

4.4.11 INSULATE ATTIC OPENINGS

Description of Measure

Version Date: 10/30/2012

Thermal barrier applied to attic hatch, attic stairs, or whole house fan.

Savings Methodology

The energy savings are estimated in two parts: conductive savings and infiltration reduction savings. The conductive savings are calculated using a degree day analysis. The infiltration reduction will be included in the blower door reduction (Measure 4.4.4) whenever possible or be estimated based on the KEMA Evaluation (Ref [1]) in combination with ASHRAE 1997 Fundamentals Handbook (Note [1]).

Reminder: Only include the infiltration savings if infiltration from this measure was not included in a blower door test.

Inputs

| Symbol | Description | Units |
|--------|--|-------|
| | Type of attic penetration being insulated. | |
| | Was the infiltration reduction included in blower door measurements? | |
| | Heating fuel /Heating system type (Electric resistive, Heat Pump, Gas) | |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|------------------------------|--|--------------------------|---------|------------|
| A | Total area of thermal barrier | ft ² | | |
| ABTU | Annual Btu savings | Btu/yr | | |
| $ABTU_{Conductive}$ | Annual Btu savings - conductive | Btu/yr | Table 1 | |
| ABTU _{Infiltration} | Annual Btu savings - Infiltration | Btu/yr | Table 2 | |
| $ACCF_H$ | Annual Natural Gas Savings- Heating | Ccf/yr | Table 4 | |
| $AKWH_H$ | Annual Electric Savings - Heating | kWh/yr | | |
| AKWH _{Conductive} | Annual Electric Savings - Conductive | kWh/yr | Table 3 | |
| AKWH _{Infiltration} | Annual Electric Savings - Infiltration | kWh/yr | Table 3 | |
| AOG_H | Annual Oil Savings - Heating | Gal/yr | Table 4 | |
| APG_H | Annual Propane savings - Heating | Gal/yr | Table 4 | |
| EF | Heating System Efficiency (Fossil fuel) | % | 75% | Estimated |
| F_{adj} | ASHRAE adjustment factor | | 0.64 | Ref [3] |
| HDD | Heating Degree Days-CT average | ⁰ F-day | 5,885 | Ref [2] |
| PD_{H} | Peak Day savings - Heating | Ccf | Table 6 | |
| PDF_{H} | Peak Day Factor - Gas Heating | | 0.00977 | Appendix 1 |
| PF_W | Peak Factor - winter | Watts/kWh | 0.57 | Ref [1] |
| R _e | Effective R-value - existing | ft ² hr°F/Btu | Table 1 | |
| R_{i} | Effective R-value - installed | ft ² hr°F/Btu | Table 1 | |
| WKW_H | Winter Seasonal Demand Savings - Heating | kW | Table 5 | |

Retrofit Gross Energy Savings, Electric

$$ABTU = ABTU_{\mathit{Conductive}} + ABTU_{\mathit{Infiltration}}$$

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Conductive Savings: $ABTU_{Conductive} = A \times \left(\frac{1}{R_e} - \frac{1}{R_i}\right) \times HDD \times 24 \frac{hrs}{day} \times F_{adj}$

Table 1: Annual Btu Savings - Conductive

| Insulation Measure | R _e | $\mathbf{R_{i}}$ | A | ABTU _{Conductive} | | |
|------------------------|----------------|------------------|-------|-----------------------------------|--|--|
| Attic Hatch | 1.69 | 21.7 | 5.60 | 276,065 | | |
| Attic pull down Stairs | 1.69 | 11.7 | 11.25 | 514,816 | | |
| Whole House Fan | 1.32 | 11.3 | 4.00 | 241,922 | | |

Table 2: Annual Btu Savings - Infiltration

| Insulation Measure | ABTU _{Inflitration} |
|---------------------------|------------------------------|
| Attic Hatch | 154,876 |
| Attic pull down Stairs | 533,461 |
| Whole House Fan | 243,195 |

Reminder: Only include infiltration savings if measure if not included in blower door.

Annual Electric Savings:

$$AKWH_{H} = AKWH_{Conductive} + AKWH_{Infiltration}$$

 $kWh = \frac{Btu}{3.412 Rtu / kWh}$

Table 3: Annual Electric Savings

| Insulation Measure | AKWH _{Conductive} For Electric Resistive | AKWH _{Infiltration} For Electric Resistive | AKWH _{Conductive} For Heat pump | AKWH _{Infiltration} For Heat pump | | |
|------------------------|---|---|---|---|--|--|
| Attic Hatch | 81 | 45 | 40.5 | 22.5 | | |
| Attic pull down Stairs | 151 | 156 | 75.5 | 78 | | |
| Whole House Fan | 71 | 71 | 35.5 | 35.5 | | |

Reminder: Only include infiltration savings if not included in blower door measure.

Retrofit Gross Energy Savings, Fossil Fuel

Using savings from Tables 1 and 2 and an Energy Factor (EF) of 75%, the fossil fuel savings are as follows. Savings by fuel type:

Gas:
$$ACCF_H = \frac{ABTU_H}{75\% \times 102,900^{Btu}/c_{cf}}$$

Oil:
$$APG_H = \frac{ABTU_H}{75\% \times 91,330^{Btu}/_{Gal}}$$

Propane:
$$AOG_H = \frac{ABTU_H}{75\% \times 138,690^{Btu}/_{Gal}}$$

Table 4: Annual Fossil Fuel Savings

| Insulation Measure | ACCF _H | | AOG_H | | APG_H | |
|------------------------|-------------------|-------|---------|-------|---------|-------|
| | Cond | Infil | Cond | Infil | Cond | Infil |
| Attic Hatch | 3.6 | 2.0 | 2.7 | 1.5 | 4.0 | 2.3 |
| Attic pull down Stairs | 6.7 | 6.9 | 4.9 | 5.1 | 7.5 | 7.8 |
| Whole House Fan | 3.1 | 3.2 | 2.3 | 2.3 | 3.5 | 3.6 |

Reminder: Only include infiltration savings if measure if not included in blower door.

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Retrofit Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

Table 5: Winter Demand Savings

| Insulation Measure | WKW _{H Conductive} For Electric Resistive | WKW _{H Infiltration} For Electric Resistive | WKW _{H Conductive} For Heat Pump | WKW _{H Infiltration} For Heat Pump |
|------------------------|---|---|--|--|
| Attic Hatch | 0.05 | 0.03 | 0.02 | 0.01 |
| Attic pull down Stairs | 0.09 | 0.09 | 0.04 | 0.04 |
| Whole House Fan | 0.04 | 0.04 | 0.02 | 0.02 |

Retrofit Gross Peak Day Savings, Natural Gas

$$PD_H = ACCF_H \times PDF_H$$

Table 6: Peak Day Savings

| Insulation Measure | PD _{Conductive} | PD _{Infiltration} |
|------------------------|--------------------------|----------------------------|
| Attic Hatch | 0.03 | 0.02 |
| Attic pull down Stairs | 0.07 | 0.07 |
| Whole House Fan | 0.03 | 0.03 |

Changes from Last Version

Added Electric Savings for Heat Pump Table 3 (Annual savings), and Table 5 (Winter demand savings). Format adjustments to Tables 3,4, 5, and 6.

References

- [1] Evaluation of WRAP and Helps Programs, KEMA, 2010, Table ES-8, page 1-10.
- [2] Degree day data from the National Climatic Data Center, Divisional Data, CT state, Jan 1979 to Dec 2008, 30 day average. http://www7.ncdc.noaa.gov/CDO/CDODivisionalSelect.jsp
- [3] ASHRAE degree-day correction. 1989 ASHRAE Handbook Fundamentals, 28.2, Fig 1.

Notes

[1] ASHRAE 1997 Handbook – Fundamentals, page 25.16, was used calculate relative infiltration of these measures to the Infiltration savings from Ref [1].

Baseline assumptions

 $R_{\text{existing}} = 0.61 + 0.47 + 0.61 = 1.69$ for hatch and stairs

 $R_{\text{existing}} = 0.61 + 0.10 + 0.61 = 1.32$ for fan.

Where:

3/8" particle board = R 0.47

Air film = 0.61

[2] Heat pump energy savings are one half of electric resistance savings based on a 2.0 COP. Since heat pumps use backup resistance heat during winter peak, winter demand savings for heat pumps equals resistance heat demand savings.

4.4.13 INFILTRATION REDUCTION (PRESCRIPTIVE)

Description of Measure

Version Date: 10/30/2012

Prescriptive infiltration reduction measures not validated by Blower Door testing, such as Electric Outlet Covers, Door Sweep, Door Kit, Caulking and Sealing, Polyethylene Tape, Weatherstrip Door or Window, and Window Repair.

Savings Methodology

Savings from this measure shall only be claimed if a blower door test (4.4.4) is not feasible. Savings estimates based on actual measured infiltration reduction (through blower door testing) are more precise.

Note: Infiltration reduction measures must be located between conditioned space and unconditioned space (outside) to be eligible for energy savings. Savings may not be claimed for both Door Sweep and Door Kit for weatherization of a single door.

Savings are calculated by multiplying the savings per unit by the number of units and adding all the different measure types together to get total savings. No summer demand savings may be claimed since cooling energy savings are not quantified.

A weatherization project should be custom only if it clearly exhibits outlier type behavior which would clearly make the existing savings algorithms inappropriate to use and if the existing savings assumptions would produce an error of unacceptable magnitude. In such a case, the energy and demand savings should be well documented.

Inputs

| Symbol | Description |
|--------|--|
| n | Number of each air sealing unit installed |
| length | Total length installed of caulking and sealing, including polyethylene tape, in linear feet. |
| | Heating system type |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|-----------------|--|-------------|-------------|-------------------------|
| · · · gasket | Installation of air sealing gasket on an electric outlet | per gasket | Tables 1, 2 | Ref [1], p. 1-11, Table |
| | | | | ES 9 |
| · · · door kit | Installation of Door Sweep or Door Kit | per sweep | Tables 1, 2 | Ref [1], p. 1-11, Table |
| | | | | ES 9 |
| ···sealing | Foot of Caulking, Sealing, or Polyethylene Tape | per foot | Tables 1, 2 | Ref [1], p. 1-11, Table |
| | | | | ES 9 |
| ···wx | Window Repaired, Window Weatherstripped, or | per linear | Tables 1, 2 | Ref [1], p. 1-11, Table |
| | Door Weatherstripped | foot | | ES 9 |
| ACCF | Annual Natural Gas Savings | Ccf/yr | | |
| AOG | Annual Savings for Oil Heat | Gal/yr/unit | | |
| APG | Annual Savings for Propane Heat | Gal/yr/unit | | |
| EF | Fossil Fuel System Efficiency including distribution | | 0.75 | |
| | loss | | | |
| PF _S | Summer Peak Factor | W/kWh | 0.017 | Ref [1] |
| PF _W | Winter Peak Factor | W/kWh | 0.570 | Ref [1] |
| WKW | Winter Seasonal Peak Electric Demand Savings | kW | | |

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Retrofit Gross Energy Savings, Electric

Table 1: Electric Savings for Infiltration Reduction Measures

| Savings | Units | Annual Savings for Electric Resistance Heating (kWh) | Annual Savings for Heat Pump (kWh) |
|--------------------------|-------------------|---|---------------------------------------|
| AKWH _{gasket} | kWh per gasket | 9 | 4.5 |
| AKWH _{door kit} | kWh per sweep | 173 | 86.5 |
| AKWH _{sealing} | kWh per linear ft | 9.9 | 4.95 |
| AKWH _{wx} | kWh per linear ft | 11.5 | 5.75 |

Retrofit Gross Energy Savings, Fossil Fuel

Annual Btu Savings =
$$\frac{AKWH \times 3412^{Btu}/_{kWh}}{75\%}$$

Table 2: Fossil Fuel Savings for Infiltration Reduction Measures

| Measure | Units | ACCF | AOG | APG |
|----------|----------------------|-------|-------|-------|
| Gasket | fuel per gasket | 0.41 | 0.29 | 0.45 |
| Door Kit | fuel per sweep | 7.87 | 5.62 | 8.59 |
| Sealing | fuel per linear foot | 0.451 | 0.322 | 0.492 |
| WX | fuel per linear foot | 0.524 | 0.374 | 0.571 |

Retrofit Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

$$WKW = AKWH_H \times PF_W / 1000 W_{kW}$$

Retrofit Gross Peak Day Savings, Natural Gas

$$PD_H = ACCF_H \times PDF_H$$

Non Energy Benefits

Increased personal comfort and decreased draftiness.

Changes from Last Version

New input (heating system type).

References

[1] KEMA, Evaluation of the Weatherization Residential Assistance Partnership and Helps Programs (WRAP/Helps), September 10, 2010

Version Date: 10/30/2012 4.4.14 WALL INSULATION

4.4.14 WALL INSULATION

Description of Measure

Batt or blown-in insulation installed in a wall located between conditioned area and ambient (attic or outside) space.

Savings Methodology

Energy savings are calculated using parallel flow method based on a typical 2x4 wall. Factors 7/12 and 3 are used to adjust for typical wall structure and framing. The savings are calculated using a degree day analysis and the difference in the pre and post R-values.

Note: The savings presented here do not apply to walls between conditioned spaces and fully enclosed unconditioned spaces, such as porches or hallways.

Inputs

| Symbol | Description | Units |
|-------------------|----------------------------------|--------------------------|
| R _{pre} | Existing Insulation R-value | ft ² hr°F/Btu |
| R _{post} | Insulation R-value after upgrade | ft ² hr°F/Btu |
| A | Total area of wall insulation | ft ² |

| Symbol | Description | Units | Values | Comments |
|-----------------------|--|--------------------------|---------|------------|
| 1 kWh | Unit conversion | kWh | 3,412 | Unit |
| | | | Btu | conversion |
| A | Total gross area of wall insulation | ft ² | | |
| $ACCF_H$ | Annual Natural Gas Savings | Ccf/yr | | |
| AKWH | Annual Electric Energy Savings | kWh/yr | | |
| $AKWH_{H,HP}$ | Annual Electric Savings due to Heat Pump heating | kWh/yr | | |
| $AKWH_{H,R}$ | Annual Electric Savings due to electric resistance heating | kWh/yr | | |
| AOG_H | Annual Savings for Oil Heat | Gal/yr/unit | | |
| APG_H | Annual Savings for Propane Heat | Gal/yr/unit | | |
| CF | Summer Seasonal Peak Coincidence Factor | • | 0.59 | Appendix 1 |
| EER _B | Energy Efficiency Ratio, Baseline | Btu/Watt- | 11 | |
| | | hr | | |
| EF | Heating system efficiency | % | 75 | Estimated |
| F_{adj} | ASHRAE adjustment factor | | 0.64 | Ref [1] |
| HDD | Heating Degree Days, CT state average | ⁰ F-day | 5,885 | Ref [2] |
| PDF_{H} | Peak Day Factor - Heating | | 0.00977 | Appendix 1 |
| PD_{H} | Peak Day savings - Heating | | | |
| R _{existing} | Effective R-value before upgrade | ft ² hr°F/Btu | | |
| R _{new} | Effective R-value after upgrade | ft ² hr°F/Btu | | |
| R _{pre} | Existing Insulation R-value | ft ² hr°F/Btu | | |
| R _{post} | Insulation R-value after upgrade | ft ² hr°F/Btu | | |
| SEERB | Seasonal Energy Efficiency Ratio, Baseline | Btu/Watt- | 13 | |
| | | hr | | |
| SKW | Summer Peak Demand Savings | kW | | |
| WKW | Winter Peak Demand Savings | kW | | |
| WPF | Winter Peak Factor | W/ kWh | 0.57 | Ref [4] |

| Symbol | Description | Units | Values | Comments |
|---------------------|---|-------|---------|-----------------|
| ΔT_{Bin} | Γ_{Bin} The sum of the temperature BIN hours (based on Hartford) | | 3,888 | Ref [3]a |
| | times delta between outside air for each BIN and average | | | |
| | indoor temperature ($T_i = 76.5$ °F) | | | |
| ΔT_{summer} | Temperature Difference | °F | 20.5 °F | Ref [3] a and b |
| | (peak $T_{\text{outside}} = 97 \text{ °F}, T_{\text{inside}} = 76.5 \text{ °F}$) | | | |
| CAC | Central Air Conditioner | | | |
| RAC | Room Air Conditioners (Cooling Only) | | | Note [1] |

Retrofit Gross Energy Savings, Electric

Effective R-value,

$$R_{existing} = \left(\frac{7}{12} \times R_{pre}\right) + 3$$

$$R_{new} = \left(\frac{7}{12} \times R_{post}\right) + 3$$

Heating Savings,

$$ABTU_{H} = \left(\frac{1}{R_{existing}} - \frac{1}{R_{new}}\right) \times HDD \times 24 \times F_{Adj} \times A$$

For Electric Resistance Heating,

$$AKWH_{H,R} = \frac{ABTU_H}{3.412}$$

For Heat Pump,

$$AKWH_{H,HP} = \frac{AKWH_{H,R}}{2}$$

Cooling Savings (Central A/C only),

$$AKWH_{C,CAC} = \left(\frac{1}{R_{existing}} - \frac{1}{R_{new}}\right) \times \Delta T_{Bin} \times A \times \frac{1}{SEER_B \times 1,000}$$

Cooling Savings (Room A/C only), Note[1]

$$AKWH_{C,RAC} = (28.3\%) \times AKWH_{C,CAC}$$

Retrofit Gross Energy Savings, Fossil Fuel

$$ACCF_{H} = \frac{ABTU_{H}}{75\% \times 102,900}$$

$$APG_{H} = \frac{ABTU_{H}}{75\% \times 91{,}330}$$

$$AOG_H = \frac{ABTU_H}{75\% \times 138,690}$$

Reminder: System Efficiency is 75%

Retrofit Gross Energy Savings, Example

Insulation in a house is upgraded from R-6 to a total of R-13. The total square feet insulation added is 100. The home is heated by electric resistance heating system and has a central AC. What are the annual electric energy savings?

$$R_{existing} = \left(\frac{7}{12} \times R_{pre}\right) + 3$$

$$R_{new} = \left(\frac{7}{12} \times R_{post}\right) + 3$$

$$R_{existing} = \left(\frac{7}{12} \times 6\right) + 3$$

$$R_{new} = \left(\frac{7}{12} \times 13\right) + 3$$

$$R_{new} = 10.6$$

Using the equation for heating savings,

$$ABTU_{H} = \left(\frac{1}{R_{existing}} - \frac{1}{R_{new}}\right) \times HDD \times 24 \times F_{Adj} \times A$$

$$ABTU_{H} = \left(\frac{1}{6.5} - \frac{1}{10.6}\right) \times 5,885 \times 24 \times 0.64 \times 100$$

$$ABTU_{H} = 537,901 Btu$$

Heating savings for electric resistance system,

$$AKWH_{H,R} = \frac{ABTU_{H}}{3,412}$$

$$AKWH_{H,R} = \frac{537,901}{3,412}$$

$$AKWH_{H,R} = 158 \text{ kWh}$$

Using the equation for cooling savings,

$$AKWH_{C,CAC} = \left(\frac{1}{R_{existing}} - \frac{1}{R_{new}}\right) \times \Delta THR \times A \times \frac{1}{SEER_B \times 1,000}$$

$$AKWH_{C,CAC} = \left(\frac{1}{6.5} - \frac{1}{10.6}\right) \times 3,888 \times 100 \times \frac{1}{13 \times 1,000}$$

$$AKWH_{C,CAC} = 1.8kWh$$

Retrofit Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

For homes with electric resistance heat,

$$WKW = \frac{AKWH_H (Electric_Resistance)}{1.000} \times WPF$$

$$WKW = \frac{AKWH_H \text{(Electric_Resistance)}}{1.000} \times 0.57$$

For homes with heat pump,

$$WKW = \frac{AKWH_H}{1,000} \times 0.57$$

For Central A/C only,

$$SKW_{CAC} = CF \times \left(\frac{1}{R_{existing}} - \frac{1}{R_{new}}\right) \times \Delta T_{Summer} \times A \times \frac{1}{EER_B \times 1,000}$$

For Room A/C only, (Note [1])

$$SKW_{RAC} = (25.1\%) \times SKW_{CAC}$$

Retrofit Gross Peak Day Savings, Natural Gas

$$PDF_{H} = 0.00977$$

 $PD_{H} = ACCF_{H} \times PDF_{H}$

Retrofit Gross Peak Demand Savings, Example

Insulation in a house is upgraded from R-6 to a total of R-13. The total square feet insulation added is 100. The home is heated by electric resistance heating system and has a central AC. What are the demand savings?

Using the equation,

$$WKW = \frac{AKWH_H \text{(Electric_Resistance)}}{1,000} \times 0.57$$

From the previous example, $AKWH_H = 158 \text{ kWh}$, therefore,

$$WKW = \frac{158}{1,000} \times 0.57$$

$$WKW = 0.090kW$$

Using the equation,

$$\begin{split} SKW_{CAC} &= CF \times \left(\frac{1}{R_{existing}} - \frac{1}{R_{new}}\right) \times \Delta T_{Summer} \times A \times \frac{1}{EER_B \times 1,000} \\ SKW_{CAC} &= 0.59 \times \left(\frac{1}{6.5} - \frac{1}{10.6}\right) \times 20.5 \times 100 \times \frac{1}{11 \times 1,000} \\ SKW_{CAC} &= 0.0065 kW \end{split}$$

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Changes from Last Version

Updated measure to account for Room A/C savings.

References

- [1] ASHRAE degree-day correction.1989 ASHRAE Handbook Fundamentals, 28.2, Fig 1.
- [2] Degree day data from the National Climatic Data Center, Divisional Data, CT state, Jan 1979 to Dec 2008, 30 day average. http://www7.ncdc.noaa.gov/CDO/CDODivisionalSelect.jsp
- [3] Residential Central AC Regional Evaluation, ADM Associates, Inc., November 2009, a) Table B-4 (Hartford) and page B-9 and b) Figures 4-1&2 (Hartford) and page 4-15.
- [4] Evaluation of WRAP and Helps Programs, KEMA, 2010, Table ES-8, page 1-10.
- [5] Nexant Market Research, Inc., "Market Assessment for ENERGY STAR Room Air Conditioners in Connecticut," Cambridge, MA, 2007, pp. 17,18
- [6] RLW Analytics, "Final Report: Coincidence Factor Study: Residential Room Air Conditioners," Middletown, CT, 2008, p. iv, p. 22
- [7] ADM Associates, Inc., "Residential Central AC Regional Evaluation," Sacramento, CA, 2009, pp. 4-4

Notes

[1] Room Air Conditioning cooling savings are derived from factors found in Ref [5,6,7].

4.4.15 CEILING INSULATION

Description of Measure

Version Date: 10/30/2012

Installation of batt or loose fill insulation located between conditioned area and ambient (attic or outside) space.

Savings Methodology

Energy savings are calculated using parallel flow method and typical ceiling structure. The savings are calculated using a degree day analysis and the difference in the pre and post R-values. The conductive savings are calculated using a degree day analysis. 0.5, 3 and 2 are factors used to adjust for typical wall structure/framing.

Note: The savings presented here do not apply to ceilings between conditioned space and fully enclosed unconditioned spaces, such as basement ceilings. It is assumed that attics are properly ventilated to the outside.

Inputs

| Symbol | Description | Units |
|-------------------|--|--------------------------|
| R _{pre} | Existing Insulation R-value | ft ² hr°F/Btu |
| R _{post} | Insulation R-value after upgrade | ft ² hr°F/Btu |
| A | Total gross area of ceiling insulation | ft^2 |

| Symbol | Description | Units | Values | Comments |
|-------------------|--|--------------------------|------------|------------|
| A | Total gross area of ceiling insulation | ft ² | | |
| AKWH | Annual Electric Energy Savings | kWh | | |
| $ACCF_H$ | Annual Natural Gas Savings | Ccf/yr | | |
| AKWH | Annual Electric Energy Savings | kWh/yr | | |
| $AKWH_{H,HP}$ | Annual Electric Savings due to Heat Pump heating | kWh/yr | | |
| $AKWH_{H,R}$ | Annual Electric Savings due to electric resistance heating | kWh/yr | | |
| AOG_H | Annual Savings for Oil Heat | Gal/yr/unit | | |
| APG_H | Annual Savings for Propane Heat | Gal/yr/unit | | |
| CF | Summer Seasonal Peak Coincidence Factor | | 0.59 | Appendix 1 |
| EER _B | Energy Efficiency Ratio, Baseline | Btu/Watt-hr | 11 | |
| EF | Heating system efficiency (Fossil fuel) | % | 75% | Estimated |
| F_{adj} | ASHRAE adjustment factor | | 0.64 | Ref [1] |
| HDD | Heating Degree Days, CT state average | ⁰ F-day | 5,885 | Ref [2] |
| PD_H | Peak Day savings - Heating | | | |
| PDF_{H} | Peak Day Factor - Heating | | 0.00977 | Appendix 1 |
| Rexisting | Effective R-value before upgrade | ft ² hr°F/Btu | Calculated | |
| R _{new} | Effective R-value after upgrade | ft ² hr°F/Btu | Calculated | |
| R _{pre} | Existing Insulation R-value | ft ² hr°F/Btu | Input | |
| R _{post} | Insulation R-value after upgrade | ft ² hr°F/Btu | Input | |
| SEERB | Seasonal Energy Efficiency Ratio, Baseline | Btu/Watt-hr | 13 | |
| SKW | Summer Peak Demand Savings | kW | | |
| WKW | Winter Peak Demand Savings | kW | | |
| WPF | Winter Peak Factor | W/ kWh | 0.57 | Ref [4] |
| ΔT_{Bin} | Is the sum of the temperature BIN hours (based on | | 3,888 | Ref [3]a |

| Symbol | Description | Units | Values | Comments |
|---------------------|--|-------|---------|-----------------|
| | Hartford) times delta between outside summer air for | | | |
| | each BIN and average indoor temperature ($T_i = 76.5$ °F) | | | |
| ΔT_{summer} | Temperature Difference | °F | 20.5 °F | Ref [3] a and b |
| | $(\text{peak T}_{\text{outside}} = 97 \text{ °F}, \text{T}_{\text{inside}} = 76.5 \text{ °F})$ | | | |
| ···H,R | Electric Resistance Heating | | | |
| •••Н,НР | Heat Pump Heating | | | |
| ···C,CAC | Central A/C cooling | | | |
| ···C,RAC | Room A/C cooling | | | Note [1] |

Retrofit Gross Energy Savings, Electric

Table 1: Effective R-values

| If | Use | | |
|-----------------------|---|--|--|
| $R_{pre} < 10$ | $R_{existing} = (0.5 \times R_{pre}) + 3$ | | |
| If $R_{pre} >= 10$ | $R_{existing} = R_{pre} - 2$ | | |
| R _{post} <10 | $R_{new} = (0.5 \times R_{post}) + 3$ | | |
| $R_{post} >= 10$ | $R_{new} = R_{post} - 2$ | | |

$$ABTU_{H} = \left(\frac{1}{R_{existing}} - \frac{1}{R_{new}}\right) \times HDD \times 24 \times F_{Adj} \times A$$

For Electric Resistance Heating Savings,

$$AKWH_{H,R} = \frac{ABTU_H}{3,412^{Btu}/_{kWh}}$$

For Heat Pump,

$$AKWH_{_{H,HP}} = \frac{AKWH_{_{H,R}}}{2}$$

Cooling Savings (Central A/C only),

$$AKWH_{C,CAC} = \left(\frac{1}{R_{existing}} - \frac{1}{R_{new}}\right) \times \Delta T_{Bin} \times A \times \frac{1}{SEER_B \times 1,000}$$

Cooling Savings (Room A/C only), Note [1]

$$AKWH_{C,RAC} = (28.3\%) \times AKWH_{C,CAC}$$

Retrofit Gross Energy Savings, Fossil Fuel

$$ACCF_{H} = \frac{ABTU_{H}}{75\% \times 102,900 \frac{Btu}{Cef}}$$
$$APG_{H} = \frac{ABTU_{H}}{75\% \times 91,330 \frac{Btu}{Cef}}$$

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$$AOG_H = \frac{ABTU_H}{75\% \times 138,690^{Btu/Gal}}$$

Reminder: EF = 75%

Retrofit Gross Energy Savings, Example

Ceiling insulation in a house is upgraded from R-9 to a total of R-60. The total square feet insulation added is 1000. The home is heated by electric resistance heating system and has a central AC. What are the annual electric energy savings?

Since
$$R_{pre} < 10$$
; Since $R_{post} > = 10$; $R_{existing} = (0.5 \times R_{pre}) + 3$ $R_{new} = R_{post} - 2$ $R_{existing} = (0.5 \times 9) + 3 = 7.5$ $R_{new} = 60 - 2 = 58$

$$\begin{split} ABTU_{H} = & \left(\frac{1}{R_{existing}} - \frac{1}{R_{new}}\right) \times HDD \times 24 \times F_{Adj} \times A \\ ABTU_{H} = & \left(\frac{1}{7.5} - \frac{1}{58}\right) \times 5,885 \times 24 \times 0.64 \times 1000 = 10,493,969 \; Btu \end{split}$$

$$AKWH_{H,R} = \frac{ABTU_{H}}{3,412^{Btu}/_{kWh}}$$

$$AKWH_{H,R} = \frac{10,493,969 \ Btu}{3,412^{Btu}/_{kWh}} = 3075 \ kWh$$

$$AKWH_{C,CAC} = \left(\frac{1}{R_{existing}} - \frac{1}{R_{new}}\right) \times \Delta THR \times A \times \frac{1}{SEER_{B} \times 1,000}$$
$$AKWH_{C,CAC} = \left(\frac{1}{7.5} - \frac{1}{58}\right) \times 3,888 \times 1,000 \times \frac{1}{13 \times 1,000} = 35kWh$$

Retrofit Gross Seasonal Peak Demand Savings, Electric, Winter, and Summer

For homes with electric resistance heat,

$$WKW = \frac{AKWH_{H,R}}{1,000} \times WPF$$

$$WKW = \frac{AKWH_{H,R}}{1,000} \times 0.57$$

For homes with heat pump,

$$WKW = \frac{AKWH_{H,HP}}{1,000} \times 0.57$$

For Homes with Central A/C only or heat pump providing cooling,

$$SKW_{C,CAC} = CF \times \left(\frac{1}{R_{existing}} - \frac{1}{R_{new}}\right) \times \Delta T_{Summer} \times A \times \frac{1}{EER_B \times 1,000}$$

$$SKW_{C,CAC} = CF \times \left(\frac{1}{R_{existing}} - \frac{1}{R_{new}}\right) \times 20.5 \times A \times \frac{1}{11 \times 1,000}$$

For Homes with Room A/C only, (Note [1])

$$SKW_{C,RAC} = (25.1\%) \times SKW_{C,CAC}$$

Retrofit Gross Peak Day Savings, Natural Gas

$$PDF_H = 0.00977$$

$$PD_H = ACCF_H \times PDF_H$$

Retrofit Gross Peak Demand Savings, Example

Ceiling insulation in a house is upgraded from R-9 to a total of R-60. The total square feet insulation added is 1000. The home is heated by electric resistance heating system and has a central AC. What are the demand savings?

Using the equation for winter demand savings,

$$WKW = \frac{AKWH_{H,R}}{1,000} \times 0.57$$

From previous example, $AKWH_H = 308 \text{ kWh}$. Therefore,

$$WKW = \frac{3075}{1,000} \times 0.57 = 1.75 \ kW$$

Using the equation for summer demand savings,

$$SKW_{C,CAC} = CF \times \left(\frac{1}{R_{existing}} - \frac{1}{R_{new}}\right) \times \Delta T_{Summer} \times A \times \frac{1}{EER_B \times 1,000}$$

$$SKW_{C,CAC} = 0.59 \times \left(\frac{1}{7.5} - \frac{1}{58}\right) \times 20.5 \times 1000 \times \frac{1}{11 \times 1,000}$$

 $SKW_{C,CAC} = 0.127kW$

Changes from Last Version

Updated measure to account for Room A/C savings.

References

Version Date: 10/30/2012

- [1] ASHRAE degree-day correction.1989 ASHRAE Handbook Fundamentals, 28.2, Fig 1.
- [2] Degree day data from the National Climatic Data Center, Divisional Data, CT state, Jan 1979 to Dec 2008, 30 day average. http://www7.ncdc.noaa.gov/CDO/CDODivisionalSelect.jsp
- [3] Residential Central AC Regional Evaluation, ADM Associates, Inc., November 2009, a) Table B-4 (Hartford) and page B-9 and b) Figures 4-1&2 (Hartford) and page 4-15.
- [4] Evaluation of WRAP and Helps Programs, KEMA, 2010, Table ES-8, page 1-10.
- [5] Nexant Market Research, Inc., "Market Assessment for ENERGY STAR Room Air Conditioners in Connecticut," Cambridge, MA, 2007, pp. 17,18
- [6] RLW Analytics, "Final Report: Coincidence Factor Study: Residential Room Air Conditioners," Middletown, CT, 2008, p. iv, p. 22
- [7] ADM Associates, Inc., "Residential Central AC Regional Evaluation," Sacramento, CA, 2009, pp. 4-4

Notes

[1] Room Air Conditioning cooling savings are derived from factors found in Ref [5,6,7].

Version Date: 10/30/2012 4.5 WATER HEATING

4.5 WATER HEATING

4.5.1 WATER HEATER THERMOSTAT SETTING

Description of Measure

Lowering the temperature set point of a domestic hot water heater.

Savings Methodology

Please see the tables below. Savings occur only when the lower temperature of the hot water does not require the use of more hot water. Savings do not occur in an application such as a shower or faucet where the user demands a certain water temperature and will increase the hot water flow to make up for the lower temperature. Additionally, this measure may increase a dishwasher's electricity consumption due to the lower hot water supply temperature; therefore negative electric energy adjustment is made when the home has a dishwasher.

Inputs

| Symbol | Description |
|---------------------|---|
| Dishwasher presence | Whether or not home has dishwasher |
| WH fuel | Type of fuel used in hot water heater. |
| T_{BR} | Temperature of hot water from tank before reset |
| T_{AR} | Temperature of hot water from tank after reset |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|---------------------|---|------------|--------|---------------------|
| $ACCF_W$ | Annual Gas Savings | Ccf/yr | | |
| $AKWH_{noDW}$ | Annual Electric Energy Savings – with no dishwasher | kWh/ yr | | |
| AKWH _{neg} | Annual Electric Energy Savings – Dishwasher | kWh/ yr | | Negative adjustment |
| $AKWH_W$ | Annual Electric Energy Savings – Water Heating | kWh/ yr | | |
| AOG_W | Annual Oil Savings | Gal/yr | | |
| APG_W | Annual Propane Savings | Gal/yr | | |
| EF_{E} | Energy Factor of Electric Water Heater | | 0.95 | Ref [4] |
| EF_F | Energy Factor of Fossil Fuel Water Heater | | 0.62 | Ref [4] |
| T_{BR} | Temperature of hot water from tank before reset | °F | | |
| T_{AR} | Temperature of hot water from tank after reset | °F | | |
| D_{w} | Density of water | lbs/gallon | 8.3 | |

Retrofit Gross Energy Savings, Electric

Table 1: Hot Water Consumption of Clothes Washer

| Table 1: Hot water Consumption of Clothes washer | | | |
|---|---------|--|--|
| Number of cycles per year | 392.0 | | |
| Water use per cycle (Note [1]) | 26.16 | | |
| Percent Hot Water (Ref [1]) | 29% | | |
| Annual clothes washer hot water consumption (Gal) - W _{cw} | 2,974.2 | | |

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Table 2: Hot Water Consumption of Dishwasher

| Number of cycles per year (Ref [4]) | 215.0 |
|---|-------|
| Water use per cycle (Note [1]) | 4.36 |
| Percent Hot Water (Ref [1]) | 100% |
| Annual dishwasher hot water consumption (Gal) - W_{dw} | 937.4 |

Use the following equation to calculate total electricity saved per year at water heater for electric heat without dishwasher. The following savings are due to lowering of electric hot water heater temperature from T_{BR} to T_{AR} .

$$E_{cw} = \frac{D_w \times W_{cw} \times (T_{BR} - T_{AR})}{10^6} MMBtu$$

The electric savings is given below:

$$AKWH_{noDW} = \frac{E_{cw} \times 10^6}{3412 \times EF_E} \, kWh$$

Where, EF = 0.95, is the energy factor of the hot water system.

If the home has a dishwasher,

Negative adjustment to account for dishwasher preheater:

$$E_{dw} = \frac{D_w \times W_{dw} \times (T_{BR} - T_{AR})}{10^6} MMBTU$$

Negative electric energy adjustment is as follows:

$$AKWH_{neg} = -\frac{E_{dw} \times 10^6}{3412 \times EF_F} kWh$$

Where, EF = 0.95, is the energy factor of the hot water system.

Total electricity saved per year at water heater for electric heat with dishwasher:

$$AKWH_{w} = AKWH_{noDW} + AKWH_{neg}$$

If the before and after reset temperatures are unknown, use the following deemed savings. See Note [2].

Total electricity saved per year without dishwasher: 114.2 kWh

Total electricity saved per year with dishwasher: 80 kWh

Retrofit Gross Energy Savings, Fossil Fuel

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| Table 3: Savings for Homes with Gas Water HeatersNatural gas savings = savings in BTU / EF_F / 102,900 Btu/Ccf | | | |
|--|--|--|--|
| Gas saved per year at the water heater (MMBtu) | $E_{cw} = \frac{D_w \times W_{cw} \times (T_{BR} - T_{AR})}{10^6} MMBtu$ | | |
| Gas Water Heater Energy Factor (Ref [3]) | 0.62 | | |
| Total gas saved per year at water heater, ACCF _W (Ccf) | $ACCF_{w} = \frac{E_{cw}}{102,900}Ccf$ | | |
| When dishwasher is present, Electricity Savings Due to Dishwasher Preheater, AKWH _{ney} (kWh) | $AKWH_{neg} = -\frac{E_{dw} \times 10^6}{3412 \times EF_E} kWh$ | | |

| Table 4: Savings for Homes with Oil Hot Water HeatersNumber 2 oil saved = savings in BTU / water heater EF / 138,690 | | | | |
|--|--|--|--|--|
| No 2 oil BTU per gallon | 138,690 | | | |
| Oil saved at the water heater (Gal) | $E_{cw} = \frac{D_w \times W_{cw} \times (T_{BR} - T_{AR})}{10^6} MMBtu$ | | | |
| Oil Fired Water Heater Energy Factor (Ref [3]) | 0.62 | | | |
| Total oil saved per year at water heater, $\mathbf{AOG}_{\mathbf{W}}\left(\mathbf{Gal}\right)$ | $AOG_{w} = \frac{E_{cw}}{138,690} Gallons$ | | | |
| When dishwasher is present, Electricity Savings Due to Dishwasher Preheater, $AKWH_{neg}$ (kWh) | $AKWH_{neg} = -\frac{E_{dw} \times 10^6}{3412 \times EF_E} kWh$ | | | |

Table 5: Savings for Homes with Propane Water Heaters

| rable 5: Savings for Homes with Propane water Heaters | | | |
|--|--|--|--|
| Number 2 propane saved = savings in BTU / water heater EF / 91,330 | | | |
| Propane BTU per gallon | 91,330 | | |
| | $E_{cw} = \frac{D_w \times W_{cw} \times (T_{BR} - T_{AR})}{10^6} MMBtu$ | | |
| Propane saved at the water heater (Gal) | 10° | | |
| Propane Fired Water Heater Energy Factor (Ref [3]) | 0.62 | | |
| Total Propane saved per year at water heater, APG _W (Gal) | $APG_{w} = \frac{E_{cw}}{91,330} Gallons$ | | |
| When dishwasher is present, Electricity Savings Due to Dishwasher Preheater, AKWH _D (kWh) | $AKWH_{neg} = -\frac{E_{dw} \times 10^6}{3412 \times EF_E} kWh$ | | |

Retrofit Gross Energy Savings, Example

Version Date: 10/30/2012

What is the energy savings from lowering of electric hot water heater temperature from 140°F to 125 °F?

Using equation,

$$E_{cw} = \frac{D_w \times W_{cw} \times (T_{BR} - T_{AR})}{10^6} MMBtu$$

$$E_{cw} = \frac{8.3 \times 2,974.2 \times (140 - 125)}{10^6} = 0.37 MMBtu$$

The electric savings is given below:

$$AKWH_{noDW} = \frac{E_{cw} \times 10^6}{3412 \times EF_E} kWh$$
$$AKWH_{noDW} = \frac{0.37 \times 10^6}{3412 \times EF_E} kWh$$

Where, EF =0.95, is the energy factor of the hot water system. Therefore, annual electric energy savings is

$$AKWH_{noDW} = \frac{0.37 \times 10^6}{3412 \times 0.95} = 114.2kWh$$

If the home has a dishwasher,

Negative adjustment has to be made to account for dishwasher preheater:

$$E_{dw} = \frac{D_w \times W_{dw} \times (T_{BR} - T_{AR})}{10^6} MMBTU$$

$$E_{dw} = -\frac{8.3 \times 937.4 \times (140 - 125)}{10^6} = -0.12 MMBtu$$

Negative electric energy adjustment is as follows:

$$AKWH_{neg} = -\frac{0.12 \times 10^6}{3412 \times EF_E} = -34.2kWh$$

Where, EF = 0.95, is the energy factor of the hot water system.

Therefore, total electricity saved per year at water heater for electric heat with dishwasher:

$$AKWH_{w} = AKWH_{noDW} - AKWH_{neg}$$

 $AKWH_{w} = 114.2 - 34.2 = 80kWh$

Changes from Last Version

New inputs (T_{BR} and T_{AR}) present. Several deemed values changed to calculated values.

References

Version Date: 10/30/2012

- [1] Table 2, LBNL-35475, "The Effect of Efficiency Standards on Water Usage and Water Heating Energy Use in the U.S.: A Detailed End-use Treatment", May 1994
- [2] US EPA ENERGY STAR Energy Savings Calculator, 2008.
- [3] Federal Register Part III, DOE Energy Conservation Program: Energy Conservation Standards for Residential Water Heaters, Direct Heating Equipment, Pool Heater; Final Rule, Table I.2. April 16, 2010.
- [4] DOE Federal Test Procedure 10 CFR 430, Appendix C, as of June 20, 2011.

Notes

- [1] Weighted average of ENERGY STAR and conventional water consumption from (Ref [2]).
- [2] The deemed savings are calculated based on 'before' temperature at 140 F and the 'reset' temperature at 125F.

4.5.2 WATER HEATER WRAP

Description of Measure

Version Date: 10/30/2012

Wrapping old electric hot water heaters with fiberglass insulation with an insulating blanket to reduce standby heat loss through the skin. Not valid for newer units which are already insulated with foam or units that are already wrapped in insulation.

Savings Methodology

The (deemed) savings for this measure are calculated based on the water heating load calculated in measure 4.5.7 and the difference of efficiency between an existing electric resistance water heater without and with an insulating blanket. Oak Ridge National Laboratory performed a study to determine the increase in water heater energy factor (EF) due to the additional insulation (Ref [1]). In this study, the home studied in the Northeast had a gas fired water heater, and was not applicable, since only electric water heaters are wrapped in this program. The southern home in the study did have an electric water heater. The difference in the actual heating and storage of hot water may be a little different in the South versus the Northeast, but the southern home can still be used as a good approximation (Note [1]).

The Oak Ridge study (Ref [1]) predicted that wrapping a 40 gallon water heater would result in an increase in the energy factor (EF) from 0.86 to 0.88. The calculations below show how a reasonable deemed savings estimate of 87 kWh has been derived.

No demand savings are claimed for this measure since there is insufficient peak coincident data.

Inputs

| Symbol | Description | Comments |
|--------|-------------------|---|
| | Water Heater Fuel | This should only be applied to electric water heaters |
| EF | Existing EF | Not required for savings calculation |

| Symbol | Description | Units | Values | Comments |
|--------------|--|---------|--------|---------------|
| $ABTU_W$ | Annual BTU savings – water heating | Btu | | |
| ADHW | Annual domestic hot water load | Btu | | |
| $AKWH_W$ | Annual Electric Energy Savings – Water Heating | kWh/ yr | 87 kWh | Deemed |
| EF_B | Energy Factor - Baseline | | 0.86 | Ref [1] |
| EF_{I} | Energy factor – Insulated Unit | | 0.88 | Ref [1] |
| GPY | Annual domestic hot water usage in Gallons | Gal/yr | 19,839 | Measure 4.5.7 |
| $T_{ m dhw}$ | Domestic hot water heater set point | °F | 125 | Measure 4.5.1 |
| T_{aiw} | Average annual incoming water temperature | °F | 57 | Note [2] |

Retrofit Gross Energy Savings, Electric

$$ADHW = GPY \times 8.3 \frac{lbs}{gal} \times (T_{dhw} - T_{aiw})$$

 $ADHW = 19,839 \times 8.3 \frac{lbs}{gal} \times (125 - 57)$
 $ADHW = 11,197,132Btu$

$$ABTU_{W} = ADHW \times \left(\frac{1}{EF_{B}} - \frac{1}{EF_{I}}\right)$$

$$ABTU_{W} = 11,197,132 \times \left(\frac{1}{0.86} - \frac{1}{0.88}\right) = 295,907 Btu$$

$$AKWH_{W} = \frac{ABTU_{W}}{3412 \frac{Btu}{kWh}} = \frac{295,907 Btu}{3412 \frac{Btu}{kWh}}$$

$$AKWH_{W} = 87 \text{ kWh}$$

References

- [1] Oak Ridge National Laboratory. "Meeting the Challenge: The Prospect of Achieving 30 Percent Energy Savings Through the Weatherization Assistance Program," May 2002.
- [2] Tool for Generating Realistic Residential Hot Water Event Schedules, Preprint, NREL, August 2010.

<u>Notes</u>

- [1] The temperature of the water entering the heater may be warmer in the South versus the Northeast, especially in the winter, but this would not affect standby losses which the wrapping seeks to reduce. The other difference is that the heat loss from the tank to the environment may be greater in the Northeast than the South because of milder Southern winters and the warmer Southern summers. However, the Southern house can be used as a good conservative approximation to a house in the Northeast.
- [2] These values were developed using the Tool in Ref [2] for Hartford area weather data and a three bedroom house.

4.5.3 SHOWERHEAD

Description of Measure

Installation of low flow showerheads meeting the EPA WaterSense specification (2.0 gpm) (Ref [1]) to replace Federal Standard (2.5 gpm) or higher flow showerheads.

Savings Methodology

Savings shall be claimed based on the type of fuel used for water heating. Water savings is based on the difference between the Federal Standard (2.5 gpm) versus WaterSense (2.0 gpm).

No electric demand savings are claimed for this measure because there is insufficient peak coincident data.

Inputs

| Symbol | Description |
|--------------------------|--|
| WH Fuel | Water Heater Fuel Type |
| n_{i} | Number of low flow showerheads installed |
| gpm _{installed} | Flow rate of installed showerhead (not required for savings) |

| Symbol | Description | Units | Values | Comments |
|---------------------|---|-----------|------------------|------------------------|
| AKWH | Annual Electric savings for homes with | kWh/yr | Calculated | |
| | Electric HW | | | |
| ACCF | Annual Gas Savings | Ccf/yr | Calculated | |
| AOG | Annual Oil Savings | Gal/yr | Calculated | |
| APG | Annual Propane Savings | Gal/yr | Calculated | |
| AWG | Annual Water Savings | Gal/yr | Calculated | |
| d_e | Median duration per event | minutes | 8.3 | Ref [4] |
| d_{W} | Density of water | lb/ Gal | 8.31 | |
| EF_{E} | Energy Factor of Electric Water Heater | | 0.95 | Ref [3] |
| EF_{F} | Energy Factor of Fossil Fuel Water Heater | | 0.62 | Ref [3] |
| gpm | Gallons per minute flow rate | gal/min | Fed Std: 2.5 | Ref [1] |
| | | | Water Sense: 2.0 | |
| n _a | Average total number showerheads per | | 2.3 | Ref [4], p185-186 |
| | household | | | Table 66 |
| n _e | Average number of shower events per day | | 1.97 | Ref [4], p144 Table 41 |
| | per household | | | |
| n_i | number of low flow showerheads installed | | As found | |
| r_g | Ratio to adjust usage for cooler climate | | 0.9344 | Note [1], Ref [4] |
| S_{W} | Annual Water Savings per showerhead | gal/yr | Calculated | |
| SH_W | Specific Heat of Water | BTU/lb-ºF | 1 | |
| T_{shower} | Temperature of water from shower | °F | 105 °F | |
| T _{supply} | Temperature of water into house | °F | 55 °F | |
| PDF_{WH} | Peak Day Factor, Water Heating | | 0.00321 | Appendix 1 |
| PD_{WH} | Peak Day savings, Water Heating | | | |

Retrofit Gross Energy Savings, Electric

$$S_{W} = n_{e} \times d_{e} \times 365^{days}/_{yr} \times r_{g} \times \left(gpm_{federal\ std} - gpm_{WaterSense}\right)/n_{a}$$

$$S_{W} = 1.97\ events \times 8.3\ ^{min}/_{event} \times 365^{days}/_{yr} \times 0.9344 \times (2.5\ gpm - 2.0\ gpm)/2.3$$

$$S_{W} = 1,212.3\ ^{Gal}/_{showerhead-yr}$$

$$MMBtu\ Savings = \sqrt{n_{i}} \times \left(T_{shower} - T_{Supply}\right) \times d_{W} \times SH_{W} \times S_{W}/10^{6}\ ^{Btu}/_{MMBtu} \quad \text{(See Note [2])}$$

$$MMBtu\ Savings = \frac{\sqrt{n_{i}} \times \left(T_{shower} - T_{sup\ ply}\right)}{10^{6}\ ^{Btu}/_{MMBtu}} \times d_{W} \times SH_{W} \times S_{W}/10^{6}\ ^{Btu}/_{MMBtu}$$

$$MMBtu\ Savings = \frac{\sqrt{n_{i}} \times \left(105^{\circ}F - 55^{\circ}F\right)}{10^{6}\ ^{Btu}/_{MMBtu}} \times 8.31^{lb}/_{Gal} \times 1 \times 1,212.3^{Gal}/_{showerhead-yr}$$

MMBtu Savings =
$$0.504 \frac{MMBtu}{showerhead} \times \sqrt{n_i}$$

$$AKWH = \frac{MMBtu_Savings}{0.003412^{MMBtu}/_{kWh} \times EF_E} = \frac{0.504 \times \sqrt{n_i}}{0.003412 \times 0.95}$$
$$AKWH = 155.5^{kWh}/_{showerhead} \times \sqrt{n_i}$$

Retrofit Gross Energy Savings, Fossil Fuel

For Natural Gas:

$$ACCF = \frac{MMBtu_Savings}{0.1029 \frac{MMBtu}{CCF} \times EF_F} = \frac{0.504 \times \sqrt{n_i}}{0.1029 \times 0.62}$$

$$ACCF = 7.90 \times \sqrt{n_i}$$

For Oil:

$$AOG = \frac{MMBtu_Savings}{0.138690^{MMBtu}/_{Gal-oil} \times EF_F} = \frac{0.504 \times \sqrt{n_i}}{0.138690 \times 0.62}$$
$$AOG = 5.86 \times \sqrt{n_i}$$

For Propane:

$$APG = \frac{MMBtu_Savings}{0.09133^{MMBtu}/_{Gal-oil} \times EF_F} = \frac{0.504 \times \sqrt{n_i}}{0.09133 \times 0.62}$$
$$APG = 8.90 \times \sqrt{n_i}$$

Retrofit Gross Energy Savings, Example

Example 1: Two showerheads are replaced in bathrooms of a home which uses electric hot water heating. What are the savings per household per year?

Annual electric savings:

$$AKWH = 155.5 \frac{kWh}{showerhead} \times \sqrt{n_i} = 155.5 \times \sqrt{2} = 220 \frac{kWh}{vr}$$

Annual water savings:

$$AWG = 1{,}212.3^{\textit{Gal}}/_{\textit{showerhead-yr}} \times \sqrt{n}_{i} = 1714^{\textit{Gallons}}/_{\textit{yr}}$$

Example 2: Two showerheads are replaced in bathrooms of a home which uses gas hot water heating. What are the savings per household per year?

Annual electric savings:

$$ACCF = 7.90$$
 ^{CCF}/_{showerhead} $\times \sqrt{n_i} = 7.90 \times \sqrt{2} = 11.2$ ^{CCF}/_{yr}

Annual water savings:

$$AWG = 1,212.3 \frac{Gal}{showerhead-yr} \times \sqrt{n}_{i} = 1714 \frac{Gallons}{yr}$$

Retrofit Gross Peak Day Savings, Natural Gas

$$PD_{WH} = ACCF \times PDF_{WH}$$

Non Energy Benefits

Annual water savings in gallons

$$AWG = 1,212.3 \frac{Gal}{showerhead-yr} \times \sqrt{n}_{i}$$

Changes from Last Version

Made corrections to the annual water savings, electric savings and fossil fuel savings

References

- [1] EPA WaterSense® Specification for Showerheads, Version 1.0, effective February 9, 2010. Accessed on July 21, 2010.
- [2] KEMA. Evaluation of the Weatherization Residential Assistance Partnership (WRAP) and Helps Programs, Final Report, September 10, 2010.
- [3] Federal Register Part III, DOE Energy Conservation Program: Energy Conservation Standards for Residential Water Heaters, Direct Heating Equipment, Pool Heater; Final Rule, Table I.2. April 16, 2010.
- [4] Aquacraft Water Engineering & Management. California Single Family Water Use Efficiency Study. June 1, 2011.

Notes

[1] Ref [4] (Table 35, page 128) showed water usage for northern sites versus southern sites to have the ratio 171/183 = 0.9344.

[2] Ref [2] recommends this method of reducing savings for additional water fixtures by multiplying by the square root of the number installed.

Version Date: 10/30/2012 4.5.4 FAUCET AERATOR

4.5.4 FAUCET AERATOR

Description of Measure

Installation of aerators meeting the EPA WaterSense specification (Ref [1]) to replace Federal Standard (2.2 gpm) or higher flow lavatory faucet aerators.

Savings Methodology

Savings shall be claimed based on the type of fuel used for water heating. Water savings is based on the difference between the Federal Standard (2.2 gpm) versus WaterSense (1.5 gpm).

The savings presented here are not applicable for installations where the flow rate does not reduce the total hot water used (i.e. kitchen sinks, laundry rooms, or tubs).

Note: No demand savings are claimed for this measure since there is insufficient peak coincident data.

Inputs

| Symbol | Description |
|--------------------------|---|
| WH Fuel | Water Heater Fuel Type |
| $n_{\rm i}$ | Number of low flow faucet aerators installed |
| gpm _{installed} | Flow rate of installed faucet, (not required for savings) |

| Symbol | Description | Units | Values | Comments |
|---------------------|--|---------|------------------|---------------|
| AKWH | Annual Electric savings for homes with Electric HW | kWh/yr | Calculated | |
| ACCF | Annual Gas Savings | Ccf/yr | Calculated | |
| AOG | Annual Oil Savings | Gal/yr | Calculated | |
| APG | Annual Propane Savings | Gal/yr | Calculated | |
| d _e | Average duration per event | minutes | 0.6167 | Ref [4] |
| d_{W} | Density of water | lb/ Gal | 8.31 | |
| EF_E | Energy Factor of Electric Water Heater | | 0.95 | Ref [3] |
| EF_F | Energy Factor of Fossil Fuel Water Heater | | 0.62 | Ref [3] |
| gpm | Gallons per minute flow rate | gal/min | Fed Std: 2.2 | Ref [1] |
| | | | Water Sense: 1.5 | |
| n_a | Estimated average total number faucets (all types) per | | 5.1 | Note [3], Ref |
| | household | | | [4] |
| n _e | Median number of faucet events per day per household | | 42.9 | Ref [4] |
| n_i | number of aerators installed | | As found | |
| r_g | Ratio to adjust usage for cooler climate | | 0.9344 | Note [1], Ref |
| ŭ | | | | [4] |
| S_{W} | Annual Water Savings per faucet | gal/yr | Calculated | |
| T _{faucet} | Temperature of water from faucet | °F | 80 °F | |
| T _{supply} | Temperature of water into house | °F | 55 °F | |
| PDF_{WH} | Peak Day Factor, Water Heating | | 0.00321 | Appendix 1 |
| PD_{WH} | Peak Day savings, Water Heating | | | |

Version Date: 10/30/2012 4.5.4 FAUCET AERATOR

Retrofit Gross Energy Savings, Electric

$$\begin{split} S_W &= n_e \times d_e \times 365^{\,days}/_{yr} \times r_g \times \left(gpm_{federal\ std} - gpm_{WaterSense}\right)/n_a \\ S_W &= 42.9 \times 0.6167 \times 365^{\,days}/_{yr} \times 0.9344 \times \left(2.2\ gpm - 1.5\ gpm\right)/5.1 \\ S_W &= 1,238^{\,Gal}/_{faucet \bullet \ yr} \end{split}$$

$$MMBtu\ Savings = \sqrt{n} \times \left(T_{Faucet} - T_{Supply}\right) \times d_W \times SH_W \times S_W / 10^6\ {}_{Btu}/_{MMBtu}\ (\textbf{See Note [2]})$$

$$MMBtu\ Savings = \sqrt{n} \times \left(80^\circ F - 55^\circ F\right) \times 8.31\ {}_{Gal}^{lb}/_{Gal} \times 1,238\ {}_{faucet\bullet\ yr}/10^6\ {}_{Btu}/_{MMBtu}$$

$$MMBtu\ Savings = 0.257\ {}_{MMBtu}/_{faucet} \times \sqrt{n}$$

$$AKWH = \frac{MMBtu\ Savings}{.003412\ ^{MMBtu}/_{kWh} \times EF_E} = \frac{0.257 \times \sqrt{n}}{0.003412 \times 0.95}$$

$$AKWH = 79.3\ ^{kWh}/_{faucet} \times \sqrt{n}$$

Retrofit Gross Energy Savings, Fossil Fuel

Natural Gas:

$$ACCF = \frac{MMBtu\ Savings}{.102900\ ^{MMBtu}/_{Ccf} \times EF_F} = \frac{0.257 \times \sqrt{n}}{0.102900 \times 0.62}$$

$$ACCF = 4.03 \times \sqrt{n}$$

Oil:

$$AOG = \frac{MMBtu \ Savings}{.138690 \ ^{MMBtu}/_{Gal \ oil} \times EF_F} = \frac{0.257 \times \sqrt{n}}{0.138690 \times 0.62}$$
$$AOG = 2.99 \times \sqrt{n}$$

Propane:

$$APG = \frac{MMBtu\ Savings}{0.09133\ ^{MMBtu}/_{Gal\ propane} \times EF_F} = \frac{0.257 \times \sqrt{n}}{0.09133 \times 0.62}$$

$$APG = 4.54 \times \sqrt{n}$$

Retrofit Gross Energy Savings, Example

Example 1. Two aerators are replaced in bathrooms of home which uses electric hot water heating. What are the total savings?

$$AKWH = 79.3 \, \text{kWh/}_{faucet} \times \sqrt{2} = 112 \, \text{kWh/}_{yr}$$

$$Annual \ Gal \ Water \ Savings = S_W \times \sqrt{n} = 1{,}238 \, \text{Gal/}_{yr} \times \sqrt{2} = 1751 \, \text{Gal/}_{yr}$$

Version Date: 10/30/2012 4.5.4 FAUCET AERATOR

Example 2. Two aerators are replaced in bathrooms of a home which uses gas hot water heating. What are the savings?

Annual Gas Ccf =
$$4.03 \times \sqrt{2} = 5.7 \frac{\text{Ccf}}{\text{yr}}$$

Annual Gal Water Savings = $S_W \times \sqrt{n} = 1{,}238 \frac{\text{Gal}}{\text{yr}} \times \sqrt{2} = 1751 \frac{\text{Gal}}{\text{yr}}$

Retrofit Gross Peak Day Savings, Natural Gas

$$PD_{WH} = ACCF \times PDF_{WH}$$

Non Energy Benefits

Annual Gal Water Savings =
$$S_W \times \sqrt{n} = 1{,}238 \frac{Gal}{yr} \times \sqrt{n}$$

References

- [1] U.S. EPA WaterSense High-Efficiency Lavatory Faucet Specification, Effective October 1, 2007, Accessed July 21, 2010.
- [2] KEMA. Evaluation of the Weatherization Residential Assistance Partnership (WRAP) and Helps Programs, Final Report, September 10, 2010.
- [3] Federal Register Part III, DOE Energy Conservation Program: Energy Conservation Standards for Residential Water Heaters, Direct Heating Equipment, Pool Heater; Final Rule, Table I.2. April 16, 2010.
- [4] Aquacraft Water Engineering & Management. California Single Family Water Use Efficiency Study. June 1, 2011.

Notes

- [1] Ref [4] (Table 35, page 128) showed water usage for northern sites versus southern sites to have the ratio 171/183 = 0.9344.
- [2] Ref [2] recommends this method of reducing savings for additional aerators by multiplying by the square root of the number installed.
- [3] Ref [4] gave the number of toilets per household, 2.4 (Table 66, pages 185-186). Assuming the number of toilets = number of primary lavatory sinks, add one primary faucet for the kitchen, add 1.3+0.4 for number of tub faucets per household, total faucets = 2.4+1+1.7=5.1. Including the tubs/HH in the calculation may understate the lavatory faucet savings since tub use is about 1/10 of the average sink faucet use per year.

4.5.7 FOSSIL FUEL WATER HEATER

Description of Measure

Version Date: 10/30/2012

Installation of a high efficiency standalone natural gas or propane tankless and storage water heaters.

Savings Methodology

Energy and demand savings calculations for a tankless or storage water heater are shown below. Savings for high efficiency indirect water heater and integrated water heater attached to an ENERGY STAR rated boiler are shown as lost opportunity water heating portion of the high efficiency boiler (Measure 4.2.17). Many of the inputs for this measure are based on the Tool for Generating Realistic Residential Hot Water Event Schedules (Ref [1]). The tool estimates hourly hot water consumption in gallons based on location of home and number of bedrooms. The tool used results from a number of metering studies to develop usage profiles based on location of home and number of bedrooms. These profiles along with incoming water temperature for Connecticut were used to calculate the water heating load for a typical Connecticut home. Assumed water heater efficiencies (energy factors) were used to calculate natural gas and propane savings from the gross energy savings.

Inputs

| Symbol | Description | Units |
|----------|-------------------------|-------|
| | Water heating fuel. | |
| EF_{I} | Energy Factor-installed | % |

Nomenclature

| Symbol | Description | Units | Values | Comments |
|--------------|--|-------|------------|------------------|
| $ABTU_W$ | Annual BTU savings – water heating | Btu | | |
| $ACCF_W$ | Annual Natural gas savings – water heating | Ccf | | |
| ADHW | Annual domestic hot water load | Btu | 11,197,132 | Note [1] |
| APG_W | Annual Propane savings – water heating | Gal | | |
| EF_B | Energy Factor - Baseline | | 0.62 | Note [2] and [3] |
| EF_{I} | Energy Factor - Installed | | | Note [3] |
| GPY | Annual domestic hot water usage in Gallons | Gal | 19,839 | Note [1] |
| PD_{W} | Peak Day water heating savings | Ccf | | |
| PDF_{W} | Peak Day factor water heating | | 0.00321 | |
| T_{aiw} | Average annual incoming water temperature | °F | 57 | Note [1] |
| $T_{ m dhw}$ | Domestic hot water heater set point | °F | 125 | Note [1] |

Lost Opportunity Gross Energy Savings, Fossil Fuel

$$ADHW = GPY \times 8.3 \frac{lbs}{Gal} \times (T_{dhw} - T_{aiw})$$

 $ADHW = 19,839 \frac{Gal}{yr} \times 8.3 \frac{lbs}{Gal} \times (125^{\circ}F - 57^{\circ}F)$
 $ADHW = 11,197,132 Btu$

Version Date : 10/30/2012

$$ABTU_{W} = ADHW \times \left(\frac{1}{EF_{B}} - \frac{1}{EF_{I}}\right)$$

$$ABTU_{W} = 11,197,132 Btu \times \left(\frac{1}{0.62} - \frac{1}{EF_{I}}\right)$$

Savings by water heating fuel:

$$ACCF_{W} = \frac{ABTU_{W}}{102,900^{Btu}/_{Cef}}$$

$$APG_W = \frac{ABTU_W}{91,330^{Btu}/_{Gal}}$$

Lost Opportunity Gross Energy Savings, Example

A natural gas water heater with an EF = 82% (0.82) is installed. What are the annual natural gas savings?

$$ABTU_{W} = 11,197,132 \ Btu \times \left(\frac{1}{0.62} - \frac{1}{0.82}\right) = 4,404,851 \ Btu$$

$$ACCF_{W} = \frac{4,404,851 \ Btu}{102,900 \ {}^{Btu}/_{Ccf}} = 42.8 \ Ccf$$

Lost Opportunity Gross Peak Day Savings, Natural Gas

$$PD_{W} = ACCF_{W} \times PDF_{W}$$

$$PD_{W} = ACCF_{W} \times 0.00321$$

Changes from Last Version

Measure now accounts for standalone storage water heaters.

References

[1] Tool for Generating Realistic Residential Hot Water Event Schedules, Preprint, NREL, August 2010.

Notes

- [1] These values were developed using the Tool in Ref [1] for Hartford area weather data and a three bedroom house.
- [2] Federal Register Part III, April 16, 2010, DOE Energy Conservation Program: Energy Conservation standards for Residential Water Heaters, Direct Heating Equipment, Pool Heater; Final Rule.
- [3] The energy factor (EF) is defined as the overall energy efficiency of a water heater based on the amount of hot water produced per unit of fuel consumed over a typical day. This includes recovery efficiency, standby losses and cycling losses (Source: www.energysavers.gov).

4.5.8 HEAT PUMP WATER HEATER

Description of Measure

Version Date: 10/30/2012

Installation of a heat pump water heater in place of an electric resistance water heater

Savings Methodology

The (deemed) savings for this measure are calculated based on the water heating load as calculated and the difference of efficiency between a baseline electric resistance water heater and a heat pump water heater. Because the efficiency of a heat pump water heater is affected by air temperature and the ENERGY STAR is RATED for an average air temperature higher than what is expected in Connecticut, the analysis adjusted the minimum ENERGY STAR qualifying COP based on the estimated basement temperature for a home in Connecticut (average day, summer day, and winter day). Effective efficiency is also affected by the recovery and location adjustments. That adjustment is described below as a space heating penalty and recovery adjustment. The peak demand savings are estimated based on the "Tool for Generating Realistic Residential Hot Water Event Schedules" (Ref [1]). The tool estimates hourly hot water usage in gallons based on location of home and number of bedrooms. The tool used results from a number of metering studies and developed usage profiles based on location of home and number of bedrooms. These profiles along with incoming water temperature for Connecticut were used to calculate the water heating load for a typical Connecticut home. Water heater Energy factors were used to calculate energy usage.

Inputs

| Symbol | Description | Units |
|--------|---------------------------|-------|
| | Number of units installed | |

| Symbol | Description | Units | Values | Comments |
|--------------------|--|---------|-------------|----------|
| AEDHW _b | Annual electric domestic hot water load baseline (for electric resistance | kWh | 3,646kWh | |
| | water heater) | | | |
| AEDHW _i | Annual electric domestic hot water load installed (for heat pump water | kWh | 1,971kWh | |
| | heater) | | | |
| ADHW | Annual domestic hot water load | Btu/ yr | 11,197, 132 | Note[1] |
| $AKWH_W$ | Annual electric energy savings (difference between AEDHW _b baseline | kWh/yr | 1,675kWh | |
| | and AEDHW _i installed) | | | |
| COP ₅₅ | COP at the estimated average basement temperature of 55 °F - winter | | 1.75 | Note [2] |
| COP ₆₀ | COP at the estimated average basement temperature of 60 °F – annual | | 1.85 | Note [2] |
| | average | | | |
| COP ₆₅ | COP at the estimated average basement temperature of 65 °F -summer | | 1.95 | Note [2] |
| EF _b | Energy Factor - baseline | % | 90 | Ref [3] |
| GPH | Average gallons per hour during peak time | gph | 1.96 | Note [1] |
| GPY | Annual domestic hot water usage in Gallons | Gal | 19,839 | Note [1] |
| P | Heating penalty and recovery adjustment | % | 90 | Assumed |
| PDHW _s | Peak hour hot water load - summer | Btu | | |
| $PDHW_{w}$ | Peak hour hot water load - winter | Btu | | |
| SKW | Summer electric demand savings | kW | | |
| T_{aiw} | Average annual incoming water temperature | °F | 57 | Note [1] |
| T_{dhw} | Domestic hot water heater set point | °F | 125 | Assumed |

Version Date: 10/30/2012

| T_{siw} | Average Summer incoming water temperature | °F | 65 | Note [1] |
|--------------|---|----|----|----------|
| $T_{ m wiw}$ | Average Winter incoming water temperature | °F | 46 | Note [1] |
| WKW | Winter electric demand savings | kW | | |

Retrofit Gross Energy Savings, Electric

$$ADHW = GPY \times 8.3 \frac{lbs}{Gal} \times (T_{dhw} - T_{aiw})$$

 $ADHW = 19,839 \frac{Gal}{yr} \times 8.3 \frac{lbs}{Gal} \times (125°F - 57°F)$
 $ADHW = 11.197.132 Btu$

$$AEDHW_b = ADHW \times \frac{1}{3,412 \frac{Btu}{kWh}} \times \frac{1}{EF_b}$$

$$AEDHW_b = 11,197,132 \frac{1}{Btu} \times \frac{1}{3,412 \frac{Btu}{kWh}} \times \frac{1}{0.9} = 3,646 \frac{kWh}{100}$$

$$AEDHW_{i} = ADHW \times \frac{1}{3,412^{Btu}/_{kWh}} \times \left[\frac{1}{COP_{60} \times P} \right]$$

$$AEDHW_{i} = 11,197,132Btu \times \frac{1}{3,412^{Btu}/_{kWh}} \times \left[\frac{1}{1.85 \times 0.9} \right] = 1,971 \, kWh$$

$$AKWH_{W} = AEDHW_{b} - AEDHW_{i} = 3,646 - 1,971 = 1,675 \text{ kWh}$$

Retrofit Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

$$PDHW_s = GPH \times 8.3^{lbs}/_{Gal} \times (T_{dhw} - T_{siw})$$

$$PDHW_s = 1.96 \frac{Gal}{hr} \times 8.3 \frac{lbs}{Gal} \times (125^{\circ}F - 65^{\circ}F) = 976 Btu$$

$$SKW_s = PDHW_s \times \frac{1}{3,412^{Btu}/_{kWh}} \times \left(\frac{1}{EF_h} - \frac{1}{COP_{65}}\right)$$

$$SKW_s = 976 \ Btu \times \frac{1}{3,412^{Btu}/_{kWh}} \times \left(\frac{1}{0.9} - \frac{1}{1.95}\right) = 0.17 \ kW$$

$$PDH_{w} = GPH \times 8.3^{lbs}/_{Gal} \times (T_{dhw} - T_{wiw})$$

$$PDHW_{w} = 1.96 \frac{Gal}{hr} \times 8.3 \frac{lbs}{Gal} \times (125^{\circ}F - 46^{\circ}F) = 1,285 Btu$$

$$WKW_{w} = PDHW_{w} \times \frac{1}{3,412 \frac{Btu}{kWh}} \times \left(\frac{1}{EF_{b}} - \frac{1}{COP_{55}}\right)$$

$$WKW_{w} = 1,285 Btu \times \frac{1}{3,412 \frac{Btu}{kWh}} \times \left(\frac{1}{0.9} - \frac{1}{1.75}\right) = 0.20 kW$$

Changes from Last Version

Savings calculations moved from Lost Opportunity to Retrofit. Updated nomenclature section to reflect derivation of annual domestic hot water load.

References

- [1] Tool for Generating Realistic Residential Hot Water Event Schedules, Preprint, NREL, August 2010.
- [2] Nyle Heat Pump Water Heater Evaluation, Final Report, AIL Research, Inc. Jan 2002.
- [3] 2004 federal standard (10CFR 430) for 50 gallon tank

Notes

- [1] These values were developed using the Tool in Ref [1] for Hartford area weather data and a three bedroom house.
- [2] The minimum ENERGY STAR COP of 2 rated at 67.5 °F was adjusted using Ref [2] to develop a relationship between COP and air temperature. The annual average basement air temperature was estimated at 60°F, and 65°F average summer and 55°F average winter temperatures.

Version Date: 10/30/2012 4.5.9 PIPE INSULATION

4.5.9 PIPE INSULATION

Description of Measure

Installation of insulation on domestic hot water (DHW) pipes and or heating pipes in unconditioned basements to reduce heat loss

Savings Methodology

Annual savings for DHW pipes estimated based on pipe size in table below. The savings values are per foot of hot pipe coming from the water heater in unconditioned space and are based on the outputs of Ref [1], based on the inputs listed in Note [1], also recommended in Ref [2]

Inputs

| Symbol | Description |
|---------------|--|
| Pipe Diameter | Pipe diameter, inches (savings are shown for ½" and ¾" pipes for domestic hot water, |
| | Savings are shown for 3/4",1",1 1/2" and 2"pipes used for heating) |
| L | Length of pipe insulation, in feet. |
| | Hot water Fuel type (Electric resistive, Gas, Oil, Propane) |
| | Heating Fuel type (Gas, Oil, Propane) |

| Symbol | Description | Units | Values | Comments |
|------------------|---|--------|------------|------------|
| $ACCF_H$ | Annual Gas Savings per linear foot, Heating | Ccf/ft | | Table 4 |
| $ACCF_W$ | Annual Gas Savings per linear foot, domestic hot water | Ccf/ft | | Table 3 |
| AKW_H | Annual kWh Energy Savings coefficient, heating | kWh/ft | | Table 2 |
| AKW_W | Annual kWh Energy Savings coefficient, domestic hot water | kWh/ft | | Table 1 |
| $AKWH_H$ | Annual Energy Savings, heating | kWh | Calculated | |
| $AKWH_W$ | Annual Energy Savings, domestic hot water | kWh | Calculated | |
| AOG_H | Annual Oil Savings, Heating | Gal/ft | | Table 4 |
| AOG_W | Annual Oil Savings, domestic hot water | Gal/ft | | Table 3 |
| APG_H | Annual Propane Savings, Heating | Gal/ft | | Table 4 |
| APG_W | Annual Propane Savings, domestic hot water | Gal/ft | | Table 3 |
| PD_{W} | Peak Day savings, domestic hot water | | | |
| PDF_{H} | Peak Day Factor, Heating | | 0.00977 | Appendix 1 |
| PDF_{W} | Peak Day Factor, domestic hot water | | 0.00321 | Appendix 1 |
| PF_S | Summer Seasonal Peak Factor | W/kWh | 0.1147 | Ref [3] |
| PF_{W} | Winter Seasonal Peak Factor | W/kWh | 0.1747 | Ref [3] |
| SKW _H | Summer Seasonal Peak Demand Savings heating | kW | | |
| SKW _W | Summer Seasonal Peak Demand Savings domestic hot water | kW | | |
| WKW _H | Winter Seasonal Peak Demand Savings heating | kW | | |
| WKWw | Winter Seasonal Peak Demand Savings domestic hot water | kW | | |

Version Date: 10/30/2012 4.5.9 PIPE INSULATION

Retrofit Gross Energy Savings, Electric

Table 1: Annual Electrical Savings per Linear Foot of Domestic Hot Water Pipe Insulation

| Pipe Diameter (inches) | AKW _W (kWh/ft) |
|------------------------|---------------------------|
| 0.50 | 10.4 |
| 0.75 | 15.9 |

Annual Electric Domestic hot water savings can be calculated using the formula below, and using the values for AKW_W from Table 1.

$$AKWH_W = AKW_W \times L$$

Table 2: Annual Electrical Savings per Linear Foot of Heating Pipe Insulation

| Pipe Diameter (inches) | AKW _H (kWh/ft) |
|------------------------|---------------------------|
| 0.75 | 12.9 |
| 1.00 | 16.0 |
| 1.25 | 19.6 |
| 1.50 | 22.2 |

Annual Electric heating savings can be calculated using the formula below, and using the value for AKW_H from Table 2.

$$AKWH_H = AKW_H \times L$$

Retrofit Gross Energy Savings, Fossil Fuel

Table 3: Annual Fossil Fuel Savings per Linear Foot of domestic hot water Pipe Insulation

| Pipe Diameter (inches) | ACCF _W (Ccf/ft) | AOG _W (Gallons/ft) | APG _W (Gallons/ft) |
|------------------------|----------------------------|-------------------------------|-------------------------------|
| 0.50 | 0.55 | 0.46 | 0.60 |
| 0.75 | 0.85 | 0.70 | 0.92 |

Annual Gas Domestic hot water savings can be calculated using the formula below and using the $ACCF_w$ coefficient in Table 3.

$$ACCF = ACCF_w \times L$$

Annual Oil Domestic hot water savings can be calculated using the formula below and using the AOG_w coefficient in Table 3.

$$AOG = AOG_{W} \times L$$

Annual Propane Domestic hot water savings can be calculated using the formula below and using the APG_w coefficient in Table 3.

$$APG = APG_w \times L$$

| Table 4. Annual Essel E. | ral Carringa non I | maan East of Heatin | a Dina Insulation |
|---------------------------|--------------------|---------------------|-------------------|
| Table 4: Annual Fossil Fu | iei Savings der Li | near root of Heaun | g Pide Insulation |

| Pipe Dia (inches) | ACCF _H (Ccf/ft) | AOG _H (Gallons/ft) | APG _H (Gallons/ft) |
|-------------------|----------------------------|-------------------------------|-------------------------------|
| 0.75 | 0.5 | 0.4 | 0.6 |
| 1.00 | 0.6 | 0.5 | 0.7 |
| 1.25 | 0.8 | 0.6 | 0.9 |
| 1.50 | 0.9 | 0.7 | 1.0 |

Annual Gas heating savings can be calculated using the formula below and using the ACCF_H coefficient in Table 4:

$$ACCF = ACCF_H \times L$$

Annual Oil Heating savings can be calculated using the formula below and using the AOG_H coefficient in Table 4:

$$AOG = AOG_H \times L$$

Annual Propane Domestic hot water savings can be calculated using the formula below and using the APG_H coefficient in Table 4:

$$APG = APG_H \times L$$

Retrofit Gross Energy Savings, Example

Five feet of pipe insulation are installed on a ½" diameter hot water pipe. The home has oil hot water heating. What are the annual energy savings?

$$AOG = AOG_H \times L$$

 $AOG = 0.46^{Gal}/_{ft} \times 5 \text{ ft} = 2.3^{Gal}/_{vear}$

Retrofit Gross Seasonal Peak Demand Savings, Electric (Winter and Summer)

For domestic Hot water the summer seasonal peak demand savings is:

$$SKW_W = \left(\frac{AKWH \times PF_S}{1000}\right)$$

For domestic Hot water the winter seasonal peak demand savings is:

$$WKW_W = \left(\frac{AKWH \times PF_S}{1000}\right)$$

For Heating summer seasonal peak demand"

$$SKW_H = 0$$

$$WKW_H = \left(\frac{AKWH \times 0.57}{1000}\right)$$

Retrofit Gross Peak Day Savings, Natural Gas

For Domestic Hot Water:

$$PD_{w} = ACCF \times PDF_{w}$$

Version Date: 10/30/2012 4.5.9 PIPE INSULATION

For Heating:

$$PD_H = ACCF \times PDF_H$$

Retrofit Gross Peak Demand Savings, Example

5 feet of pipe insulation are installed on a ½" diameter hot water pipe. The home has electric hot water heating. What are the summer and winter peak demand savings?

$$AKWH = 5 \ feet \times 10.4^{kWh}/_{fi \bullet yr} = 52^{kWh}/_{yr}$$

$$SKW = \frac{\left(52 \ kWh \times 0.1147 \ W/_{kWh}\right)}{1000 \ W/_{kW}} = 0.0060 \ kW$$

$$WKW = \frac{\left(52 \ kWh \times 0.1747 \ W/_{kWh}\right)}{1000 \ W/_{kW}} = 0.0091 \ kW$$

Changes from Last Version

Added Savings for heating pipes as Tables 2 & 4.

References

- [1] NAIMA, 3E Plus software tool, Version 4.0, Released 2005.
- [2] Nexant. Home Energy Solutions Evaluation: Final Report, submitted to Connecticut Energy Efficiency Board. March 2011.
- [3] KEMA. Evaluation of the Weatherization Residential Assistance Partnership (WRAP) and Helps Programs, Final Report, September 10, 2010.

Notes

- [1] 3E Plus Inputs for Domestic hot water:
 - 1. Polyolefin (Polyethylene) Foam Tube insulation, 3/8" Thk for 1/2" pipe, 1/2" Thk for 3/4" pipe.
 - 2. No Jacket installed, so assume emittance (emissivity) of "jacket" is 1.0 (maximum)
 - 3. Ambient Temp range 40-70 deg F, no wind speed (used 60 typical)
 - 4. Process Temp (water heater temp) 90 deg F to reflect average temperatures (normal range of WH setting is 120-140; 120 for energy savings, 140 carries risk of scalding)
 - 5. Tubing is copper
 - 6. Savings counted 8760 hours/yr since average temperature is used.
 - 7. Heat in pipes will dissipate during the time hot water is not being used, thus reducing the average water temperature in the pipe.
 - 8. Only 0.5 and 0.75 inch pipe necessary, since most HW supply pipes are either 1/2 or 3/4 in
 - 9. 3E Plus software (from NAIMA) used to calculate heat loss
 - 10. Temp difference between ambient temperatures and pipe temperatures: 30 correlates with 90 F pipe and 60 F ambient
 - 11. Efficiency of water heaters same as that used for faucet aerators and showerheads, see 13.
 - 12. Horizontal pipes
 - 13. WH efficiencies: Electric 90%, Oil 49.5%, Gas and propane: 57.5%

4.6.1 RESIDENTIAL CUSTOM

Description of Measure

Version Date: 10/30/2012

This measure may apply to any project whose scope may be considered custom or comprehensive. Applicable measures may include the replacement of an inefficient HVAC system (or component) such as a fossil fuel furnace, boiler, heat pump, air conditioner, Home Performance with ENERGY STAR project measures, or any other project where interactive effects between two or more measures are present.

4.6 OTHER

Savings Methodology

These custom measures can be evaluated using either the appropriate measure, if found in this document, or other acceptable modeling tools such as DOE-2, Elite, PRISM, REM/Rate, or engineering spreadsheets (Notes [1], [2] & [3]). Custom measures should use site-specific information when available (i.e. existing conditions, etc.). The analysis of the site-specific measures will be reviewed for reasonableness by a qualified internal program administrator or independent third party engineer. Whenever possible, site utility billing history must be utilized as appropriate. When a measure meets the requirements for early retirement (existing equipment is in good working order), use the partial savings methodology outline for that measure (or similar measure) outlined in this document. For an early retirement measure the savings may need to be calculated in two parts, as follows:

- 1. Retrofit savings based on the early retirement of a working existing unit, and
- 2. Lost Opportunity savings for installing a new efficient unit for the life of the measure

In case where interactive effects between two or more measures are present, a comprehensive analysis must be conducted and fully documented, with assumptions and methodology clearly indicated.

Changes from Last Version

Formerly measure 4.2.16 (Residential Custom). Measure updated to apply to custom residential measures in general, not just HVAC custom.

Notes

- [1] REM/RateTM is a residential energy analysis, code compliance and rating software developed by Architectural Energy Corporation. This software calculates heating, cooling, hot water, lighting, and appliance energy loads, consumption and costs for new and existing single and multi-family homes.
- [2] PRISM is an established statistical procedure for measuring energy conservation in residential housing. The PRISM software package was developed by the Center for Energy and Environmental Studies, Princeton University. The tool is used for estimating energy savings from billing data. http://www.princeton.edu/~marean/>
- [3] DOE-2 is a widely used and accepted building energy analysis program that can predict the energy use and cost for all types of buildings. DOE-2 uses a description of the building layout, constructions, operating schedules, conditioning systems (such as lighting & HVAC) and utility rates provided by the user, along with weather data, to perform an hourly simulation of the building and to estimate utility bills. http://www.doe2.com/>

Version Date: 10/30/2012 4.6.2 BEHAVIORAL CHANGE

4.6.2 BEHAVIORAL CHANGE

Description of Measure

This measure covers enrollment in a residential behavioral program, including periodic normative reports on energy consumption designed to encourage lower usage.

Savings Methodology

Because the characteristics of behavioral programs make them amenable to robust, unbiased evaluation through randomized, controlled trials, and because Connecticut is expected to regularly evaluate its behavioral energy efficiency programs, use of evaluated savings estimates is recommended.

Evaluations should be conducted and savings calculated in accordance with the Department of Energy's SEE Action Recommendations, including but not limited to the use of a randomized controlled trial and a panel data model¹.

Savings are estimated by the difference between usage with the behavioral program and usage without the behavioral program. Usage without the behavioral program can be estimated by dividing adjusting actual usage by an adjustment factor based on the treatment effect to back out the effect of the program.

Inputs

| Symbol | Description | Comments |
|--------|------------------------------------|----------|
| Usage | Annual Electric Energy Consumption | |

Nomenclature

| Symbol | Description | Units | Comments |
|--------|------------------------------------|-------|----------|
| AKWH | Annual Electric Energy Savings | kWh | |
| ATE | Average Treatment Effect | | Input |
| Usage | Annual Electric Energy Consumption | kWh | Input |

Changes from Last Version

New measure

References

[1] Department of Energy, SEE Action, "Evaluation, Measurement, and Verification (EM&V) of Residential Behavior-Based Energy Efficiency Programs: Issues and Recommendations". May 2012. Page xi.

APPENDIX 1. PEAK FACTORS

Coincidence Factors for ISO-NE Seasonal Peak Demand Reductions

| Commercial and Industrial Lighting and Occupancy Sensors | | | | | | | | |
|--|------------------------|------------------------|------------------------|------------------------|--|--|--|--|
| | Lighting | | Occupancy Sensors | | | | | |
| Facility Type | Summer | Winter | Summer | Winter | | | | |
| Grocery | 90.4% _(d,3) | 77.0% _(d,4) | | | | | | |
| Manufacturing | 67.1% _(d,3) | 43.2% _(d,4) | 19.8% _(d,5) | 17.2% _(d,6) | | | | |
| Medical (Hospital) | 74.0% _(d,3) | 61.8% _(d,4) | 23.9% _(d,5) | 22.1% _(d,6) | | | | |
| Office | $70.2\%_{(d,3)}$ | 53.9% _(d,4) | 27.4% _(d,5) | 29.6% _(d,6) | | | | |
| Other | 47.6% _(d,3) | 42.8% _(d,4) | 2.4% _(d,5) | 6.6% _(d,6) | | | | |
| Restaurant | 77.5% _(d,3) | 64.4% _(d,4) | | | | | | |
| Retail | 79.5% _(d,3) | 64.7% _(d,4) | | | | | | |
| University / College | 65.0% _(d,3) | 52.8% _(d,4) | 28.3% _(d,5) | 23.1% _(d,6) | | | | |
| Warehouse | 72.7% _(d,3) | 53.5% _(d,4) | 24.6% _(d,5) | 18.3% _(d,6) | | | | |
| School | 59.9% _(d,3) | 38.8% _(d,4) | 20.9% _(d,5) | 15.9% _(d,6) | | | | |

| Other Commercial and Industrial Measures | | | | | | | |
|--|----------------------|----------------------|--|--|--|--|--|
| Measure | Summer | Winter | | | | | |
| Unitary A/C | 82.0% _(c) | $0.0\%_{(c)}$ | | | | | |
| Efficient Motors (cooling) | 73.0% _(c) | 60.0% _(c) | | | | | |
| Efficient Motors (heating) | $0.0\%_{(c)}$ | 80.0% _(c) | | | | | |
| Refrigeration Controls | $10.0\%_{(f)}$ | $10.0\%_{(f)}$ | | | | | |

| Residential | | |
|------------------------|-----------------------|------------------------|
| Measure | Summer | Winter |
| Lighting | 8.8% _(d,1) | 26.4% _(d,2) |
| Central A/C | 59.0% _(b) | $0.0\%_{(b)}$ |
| Window A/C | 30.3% _(e) | $0.0\%_{(e)}$ |
| Heating | $0.0\%_{ m (f)}$ | $50.0\%_{(f)}$ |
| Refrigeration | $30.0\%_{(f)}$ | 21.0% _(f) |
| Water Heating Measures | $10.0\%_{(f)}$ | 15.0% _(f) |

Calculating Peak Day savings for gas measures

Natural gas peak day usage is driven by the heating load; thus peak day savings is the savings associated with conservation measures that takes place during the coldest continuous 24 hour period of the year.

The methodology for peak day savings estimating for natural gas efficiency measures is summarized below:

1) **Residential space heating efficiency upgrades**: Since energy savings correlate directly to outside air temperatures, the demand savings for residential space heating measures is estimated based on as a percentage (0.977%) of annual savings The 0.977% factor is based on Bradley Airport peak degree day average (58.5) of the last thirty years divided by the average heating degree days (5,990) for the last thirty years. (note 1)

Peak Day Savings (residential heating) = 0.00977 × Annual Heating Savings

2) **Residential gas water heating:** The peak day savings are estimated by estimating the percent of hot water consumption during the peak day. This is done by multiplying the annual savings associate with a hot water measure by 0.321%. This factor is based on water heating load and inlet temperatures from the NREL tool in

Reference [1]. Hartford the coldest inlet water temperature was 45.96 degrees and average is 56.72 degrees.

Peak Factor =
$$\frac{(1 \text{ day}) \times (120 \text{ °}F - 45.96 \text{ °}F)}{(365 \text{ days}) \times (120 \text{ °}F - 56.72 \text{ °}F)} = 0.00321$$

Assumed hot water set point is 120 degrees. Therefore,

Peak Day Savings (residential water) = 0.00321× Annual Water Heating Savings

3) **Measures with savings daily constant saving:** An example would be a process heating measure. For these measures the peak day savings will be estimated by dividing the annual savings by 365 days per year.

$$Peak \ Day \ Savings = \frac{Annual \ Savings}{365 \ days \ per \ year}$$

4) **Custom measures:** Measures that are not weather dependent, nor have consistent savings from day to day or are analyzed with a more detailed analysis tool such as the hourly DOE-2 program will be analyzed on a case by case basis. For example a complex boiler replacement or controls measure might be modeled using DOE-2. In this case hourly building simulation can calculate the savings for the peak day based on (TMY) data used in the program. These measures are typically analyzed by a third party consultant and reviewed for reasonableness.

References

- [1] Tool for Generating Realistic Residential Hot Water Event Schedules, Preprint, NREL, August 2010.
- [b] Residential Central AC Regional Evaluation: Final Report, Prepared by ADM Associates, Inc., November 2009, Table 4-17, CT weighted average. Winter seasonal peak CF is assumed to be zero.
- [c] 2005 Coincident Factor Study for UI & CL&P by RLW, January 2007, Table 5.
- [d] Coincidence Factor Study Residential and Commercial Industrial Lighting Measures by RLW, Spring 2007. [d,1] Page IV, Table i-5.
- [d,2] Page V, Table i-6.
- [d,3] Page VIII, Table i-11.

- [d,4] Page IX, Table i-12.
- [d,5] Page XII, Table i-17.
- [d,6] Page XII, Table i-18.
- [e] Coincidence Factor Study, Residential Room Air Conditioners, Prepared by RLW, December 2007, Table 22, Hartford, CT seasonal CF. Winter seasonal peak CF is assumed to be zero.
- [f] Estimated.

APPENDIX 2. LOAD SHAPES

Load Shapes by End Use and Sector.

| | Winter | Winter | Summer | Summer |
|---------------|------------|-------------|--------|----------|
| | Peak | Off-Peak | Peak | Off-Peak |
| | Energy | Energy | Energy | Energy |
| Load Shape | % | % | % | % |
| End Use | Residentia | al | | |
| Cooling | 5.0% | 5.0% | 65.0% | 25.0% |
| Heating | 55.0% | 30.0% | 5.0% | 10.0% |
| Lighting | 30.0% | 40.0% | 10.0% | 20.0% |
| Refrigeration | 30.0% | 30.0% | 20.0% | 20.0% |
| Water Heating | 30.0% | 30.0% | 20.0% | 20.0% |
| | Commerc | ial & Indus | trial | |
| Cooling | 3.0% | 2.0% | 80.0% | 15.0% |
| Heating | 60.0% | 35.0% | 5.0% | 0.0% |
| Lighting | 50.0% | 10.0% | 30.0% | 10.0% |
| Refrigeration | 30.0% | 30.0% | 20.0% | 20.0% |
| Other | 50.0% | 10.0% | 30.0% | 10.0% |
| Motors | 50.0% | 10.0% | 30.0% | 10.0% |
| Process | 50.0% | 10.0% | 30.0% | 10.0% |

Winter is defined as October – May Summer is defined as June – September Peak is defined as 7:00 AM – 11:00 PM weekdays (no holidays) Off-peak is defined 11:00 PM to 7:00 AM, plus all weekend and holiday hours.

Changes from Last Version

Identified source references.

APPENDIX 3. REALIZATION RATES

CL&P & UI Commercial & Industrial Realization Rates

| | Gross Real | ization % | | FR & | & SO | Net R | ealization % | (Note 3) | | | |
|---------------|----------------------------|-------------------------------|-------------------------------|----------------------|----------------------|--------|-------------------------------|-------------------------------|--|--|--|
| | | | | | | | | | | | |
| | | | | | | | | | | | |
| End-use | kWh | Winter Seasonal Peak kW | Summer Seasonal Peak kW | Free- ridership | Spillover | kWh | Winter Seasonal Peak kW | Summer Seasonal Peak kW | | | |
| | Energy Conscious Blueprint | | | | | | | | | | |
| Cooling | 77.0% _(a,1) | $235.0\%_{(a,3)}$ | 72.0% _(a,2) | 29.5% _(d) | 12.4% _(d) | 63.8% | 194.8% | 59.7% | | | |
| Custom | 118.0% _(a,1) | $115.0\%_{(a,3)}$ | 89.0% _(a,2) | $22.5\%_{(d)}$ | 16.9% _(d) | 111.4% | 108.6% | 84.0% | | | |
| Heating | 134.0% _(a,1) | 169.0% _(a,3) | 50.0% _(a,2) | 23.7% _(d) | 28.0% _(d) | 139.8% | 176.3% | 52.2% | | | |
| Lighting | 98.0% _(a,1) | 87.0% _(a,3) | 72.0% _(a,2) | 16.7% _(d) | 2.4% _(d) | 84.0% | 74.6% | 61.7% | | | |
| Motors | 118.0% _(a,1) | 115.0% _(a,3) | 89.0% _(a,2) | 18.2% _(d) | 7.1% _(d) | 104.9% | 102.2% | 79.1% | | | |
| Other | 118.0% _(a,1) | 115.0% _(a,3) | 89.0% _(a,2) | 18.2% _(d) | 7.1% _(d) | 104.9% | 102.2% | 79.1% | | | |
| Process | 112.0% _(a,1) | 106.0% _(a,3) | 199.0% _(a,2) | 17.6% _(d) | 0.9% _(d) | 93.3% | 88.3% | 165.8% | | | |
| Refrigeration | 118.0% _(a,1) | 115.0% _(a,3) | 89.0% _(a,2) | 3.6% _(d) | 25.9% _(d) | 144.3% | 140.6% | 108.8% | | | |
| | | | Energy | Opportunities | S | | | | | | |
| Cooling | 84.3% _(b,1) | 136.3% _(b,3) | 80.2% _(b,2) | 20.0% _(d) | $0.0\%_{(d)}$ | 67.4% | 109.0% | 64.2% | | | |
| Custom | 84.3% _(b,1) | $136.3\%_{(b,3)}$ | 80.2% _(b,2) | 25.9% _(d) | 1.8% _(d) | 64.0% | 103.5% | 60.9% | | | |
| Heating | 84.3% _(b,1) | $136.3\%_{(b,3)}$ | 80.2% _(b,2) | 14.8% _(d) | $0.0\%_{(d)}$ | 71.8% | 116.1% | 68.3% | | | |
| Lighting | 98.8% _(b,1) | $106.7\%_{(b,3)}$ | 104.8% _(b,2) | 10.8% _(d) | 6.3% _(d) | 94.4% | 101.9% | 100.1% | | | |
| Motors | 84.3% _(b,1) | 136.3% _(b,3) | 80.2% _(b,2) | 11.5% _(d) | 4.5% _(d) | 78.3% | 126.6% | 74.5% | | | |
| Other | 84.3% _(b,1) | $136.3\%_{(b,3)}$ | 80.2% _(b,2) | $2.6\%_{(d)}$ | $0.0\%_{(d)}$ | 82.1% | 132.8% | 78.1% | | | |
| Process | 84.3% _(b,1) | 136.3% _(b,3) | 80.2% _(b,2) | 6.9% _(d) | 3.7% _(d) | 81.6% | 131.9% | 77.6% | | | |
| Refrigeration | 84.3% _(b,1) | $136.3\%_{(b,3)}$ | 80.2% _(b,2) | 3.2% _(d) | $0.0\%_{(d)}$ | 81.6% | 131.9% | 77.6% | | | |
| | | | Small Business | s Energy Adva | antage | | _ | | | | |
| Cooling | 100.0% | 100.0% | 100.0% | 15.3% _(d) | 0.2% _(d) | 84.9% | 84.9% | 84.9% | | | |
| Heating | 100.0% | 100.0% | 100.0% | $0.0\%_{(d)}$ | $0.0\%_{(d)}$ | 100.0% | 100.0% | 100.0% | | | |
| Lighting | 99.1% _(c,1) | 66.9% _(c,1) | 77.3% _(c,1) | 3.8% _(d) | 2.5% _(d) | 97.8% | 66.0% | 76.3% | | | |
| Custom | 100.0% | 100.0% | 100.0% | 0.3% _(d) | $0.0\%_{(d)}$ | 99.7% | 99.7% | 99.7% | | | |
| Other | 100.0% | 100.0% | 100.0% | 0.5% _(d) | 0.2% _(d) | 99.8% | 99.8% | 99.8% | | | |
| Comp. Air | 15.0% _(c,2) | 95.4% _(c,3) | 95.4% _(c,3) | 0.3% _(d) | $0.0\%_{(d)}$ | 15.0% | 95.1% | 95.1% | | | |
| Refrigeration | 105.8% _(c,2) | $9.3\%_{(c,3)}$ | 8.9% _(c,3) | 1.4% _(d) | $0.0\%_{(d)}$ | 104.3% | 9.2% | 8.8% | | | |

O&M PRIME 0.0% 0.0% 100.0% 100.0% 100.0% 100.0% 100.0% 100.0% O&M 0.0%0.0% $90.9\%_{(e,2)}$ $64.6\,\%$ $61.9\,\%$ 90.9% $64.6\%_{(e,2)}$ $61.9\%_{(e,2)}$ 0.0% 0.0% 73.9% 102.9% Retro-com $73.9\%_{\underline{(e,1)}}$ $102.9\%_{\underline{(e,1)}}$ $121.4\,\%$ $121.4\%_{(e,1)}$ Load Management **Load Response** 100.0% 100.0% 100.0% 0.0% 0.0% 100.0% 100.0% 100.0%

CL&P & UI Residential Realization Rates

| Gross Realization % | | | | | FR & SO | | Net Reali | zation % (N | Note 4) |
|----------------------------|------------------------|--|-------------------------------|------------------------|-----------------------|-----------------------|-----------|-------------------------------|-------------------------------|
| Measure | kWh (or CcF) | Winter Seasonal Peak kW (or Peak Day CcF) | Summer Seasonal Peak kW | Installation Rate | Free-ridership | Spillover | kWh | Winter Seasonal Peak kW | Summer Seasonal Peak kW |
| | | | Energy Solu | | | | | | |
| Electric measures | 97.6% _(f,1) | $91.9\%_{(f,1)}$ | 83.4% _(f,1) | 100.0% | 0.0% | 0.0% | 97.6% | 91.9% | 83.4% |
| Gas Measures (CcF) | $107.5\%_{(f,1)}$ | $107.5\%_{(f,1)}$ | N/A | 100.0% | 0.0% | 0.0% | 107.5% | 107.5% | N/A |
| | | Home | Energy Sol | lutions-Inco | me eligible | | | - | |
| Bulbs (Note 5) | 100.0% | $73.1\%_{(g,2)}$ | 100.0% | $75.0\%_{(g,1)}$ | 0.0% | 0.0% | 75.0% | 54.8% | 75.0% |
| Portable Lamps (Note 5) | 100.0% | $73.1\%_{(g,2)}$ | 100.0% | $75.0\%_{(g,1)}$ | 0.0% | 0.0% | 75.0% | 54.8% | 75.0% |
| Fixtures (Note 5) | 100.0% | 73.1% _(g,2) | 100.0% | 100.0% | 0.0% | 0.0% | 100.0% | 73.1% | 100.0% |
| Other electric measures | 100.0% | 100.0% | 100.0% | 100.0% | 0.0% | 0.0% | 100.0% | 100.0% | 100.0% |
| Gas Measures (CcF) | 100.0% | 100.0% | N/A | 100.0% | 0.0% | 0.0% | 100.0% | 100.0% | N/A |
| | | | Retai | l Products | | | I. | | |
| CFL Bulbs (Note 6) | 100.0% | 100.0% | 100.0% | 87.1% _(i) | 19.0% _(k) | 0.0% | 81.0% | 81.0% | 81.0% |
| LED Bulbs | 100.0% | 100.0% | 100.0% | 100.0% | 0.0% | 0.0% | 100.0% | 100.0% | 100.0% |
| Portable Lamps | 100.0% | 100.0% | 100.0% | 70.0% _(h,1) | 3.1% _(h,1) | 6.0% _(h,2) | 72.0% | 72.0% | 72.0% |
| Torchiere | 100.0% | 100.0% | 100.0% | 70.0% _(h,1) | 3.1% _(h,1) | 6.0% _(h,2) | 72.0% | 72.0% | 72.0% |
| Hard Wired Fixtures | 100.0% | 100.0% | 100.0% | 80.0% _(h,1) | 3.1% _(h,1) | 6.0% _(h,2) | 82.3% | 82.3% | 82.3% |
| Ceiling Fans & Lights | 100.0% | 100.0% | 100.0% | 80.0% _(h,1) | 3.1% _(h,1) | 6.0% _(h,2) | 82.3% | 82.3% | 82.3% |
| CFL giveaway (Note 6) | 100.0% | 100.0% | 100.0% | 87.1% _(i) | 19.0% _(k) | 0.0% | 81.0% | 81.0% | 81.0% |

| | | | HI | ES Rebate | | | | | |
|-------------------|--------|--------|--------|-------------|----------------------|------|--------|--------|--------|
| Central AC/HP- | 100.0% | 100.0% | 100.0% | 100.0% | 42.0% _(j) | 0.0% | 58.0% | 58.0% | 58.0% |
| CLP | | | | | | | | | |
| Central AC/HP-UI | 100.0% | 100.0% | 100.0% | 100.0% | 26.0% _(i) | 0.0% | 74.0% | 74.0% | 74.0% |
| Other electric | 100.0% | 100.0% | 100.0% | 100.0% | 0.0% | 0.0% | 100.0% | 100.0% | 100.0% |
| measures | | | | | | | | | |
| Gas Measures | 100.0% | 100.0% | 100.0% | 100.0% | 0.0% | 0.0% | 100.0% | 100.0% | 100.0% |
| (CcF) | | | | | | | | | |
| | | | Behavi | oral Progra | ms | | | | |
| Home Energy | 100.0% | 100.0% | 100.0% | 100.0% | 0.0% | 0.0% | 100.0% | 100.0% | 100.0% |
| Reports | | | | | | | | | |
| | | | Appli | ance Turn-I | n | | | | |
| Refrigerator | 100% | 100% | 100% | 100% | 31.0%(1) | 0.0% | 69.0% | 69.0% | 69.0% |
| Recycling | | | | | | | | | |
| Freezer Recycling | 100% | 100% | 100% | 100% | 41.0% ₍₁₎ | 0.0% | 59.0% | 59.0% | 59.0% |

References

- [a] Global Energy Partners, Evaluation of The Energy Conscious Blueprint Program, August 4, 2011.
- [a,1] Table ES-4.

- [a,2] Table ES-5.
- [a,3] Table ES-6.
- [b] KEMA, 2008 Energy Opportunities Program Impact Evaluation, June 18, 2010.
- [b,1] Table 1-1.
- [b,2] Table 1-2.
- [b,3] Table 1-3.
- [c] The Cadmus Group, Connecticut Small Business Energy Advantage Year 2007 Impact Evaluation, Final Report, August 24, 2009
- [c,1] Page ii, footnote 4.
- [c,2] Table ES.2.
- [c,3] Table ES.3.
- [c,4] Page iii, footnote 5.
- [c,5] Page iv, footnote 8.
- [c,6] Table ES.6.
- [c,7] Table ES.7.
- [c,8] Page v, footnote 9.
- [d] PA Consulting Group, CL&P/UI 2007 C&I Program Free-ridership & Spillover, October 28, 2008
- [d,1] Table 1-1.
- [d,2] Table 1-2.
- [d,3] Table 1-3.
- [d,4] Table 1-4.
- [d,5] Table 1-5.
- [d,6] Table 1-6.
- [e] RLW Analytics, Inc., 1999 O&M Services Program Impact Evaluation, Final Report, October 2001.
- [e,1] Page 29, Table 15.
- [e,2] Page 27, Table 14. Note [5]
- [e,3] Page 29, Table 14. Note [6]

- [f] Nexant, Home Energy Solutions Evaluation, Final Report, March 2011.
- [f,1] Page 3, Table E.1-1.
- [g] KEMA, Evaluation of the Weatherization Residential Assistance Partnership (WRAP) and Helps Programs, September 10, 2010
- [g,1] Page 1-13.
- [g,2] Table ES-9, Page 1-11. Note [7]
- [h] Point of Purchase Lighting Impact Evaluation, 2003
- [h,1] Page 6, Table 2.
- [h,2] Page 6, Table 2. Note [8]
- [i] NMR, Residential Markdown Impact Evaluation, January 20, 2009, Page 59, Table 5-21. Note [9]
- [j] ADM Associates, Inc., Residential Central AC Regional Evaluation Free-Ridership Analysis, October 2009, Page 9.
- [k] NMR, 2010 Results of the Multistate CFL Modeling Effort, February 2, 2010, Page VI, Table 3.

Notes

- [1] Realization rates based on references [1], [2], [3] & [5] based on program. If study not available value set to 100%.
- [2] Based on reference [4]. If study not available values set to 0.
- [3] Net Realization = (Gross realization %) x (100%-Freeridership %+ Spillover %) UI caps net realization rate at 100%
- [4] Net Realization = (Gross realization %) x (installation rate %) x (100%-Freeridership %+ Spillover %) UI caps net realization rate at 100%
- [5] Figure derived from net Process RR by backing out free-ridership, 77.5%/(100.0% 12.1%).
- [6] Figure derived from net Process RR by backing out free-ridership, 79.3%/(100.0% 3.1%).
- [7] Figure of 73.1% is the ratio of the evaluated coincidence factor (.19) to the coincidence factor in use (.26). This method of incorporating the evaluation allows the use of a consistent 0.26 coincidence factor throughout lighting.
- [8] Figure of 6.0% is a conservative estimate; estimate from table is 8.5%.
- [9] Installation rate is the average of the first-year installation rate and the lifetime installation rate; this is due to the 4-year measure life, halfway between 1-year and the 7-year measure life used in the study.

APPENDIX 4. LIFETIMES

Commercial and Industrial Lifetimes

Version Date: 10/30/2012

C&I measure life includes equipment life and measure persistence (not savings persistence).

- 1. Equipment Life means the number of years that a measure is installed and will operate until failure, and
- 2. Measure Persistence takes into account business turnover, early retirement of installed equipment, and other reasons measures might be removed or discontinued.

For retrofit/early retirement programs, the measure life will take into account both the expected remaining life of the measure being replaced and the expected changes in baselines over time.

| Description | Retrofit | Lost | Operations | Maintenance | RCx |
|---|------------------------|------------------------|--------------------|------------------|-----------|
| T' 1.0' C 1 1' | | Opportunity | | | |
| Lighting Systems, including | | T | T | Lazza | |
| Fixtures | 13 _(a) | 15 _(a) | N/A | N/A | N/A |
| CFLs | 5 _(a) | N/A | | | |
| LEDs | $8_{(g)}$ | N/A | | | |
| Lamp and Ballast Conversions | 13 _(a) | N/A | N/A | N/A | N/A |
| Remove Unnecessary Lighting Fixtures | 5 _(g) | N/A | N/A | N/A | N/A |
| Lamp Replacement | N/A | N/A | 5 _(g) | 5 _(g) | N/A |
| Sweep Controls / EMS Based Controls | $10_{(a,*)}$ | 15 _(a,*) | N/A | N/A | N/A |
| Occupancy Sensors | 9 _(a) | 10 _(a) | N/A | N/A | N/A |
| Automatic Photocell Dimming Systems | 9 _(a) | $10_{(a)}$ | N/A | N/A | N/A |
| Recircuiting and New Controls | $10_{(a,*)}$ | N/A | N/A | N/A | N/A |
| Bi-Level Switching (Demand Reduction) | $10_{(a,*)}$ | 10 _(a,*) | N/A | N/A | N/A |
| Timer Switch | $10_{(a,*)}$ | N/A | N/A | N/A | N/A |
| Reprogramming of EMS Controls | N/A | N/A | 5 _(b,2) | N/A | $8_{(g)}$ |
| Fluorescent Lighting system power reduction | $9_{(a,*)}$ | N/A | N/A | N/A | N/A |
| controls | | | | | |
| Building Envelope | | | | | |
| Insulation | 20 _(c/19) | 20 _(c/19) | N/A | N/A | N/A |
| New Windows | N/A | 20 _(c/16) | N/A | N/A | N/A |
| Window Film | $10_{(c/18)}$ | 10 _(c/18) | N/A | N/A | N/A |
| Movable Window Insulation | $10_{(g)}$ | $10_{(g)}$ | N/A | N/A | N/A |
| Roof Spray Cooling | 15 _(g) | 15 _(g) | N/A | N/A | N/A |
| Cool Roofs | N/A | 15 _(c/14) | N/A | N/A | N/A |
| Domestic Hot Water | • | • | • | • | |
| Heat Pump Water Heater | 10 _(c/143*) | 10 _(c/143*) | N/A | N/A | N/A |
| Point-of-Use Water Heater | $20_{(c/95)}$ | 20 _(c/95) | N/A | N/A | N/A |
| Gas Fired Water Heater | N/A | 15 _(c/93) | N/A | N/A | N/A |
| Solar Water Heater | $20_{(g)}$ | 20 _(g) | N/A | N/A | N/A |
| Heat Recovery | 15 _(g) | 15 _(g) | N/A | N/A | N/A |
| Energy-Efficient Motors | 15 _(a) | 20 _(a) | N/A | N/A | N/A |
| Pre-Rinse Spray Valve | 5 _(h) | N/A | N/A | N/A | N/A |
| Heating, Ventilating and Air Condition (HVA | | 1 | 1 | 1 | |
| Energy-Efficient Motors | 15 _(a) | 20 _(a) | N/A | N/A | N/A |
| C. | (u) | (u) | I | | |

| Description | Retrofit | Lost Opportunity | Operations | Maintenance | RCx |
|---|----------------------|-----------------------|-------------|--------------------|------------------|
| Variable Speed Drives | 13 _(b,1) | 15 _(b,1) | N/A | N/A | N/A |
| High-Efficiency Unitary Equipment (A/C and Heat Pumps) | N/A | 15 _(a) | N/A | N/A | N/A |
| Energy-Efficient Packaged Terminal Units | N/A | 15 _(a) | N/A | N/A | N/A |
| Dehumidifiers | 13 _(g) | 15 _(g) | N/A | N/A | N/A |
| Evaporative Cooling (unitary) | N/A | 15 _(a,*) | N/A | N/A | N/A |
| 2-Speed Motor Control in Rooftop units | 13 _(a,*) | 15 _(a,*) | N/A | N/A | N/A |
| Electric Chillers | N/A | 23 _(a) | N/A | N/A | N/A |
| Gas Engine Chillers | N/A | 15 _(d) | N/A | N/A | N/A |
| Cool Thermal Storage | 15 _(g) | 15 _(g) | N/A | N/A | N/A |
| Cooling Tower Alternates | 13 _(g) | 15 _(c/45*) | N/A | N/A | N/A |
| Air Distribution System Modifications & Conversions | 20 _(g) | 20 _(g) | N/A | N/A | N/A |
| VAV System Components | 13 _(g) | N/A | N/A | N/A | N/A |
| Plate/Heat Pipe Type Heat Recovery System | 14 _(c/27) | 14 _(c/27) | N/A | N/A | N/A |
| Rotary Type Heat Recovery System | 14 _(c/41) | 14 _(c/41) | N/A | N/A | N/A |
| Economizer - Air/Water | 7 _(a) | 10 _(a) | N/A | N/A | N/A |
| Low-Leakage Damper | 12 _(g) | 12 _(g) | N/A | 5 _(b,2) | N/A |
| Repair Air Side Economizer | N/A | N/A | N/A | 5 _(b,2) | N/A |
| Outdoor Air Damper Adjustment or Modification | N/A | N/A | N/A | 5 _(b,2) | N/A |
| Make-up Air Unit for Exhaust Hood | 15 _(g) | 15 _(g) | N/A | N/A | N/A |
| Paddle Type Air Destratification Fan | 15 _(f*) | 15 _(f*) | N/A | N/A | N/A |
| Duct Type Air Destratification System | 15 _(f*) | 15 _(f*) | N/A | N/A | N/A |
| Air Curtain | 15 _(g) | 15 _(g) | N/A | N/A | N/A |
| Water/Steam Distribution System Modifications & Conversions | 20 _(g) | 20 _(g) | N/A | N/A | N/A |
| Zoned Circulator Pump System | $15_{(g)}$ | N/A | N/A | N/A | N/A |
| Electric Spot Radiant Heat | $10_{(g)}$ | $10_{(g)}$ | N/A | N/A | N/A |
| Additional Vessel Insulation | $10_{(g)}$ | $10_{(g)}$ | N/A | N/A | N/A |
| Additional Pipe Insulation | $10_{(g)}$ | $10_{(g)}$ | N/A | N/A | N/A |
| Repair Steam/Air Leaks | N/A | N/A | N/A | $5_{(b,2)}$ | N/A |
| Gas Fired Boiler (Non-Condensing) | N/A | 20 _(c/24) | N/A | N/A | N/A |
| Gas Fired Boiler (Condensing) | N/A | 15 _(g) | N/A | N/A | N/A |
| Gas Furnace | N/A | 20 _(c/24*) | N/A | N/A | N/A |
| Gas Fired Radiant Heater | N/A | 15 _(g) | N/A | N/A | N/A |
| Duct Sealing | 18 _(c/31) | N/A | N/A | N/A | N/A |
| Duct Insulation | 20 _(a,**) | N/A | N/A | N/A | N/A |
| HVAC Controls | | | | | |
| EMS/Linked HVAC Controls | $10_{(a)}$ | 15 _(a) | N/A | N/A | $8_{(g)}$ |
| New/Additional EMS Points | 10 _(a) | 15 _(a) | N/A | N/A | N/A |
| Single Zone Controls NOT Linked to other | 10 _(a) | N/A | N/A | N/A | N/A |
| Controls | | | | | |
| Time Clocks | 11 _(c/43) | N/A | N/A | N/A | N/A |
| Modify HVAC Controls | $10_{(a)}$ | N/A | N/A | N/A | 8 _(g) |
| Repair HVAC Controls | N/A | N/A | N/A | $5_{(b,2)}$ | N/A |
| Adjust Scheduling | N/A | N/A | $5_{(b,2)}$ | N/A | $6_{(g)}$ |

| Description | Retrofit | Lost Opportunity | Operations | Maintenance | RCx |
|--|--|-----------------------|--------------------|--------------------|----------------------|
| Reset Setpoints | N/A | N/A | 5 _(b,2) | N/A | $6_{(g)}$ |
| Reprogramming of EMS Controls | N/A | N/A | 5 _(b,2) | N/A | 8 _(g) |
| Controls to Eliminate Simultaneous Heating and | $10_{(a)}$ | N/A | 5 _(b,2) | N/A | 8 _(g) |
| Cooling | | | | | |
| Demand Control Ventilation - Single Zone | $10_{(a)}$ | $10_{(g)}$ | N/A | N/A | 8 _(g) |
| Demand Control Ventilation - Multi Zone | $10_{(a)}$ | $10_{(g)}$ | N/A | N/A | N/A |
| Enthalpy Control Economizer | $7_{(a)}$ | $10_{(a)}$ | N/A | N/A | N/A |
| Upgrade to dual/comparative Enthalpy | $10_{(a,*)}$ | 10 _(a,*) | N/A | N/A | N/A |
| Economizer | 0 | 27/4 | 27/4 | 37/4 | 27/4 |
| Programmable Thermostat | 8 _(a) | N/A | N/A | N/A | N/A |
| Refrigeration | | T | | 1 | _ |
| Industrial Refrigeration Systems/Components | $20_{(b,1)}$ | 20 _(b,1) | $3_{(g)}$ | N/A | N/A |
| Commercial Refrigeration Systems/Components | 15 _(c/85) | 15 _(c/85) | $3_{(g)}$ | N/A | N/A |
| Heat Recovery from Refrigeration System | 10 _(c/80) | 13 _(g) | N/A | N/A | N/A |
| Refrigeration Controls | $10_{(b,1)}$ | $10_{(b,1)}$ | 5 _(b,2) | N/A | 10 _(c/86) |
| Adjust Scheduling | N/A | N/A | $5_{(b,2)}$ | N/A | 8 _(g) |
| Reset Setpoints | N/A | N/A | 5 _(b,2) | N/A | 8 _(g) |
| Mechanical Subcooling | 15 _(c/85) | 15 _(c/85) | N/A | N/A | N/A |
| Ambient Subcooling | 15 _(c/85) | 15 _(c/85) | N/A | N/A | N/A |
| Auto Cleaning System for Condenser Tubes | $10_{(g)}$ | $10_{(g)}$ | N/A | N/A | N/A |
| Hot Gas Bypass for Defrost or Regeneration | $10_{(g)}$ | $10_{(g)}$ | N/A | N/A | N/A |
| Open or Enclosed Display Cases | 12 _(c/76) | 12 _(c/76) | N/A | N/A | N/A |
| Case Cover | 5 _(c/84) | $5_{(c/84)}$ | N/A | N/A | N/A |
| Polyethylene Strip Curtain | 4 _(c/88) | 4 _(c/88) | N/A | N/A | N/A |
| Motorized Insulated Doors | 8 _(c/75) | 8 _(c/75) | N/A | N/A | N/A |
| Oversized Condensers | 15 _(c/85) | 15 _(c/85) | N/A | N/A | N/A |
| Low Case HVAC Returns | $10_{(g)}$ | $10_{(g)}$ | N/A | N/A | N/A |
| Demineralized Water for Ice | $10_{(g)}$ | $10_{(g)}$ | N/A | N/A | N/A |
| Electronically Commutated Motors | 15 _(c/85) | 15 _(c/85) | N/A | N/A | N/A |
| Low Emissivity Ceiling Surface | $15_{(g)}$ | 15 _(g) | N/A | N/A | N/A |
| Additional Pipe Insulation - Refrigeration System | 11 _(c/83) | 11 _(c/83) | N/A | N/A | N/A |
| Additional Vessel Insulation - Refrigeration | 11 _(c/83*) | 11 _(c/83*) | N/A | N/A | N/A |
| System | | | | | |
| Process Equipment | L 12 | 1.7 | NT/A | I NT/A | LATIA |
| Air Compressor | 13 _(b,1) | 15 _(b,1) | N/A | N/A | N/A |
| Refrigerated Air Dryer | 13 _(b,1) | 15 _(b,1) | N/A | N/A | N/A |
| Variable Frequency Drives | $13_{(b,1)}$ | 15 _(b,1) | N/A | N/A | N/A |
| Repair Steam/Compressed Air Leaks | N/A | N/A | N/A | 5 _(b,2) | N/A |
| Add Regulator Valves in Compressed Air System | $10_{(g)}$ | 10 _(g) | N/A | N/A | 10 _(c/86) |
| Install Air Compressor No-Loss Condenser Drains | $10_{(g)}$ | $10_{(g)}$ | N/A | 5 _(b,2) | 10 _(c/86) |
| Interlock Air System Solenoid Valves with | $10_{(a,*)}$ | 10 _(a,*) | N/A | N/A | 10 _(c/86) |
| Machine Operation Interlock Exhaust Fans with Machine Operations | 10 _(a,*) | 10 _(a,*) | N/A | N/A | 10 _(c/86) |
| Injection Molding Machine Jackets | | N/A | N/A N/A | N/A N/A | N/A |
| Compressed Air Distribution and Storage Systems | $ \begin{array}{c} 5_{(g)} \\ 10_{(g)} \end{array} $ | N/A N/A | N/A N/A | N/A N/A | N/A |
| Plastic Injection Molding Machine | | | N/A N/A | N/A N/A | N/A N/A |
| Energy-Efficient Motors | 13 _(g) | 15 _(g) | N/A N/A | N/A N/A | N/A N/A |
| Energy-Efficient Motors | $15_{(a)}$ | 20 _(a) | IN/A | 1W/A | IN/A |

| Description | Retrofit | Lost | Operations | Maintenance | RCx |
|-------------------------------|---------------------|-------------------------|------------|-------------|-----|
| | | Opportunity | | | |
| Energy Efficient Transformers | 15 _(a,*) | 20 _(a,*) | N/A | N/A | N/A |
| Water treatment magnets | $10_{(g)}$ | N/A | N/A | N/A | N/A |
| PRIME | N/A | 5 _(e) | N/A | N/A | N/A |
| Clothes Washer | N/A | 11 _(i) | N/A | N/A | N/A |
| Kitchen Equipment | | | | | |
| Cooking Equipment | N/A | 12 _(c/20-23) | N/A | N/A | N/A |

Changes from Last Version

Identified source references.

References

- [a] GDS Associates Inc, Measure Life Report, Residential and Commercial Industrial Lighting and HVAC Measures, June 2007, Table 2.
- [a,*] This measure is similar to those in the report, so a measure life from Table 2 was used.
- [a,**] This measure is similar to those in the report, so a measure life from Table 1 was used.
- [b] Energy & Resource Solutions (ERS), Measure Life Study: prepared for The Massachusetts Joint Utilities, October 10, 2005.
- [b,1] Table 1-1.
- [b,2] Page 4-9.
- [c] California Public Utilities Commission, 2008 Database for Energy-Efficient Resources, Version 2008.2.05, December 16, 2008, EUL/RUL (Effective/Remaining Useful Life) Values, MS Excel Spreadsheet. [c/#] Row #.
- [c/#*] Similar measure to row #; row # used.
- [d] Gas chiller measure life was set by the CT DPUC in their decision in Docket 05-07-14, in response to Public Act 05-01, "An Act Concerning Energy Independence". Dec 28, 2005, Page 29, Table 4
- [e] Energy & Resource Solutions (ERS), Process Reengineering for Increased Manufacturing Efficiency Program Evaluation, March 26, 2007, Page 1-5.
- [f*] Efficiency Maine TRM, 3/5/07, Page 91. Similar measure.
- [g] Estimate.
- [h] Veritec Consulting, "Region of Waterloo Pre-Rinse Spray Valve Pilot Study Final Report", January, 2005, Executive Summary.
- [i] Appliance Magazine. U.S. Appliance Industry: Market Share, Life Expectancy & Replacement Market, and Saturation Levels. January 2010. Page 10.

Version Date: 10/30/2012 Residential Lifetimes

Residential Lifetimes

Measure life for residential measures includes equipment life and measure persistence (not savings persistence).

Equipment life means the number of years that a measure is installed and will operate until failure, and measure persistence takes into account transfer of ownership, early retirement of installed equipment, and other reasons measures might be removed or discontinued.

Gross lifetime energy savings are calculated by multiplying the gross annual energy savings by the measure life in the following table. Likewise, net lifetime savings are calculated by multiplying the net energy by the measure life in the following table.

The residential programs use a slightly different definition of "retrofit" savings than C&I programs. Where "retrofit" measures in C&I utilize a blended "retrofit" lifetime, Residential measures utilize a two-part lifetime savings calculation. In certain situations, such as early retirement, savings may be claimed in two parts, where the retirement part is additional to the lost opportunity part until the end of the remaining useful life (RUL), after which lost opportunity savings continue until the last year of the retrofit measure's effective useful life (EUL).

For example, in an "Early Retirement" case where the existing unit (using lower efficiency, out-of date technology) would have been operating until failure and early retirement is stimulated by the program measure, savings may be claimed between the existing unit to the standard baseline unit (driven by the level of efficiency most standard units achieve), for the retirement measure life. The residential "retirement" lifetime refers to how much longer the existing unit would have operated absent the influence of the program.

Lost Opportunity lifetimes apply to the portion of savings due to choosing a high efficiency product over a standard efficiency product available on the market.

Both Retail and New Home measure applications fall under the Lost Opportunity category, while measures applied in existing homes and turn-in measures may be eligible for both Retirement and Retrofit.

Numbers in parentheses refer to lifetimes specially pertaining to a low income home.

| | Existing Home, Retirement RUL | Existing Home, Retrofit EUL | New Home & Retail, Lost Opportunity EUL | Comments |
|---|-------------------------------------|-----------------------------------|---|-------------------|
| Light Bulbs | | | | |
| CFL, General Service | N/A | 4 | 4 | Notes [1], [2] |
| CFL, Non-General Service 6,000 hr | N/A | 4 | 4 | Note [1] |
| CFL, Non-General Service 7,000 hr | N/A | 4 | 4 | Note [1] |
| CFL, Non-General Service, 8,000 hr | N/A | 5 | 5 | Note [1] |
| CFL, Non-General Service, 10,000 hr | N/A | 6 | 6 | Note [1] |
| CFL, Non-General Service, 12,000 hr | N/A | 7 | 7 | Note [1] |
| CFL, Non-General Service, 15,000 hr | N/A | 8 | 8 | Note [1] |
| CFL, Non-General Service, >15,000 hr | N/A | 8 | 8 | Note [1] |
| LED, Down light | N/A | $16_{(b,1)}$ | $16_{(b,1)}$ | Note [4] |
| LED, General Service | N/A | 10 | 10 | Ref [2], Note [4] |
| LED, Non-General Service, Non-Downlight | N/A | 10 | 10 | Ref [2], Note [4] |

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| | Existing Home, | Existing | New Home & | Comments |
|--|-----------------------|--------------------------------------|---------------------|----------|
| | Retirement | Home, | Retail, Lost | |
| | RUL | Retrofit EUL | Opportunity EUL | |
| Luminaires | 1 | T | 1 | 1 |
| CFL, Hardwired Indoor Fixture | N/A | 16 _(b,1) | 16 _(b,1) | |
| CFL, Hardwired Exterior Fixture | N/A | $6_{(e,1)}$ | $6_{(e,1)}$ | |
| CFL, Portable Table Lamp | N/A | 8 _(c) | 8 _(c) | |
| CFL, Portable Torchiere | N/A | 8 _(c) | $8_{(c)}$ | |
| CFL, Security Exterior | N/A | 15 _(d,3) | $15_{(d,3)}$ | |
| LED, Portable Table Lamp | N/A | 8 _(c) | 8 _(c) | |
| LED, Portable Torchiere | N/A | 8 _(c) | $8_{(c)}$ | |
| LED, Hardwired Exterior Fixture | N/A | $16_{(b,1)} \ 16_{(b,1)}$ | $16_{(b,1)}$ | |
| LED, Hardwired Indoor Fixture | N/A | | $16_{(b,1)}$ | |
| Heating, Ventilation, and Air-Conditioning | (HVAC) systems | | | |
| Central Air Conditioning System | 5 _(d) | 18 _(c) | 25 _(c) | |
| Air Source Heat Pump | 5 _(d) | 18 _(c) | 25 _(c) | |
| Geothermal Heat Pump | N/A | 18 _(c) | 25 _(c) | |
| Ductless Split Heat Pump | N/A | 18 _(c) | N/A | |
| Package Terminal Heat Pump | 5 _(d) | 18 _(c) | N/A | |
| Furnace (Gas) | $5_{\rm (d)}$ | 20 _(d) | $20_{(d)}$ | |
| Boiler (Gas) | $5_{(d)}$ | 20 _(a) | 20 _(a) | |
| QIV, Central Air Conditioning System | N/A | 18 _(c) | 18 _(c) | |
| QIV, Air Source Heat Pump | N/A | 18 _(c) | 18 _(c) | |
| QIV, Geothermal Heat Pump | N/A | 18 _(c) | 18 _(c) | |
| QIV, Boiler (Boiler Reset) | N/A | 20 _(a) | 20 _(a) | |
| Electronically Commutated Motor (Fan) | N/A | 18 _(c) | 18 _(c) | |
| Duct Blaster Test (New Construction) | N/A | N/A | 25 _(c) | |
| Duct Sealing | N/A | 20 _(c) | N/A | |
| Duct Insulation | N/A | 20 _(c) | N/A | |
| Appliances | • | | • | • |
| Room AC Units | 4 _(d) | 9 _(a) | 9 _(a) | |
| Clothes Washers | 4 _(d) | 11 _(a) | 11 _(a) | |
| Dish Washers | 4 _(d) | 10 _(a) | 10 _(a) | |
| Refrigerators | 5 (10) _(d) | 12 _(a) | 12 _(a) | |
| Freezers | 4 (8) _(d) | 11 _(a) | 11 _(a) | |
| Dehumidifiers | 4 _(d) | 12 _(c) | 12 _(c) | |
| Envelope | - (u) | (c) | (c) | <u> </u> |
| Blower Door | N/A | 20 _(c) | 25 _(c) | |
| Air Sealing and Weatherization (Non- | N/A | $20_{(c)}$ | N/A | |
| Blower Door) | 1471 | 20(c) | 1471 | |
| Thermal Bypass | N/A | N/A | 25 _(c) | |
| Insulation | N/A | 25 _(c) | N/A | |
| Window Replacement | N/A | 25 _(c) | N/A | |
| Storm Window Installation | N/A | 20 _(c) | N/A | |
| Broken Window Repair | N/A | $5_{(d)}$ | N/A | |
| Insulating Attic Openings | N/A | 25 _(c) | N/A | |
| Domestic Hot Water | 2.772 | (c) | ***** | 1 |
| Water Heater Thermostat Setting (Existing | N/A | 4 | N/A | |
| Unit) | 11/71 | 4 _(d) | 17/71 | |
| Low Flow Shower Head | N/A | 5 | N/A | |
| Water Heater Wrap | N/A N/A | 5 _(d) 5 _(d) | N/A N/A | |
| Flip and Faucet Aerators | N/A N/A | $5_{(d)}$ | N/A N/A | |
| Pipe Insulation | 11/71 | 15 _(d) | N/A N/A | |
| 1 ipe ilisulation | | 1 J(d) | 14/74 | 1 |

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| | Existing Home, Retirement RUL | Existing Home, Retrofit EUL | New Home & Retail, Lost Opportunity EUL | Comments |
|---|-------------------------------------|-----------------------------------|---|----------|
| Heat Pump Water Heater | | 12 _(d) | 12 _(d) | |
| High Efficiency Indirect Gas Water Heater | | N/A | $20_{(d)}$ | |
| On Demand Tankless Gas Water Heater | | $20_{(b,2)}$ | $20_{(b,2)}$ | |
| REM Savings (for ENERGY STAR Homes |) | | | |
| Heating | N/A | N/A | 25 _(c) | |
| Cooling | N/A | N/A | 25 _(c) | |
| Dom. Water Heating | N/A | N/A | 25 _(c) | |
| BOP (Builder Option Plan for ENERGY S' | ΓAR homes) | | | |
| Heating | N/A | N/A | 25 _(c) | |
| Cooling | N/A | N/A | 25 _(c) | |
| Dom. Water Heating | N/A | N/A | 25 _(c) | |
| Behavioral Programs | | | | |
| Home Energy Reports | N/A | 1 _(d) | N/A | [5] |

Changes from Last Version

Identified source references

References

- [a] Appliance Magazine. U.S. Appliance Industry: Market Share, Life Expectancy & Replacement Market, and Saturation Levels. January 2010. Page 10.
- [b] California Public Utilities Commission, 2008 Database for Energy-Efficient Resources, December 16, 2008. http://www.deeresources.com/deer0911planning/downloads/EUL_Summary_10-1-08.xls, last accessed May 31, 2011, Version 2008.2.05.
 - [b,1] Cell D135.
 - [b,2] Cell D146.
 - [b,3] Cell D141.
- [c] GDS Associates Inc. Measure Life Report, Residential and Commercial Industrial Lighting and HVAC Measures, June 2007, Table 1.
- [d] Estimated.
- [e] Nexus Market Research, Inc. (NMR). RLW Analytics, Inc. Residential Lighting Measure Life Study, June 4, 2008.
 - [e,1] Page 1, Table 1-2.

Notes

- [1] Based on Ref [4], Ref [2], and Ref [5]. References [4] and [2] present a CFL switching degradation factor (SDF) of 0.523 to calculate Effective Useful Life (EUL): EUL = Rated lifetime hours * SDF / (annual hours). Based on 2.8 hr/day from NMR 2009.
- [2] General Service CFLs have been capped at 4 years to reflect measure persistence.
- [3] Exterior fixture from Ref [5], Table 1-2, Page 1.
- [4] LED Bulbs are rated at 25,000 hour life, but have been capped here to the fixture lifetime.
- [5] Persistence of behavioral savings is conservatively assumed to be zero.

APPENDIX 5. HOURS OF USE

Commercial and Industrial Hours of Use and EFLH

(Note[1])

| Facility Type | Lighting Hours | Cooling FLHrs | Heating FLHrs | Fan Motor Hours | CHWP & Cooling Towers (Note [2]) | Heating Pumps (Note [2]) |
|----------------------------------|-------------------|------------------|------------------|-----------------------|---|--------------------------------|
| Auto Related | 4,056 | 837 | 1,171 | 4,056 | 1,878 | 5,376 |
| Bakery | 2,854 | 681 | 1,471 | 2,854 | 1,445 | 5,376 |
| Banks, Financial Centers | 3,748 | 797 | 1,248 | 3,748 | 1,767 | 5,376 |
| Church | 1,955 | 564 | 1,694 | 1,955 | 1,121 | 5,376 |
| College - Cafeteria | 6,376 | 1,139 | 594 | 6,376 | 2,713 | 5,376 |
| College - Classes/Administrative | 2,586 | 646 | 1,537 | 2,586 | 1,348 | 5,376 |
| College - Dormitory | 3,066 | 709 | 1,418 | 3,066 | 1,521 | 5,376 |
| Commercial Condos | 4,055 | 837 | 1,172 | 4,055 | 1,877 | 5,376 |
| Convenience Stores | 6,376 | 1,139 | 594 | 6,376 | 2,713 | 5,376 |
| Convention Center | 1,954 | 564 | 1,695 | 1,954 | 1,121 | 5,376 |
| Court House | 3,748 | 797 | 1,248 | 3,748 | 1,767 | 5,376 |
| Dining: Bar Lounge/Leisure | 4,182 | 854 | 1,140 | 4,182 | 1,923 | 5,376 |
| Dining: Cafeteria / Fast Food | 6,456 | 1,149 | 574 | 6,456 | 2,742 | 5,376 |
| Dining: Family | 4,182 | 854 | 1,140 | 4,182 | 1,923 | 5,376 |
| Entertainment | 1,952 | 564 | 1,695 | 1,952 | 1,120 | 5,376 |
| Exercise Center | 5,836 | 1,069 | 728 | 5,836 | 2,518 | 5,376 |
| Fast Food Restaurants | 6,376 | 1,139 | 594 | 6,376 | 2,713 | 5,376 |
| Fire Station (Unmanned) | 1,953 | 564 | 1,695 | 1,953 | 1,121 | 5,376 |
| Food Stores | 4,055 | 837 | 1,172 | 4,055 | 1,877 | 5,376 |
| Gymnasium | 2,586 | 646 | 1,537 | 2,586 | 1,348 | 5,376 |
| Hospitals | 7,674 | 1,308 | 270 | 7,674 | 3,180 | 5,376 |
| Hospitals / Health Care | 7,666 | 1,307 | 272 | 7,666 | 3,177 | 5,376 |
| Industrial - 1 Shift | 2,857 | 681 | 1,470 | 2,857 | 1,446 | 5,376 |
| Industrial - 2 Shift | 4,730 | 925 | 1,003 | 4,730 | 2,120 | 5,376 |
| Industrial - 3 Shift | 6,631 | 1,172 | 530 | 6,631 | 2,805 | 5,376 |
| Laundromats | 4,056 | 837 | 1,171 | 4,056 | 1,878 | 5,376 |
| Library | 3,748 | 797 | 1,248 | 3,748 | 1,767 | 5,376 |
| Light Manufacturers | 2,857 | 681 | 1,470 | 2,857 | 1,446 | 5,376 |
| Lodging (Hotels/Motels) | 3,064 | 708 | 1,418 | 3,064 | 1,521 | 5,376 |
| Mall Concourse | 4,833 | 938 | 978 | 4,833 | 2,157 | 5,376 |
| Manufacturing Facility | 2,857 | 681 | 1,470 | 2,857 | 1,446 | 5,376 |
| Medical Offices | 3,748 | 797 | 1,248 | 3,748 | 1,767 | 5,376 |
| Motion Picture Theatre | 1,954 | 564 | 1,695 | 1,954 | 1,121 | 5,376 |
| Multi-Family (Common Areas) | 7,665 | 1,306 | 273 | 7,665 | 3,177 | 5,376 |
| Museum | 3,748 | 797 | 1,248 | 3,748 | 1,767 | 5,376 |
| Nursing Homes | 5,840 | 1,069 | 727 | 5,840 | 2,520 | 5,376 |

| Facility Type | Lighting Hours | Cooling FLHrs | Heating FLHrs | Fan Motor Hours | CHWP & Cooling Towers (Note [2]) | Heating Pumps (Note [2]) |
|---|-------------------|------------------|------------------|-----------------------|---|--------------------------------|
| Office (General Office Types) | 3,748 | 797 | 1,248 | 3,748 | 1,767 | 5,376 |
| Office/Retail | 3,748 | 797 | 1,248 | 3,748 | 1,767 | 5,376 |
| Parking Garages & Lots | 4,368 | 878 | 1,094 | 4,368 | 1,990 | 5,376 |
| Penitentiary | 5,477 | 1,022 | 817 | 5,477 | 2,389 | 5,376 |
| Performing Arts Theatre | 2,586 | 646 | 1,537 | 2,586 | 1,348 | 5,376 |
| Police / Fire Stations (24 Hr) | 7,665 | 1,306 | 273 | 7,665 | 3,177 | 5,376 |
| Post Office | 3,748 | 797 | 1,248 | 3,748 | 1,767 | 5,376 |
| Pump Stations | 1,949 | 563 | 1,696 | 1,949 | 1,119 | 5,376 |
| Refrigerated Warehouse | 2,602 | 648 | 1,533 | 2,602 | 1,354 | 5,376 |
| Religious Building | 1,955 | 564 | 1,694 | 1,955 | 1,121 | 5,376 |
| Residential (Except Nursing Homes) | 3,066 | 709 | 1,418 | 3,066 | 1,521 | 5,376 |
| Restaurants | 4,182 | 854 | 1,140 | 4,182 | 1,923 | 5,376 |
| Retail | 4,057 | 837 | 1,171 | 4,057 | 1,878 | 5,376 |
| School / University (Ref [1]) | 2,187 | 594 | 1,637 | 2,187 | 1,205 | 5,376 |
| Schools (Jr./Sr. High) (Ref [1]) | 2,187 | 594 | 1,637 | 2,187 | 1,205 | 5,376 |
| Schools (Preschool/Elementary) (Ref [1]) | 2,187 | 594 | 1,637 | 2,187 | 1,205 | 5,376 |
| Schools (Technical/Vocational) (Ref [1]) | 2,187 | 594 | 1,637 | 2,187 | 1,205 | 5,376 |
| Small Services | 3,750 | 798 | 1,247 | 3,750 | 1,768 | 5,376 |
| Sports Arena | 1,954 | 564 | 1,695 | 1,954 | 1,121 | 5,376 |
| Town Hall | 3,748 | 797 | 1,248 | 3,748 | 1,767 | 5,376 |
| Transportation | 6,456 | 1,149 | 574 | 6,456 | 2,742 | 5,376 |
| Warehouse (Not Refrigerated) | 2,602 | 648 | 1,533 | 2,602 | 1,354 | 5,376 |
| Waste Water Treatment Plant | 6,631 | 1,172 | 530 | 6,631 | 2,805 | 5,376 |

Changes from Last Version

Version Date: 10/30/2012

Added notes, Modified heating pumps to be based on 8 months of operation per year.

References

[1] "CT & MA Utilities 2004-2005 Lighting Hours of Use for School Buildings Baseline Study", Final Report, September 7, 2006, by RWL Analytics.

Notes

- [1] The hours listed in table are default hours to be used when site specific hours are not available. These hours have been developed over the years and are taken into account during program evaluations. Any errors, whether positive or negative, are trued up in the realization rates. Significant changes to this table will only be done if the evaluation contractor provides "going forward" realization rates along with updated hours.
- [2] Since it is common to have redundant pumps, the hours provided above are estimated based on full operation of only the pumps(s) required to maintain system flow (lead pump(s)). Therefore, lag pump(s) have 0 hours of operation even if the pumps are typically alternated. For example, if a system had two 10hp pumps but only one was required to operate at any given time to maintain system flow (lead/lag), then the EFLH's would be based on one 10hp pump.

APPENDIX 6. NOMENCLATURE

Abbreviations/Acronyms

| Symbol | Description (See Note [1]) | Units |
|----------|---|-----------------------------|
| A | Amperage (of fan) | Amps |
| A | Area | Ft^2 , in^2 |
| AA | Hartford kWh savings factor from pilot | kWh/ 1000 Btu |
| ABTU | Annual Btu Savings | Btu/yr |
| AC | Air Conditioning | |
| AC | Annual Cooling Energy Usage | kWh/yr |
| ACCF | Annual Natural Gas Energy Savings | Ccf/yr |
| ACOP | Average Coefficient of Performance | |
| ADET | Annual Differential Electrical energy savings per Ton | kWh/Ton/yr |
| ADHW | Annual domestic water heating load | Btu/yr |
| AEC | Annual Electric Cooling Usage per sq ft | kWh/ft²/ yr |
| AEH | Annual Electric Heating Usage per sq ft | kWh/ft²/ yr |
| AF/BI | Air foil / backward inclined fan | , |
| AFUE | Annual Fuel Utilization Efficiency | |
| AGU | Annual Gas Usage per sq ft | Ccf/ ft ² /yr |
| AH | Annual heating energy usage | kWh/yr |
| AKW | Average hourly demand savings for both summer and winter | |
| AKWH | Annual gross electric energy savings | kWh/yr |
| AOG | Annual Oil Savings | Gallon/yr |
| AOU | Annual Oil Usage per sq ft | gal/ft²/yr |
| APG | Annual Propane Savings | Gallon/yr |
| APU | Annual Propane Usage per sq ft | gal/ft²/yr |
| ASF | Annual Savings Factor | kWh/ton |
| ASHRAE | American Society of Heating, Refrigerating and Air-Conditioning | |
| | Engineers | |
| AV | Adjusted Volume | ft ³ |
| BB | Hartford kW savings factor from pilot | kW/ 1000 Btu |
| BCR | Benefit Cost Ratio | |
| BER | Total Annual Clothes Washer Btu Equivalent energy Reduction | Btu/yr |
| BHP | Brake Horsepower (motor load) | |
| BI | Backward Incline (Fan) | |
| BIY | Baseline Implementation Year | |
| BTU | British Thermal Unit | BTU |
| BTUH | Heat Transfer rate of ducting | Btu/hr/ 100 ft ² |
| C&I | Commercial and Industrial | |
| C&LM | Conservation And Load Management | |
| CAC | Central Air Conditioning | |
| CAP | Capacity of the Equipment | BTU/h or Ton |
| CC | Bridgeport kWh savings factor from pilot | kWh/ 1000 Btu |
| Ccf, CCF | 100 Cubic Feet, quantity of natural gas | 100 Cubic Feet |
| CDD | Cooling Degree Days for CT | 603 |
| CEEF | Connecticut Energy Efficiency Fund | |
| CF | Seasonal Coincidence Factor | |
| CFL | Compact Florescent Light | 2 |
| CFM | Cubic Feet per Minute, Air Flow rate | ft ³ /min |
| CHWP | Chilled Water Pump | |
| CL&P | Connecticut Light and Power | |

| Symbol | Description (See Note [1]) | Units |
|-------------|---|--------------|
| COP | Coefficient of Performance | |
| CWP | Condenser Water Pump | |
| d | Duration | minutes |
| D | Density | lb/Gal |
| D | Dimension (height or width) | inches |
| Days | Annual Days of use | Days/yr |
| DD | Bridgeport kW savings factor from pilot | kW/ 1000 Btu |
| DEEP | Department of Energy and Environmental Protection | 12, 2000 200 |
| DHW | Domestic Hot Water | |
| DHWH | Domestic Hot Water Heater | |
| DI | Annual savings per sq ft of duct insulation | |
| DOE-2 | Computer Energy Simulation Tool | |
| DP | Power Reduction Factor | % |
| DP | Drying Proportion of clothes washer energy | % |
| DPUC | Department of Public Utility Control | 70 |
| DRIPE | Demand Reduction-Induced Price Effects | |
| DSF | Seasonal Demand Savings Factor | kW/ton |
| E | Energy use rate | KW/toll |
| ECM | Electronically Commutated Motor | |
| EE | Efficiency conversion factor | |
| EEB | Energy Efficiency Board | |
| EER | Energy Efficiency Ratio | |
| EF | | L/kWh, % |
| EF | Energy Factor (Dehumidifier, Water Heater) | L/KWII, % |
| EF | Efficiency Factor | |
| | Heating System Efficiency | |
| EFF EFLH | Rated Motor Efficiency | 1 |
| | Equivalent Full Load Hours | hours |
| EKWH | Estimated Annual electric usage with increase in production | |
| EUL | Effective Useful Life | years |
| F | Fraction of lighting heat affecting cooling | |
| F | Factor | various |
| FC | Forward Curved Fan | |
| FCM | Forward Capacity Market | |
| FHLE | Fryer Heavy Load Efficiency | D. # |
| FIR | Fryer Idle Energy Rate | Btu/hr |
| FLH | Annual Full Load Hours | Hr/yr |
| FPC | Fryer Production Capacity | Lbs/hr |
| FPE | Fryer Preheat Energy | Btu |
| FR | Free-rider | |
| ACCF | Annual Gas Savings | Ccf/yr |
| G | Estimated lighting energy heat to space based on modeling | ~ |
| GPH | Average Peak Gallons per hour | Gal/hr |
| gpm | Gallons Per Minute | |
| GPY | Gallons (of water) per year | Gal/yr |
| GSHP | Ground Source Heat Pump | |
| H, h | hours (annual or daily) | hours |
| HAP | Computer Energy Simulation Tool | |
| HDD | Heating Degree Days for CT | °F |
| HF | Heating Factor | Btu/ft²/yr |
| HL | Heat loss savings per linear foot | Btu/hr/ft |
| HP | Horsepower (nameplate) | |
| HPWH | Heat Pump Water Heater | |
| HR | Ice Harvest Rate for ice-cube machines | |

Version Date: 10/30/2012 Abbreviations/Acronyms

| Symbol | Description (See Note [1]) | Units |
|--------------|--|-----------------------------|
| HR | Annual Electric Energy Usage Dependent on hours of Production | kWh/yr |
| HR | Percent heating not using backup electric resistance | % |
| Hrs | Operating hours per day | Hr/day |
| HSPF | Heating Seasonal Performance Factor | |
| HVAC | Heating, Ventilation, and Air Conditioning | |
| HWP | Hot Water Pump | |
| IGV | Inlet Guide Vane fan control | |
| IND | Annual Electric Energy Usage Independent of Production | kWh/yr |
| IPLV | Integrated Part Load Value | EER or kW/ton |
| ISO-NE | Independent System Operator New England | ELIC OF RAY, ton |
| kW | Electric Demand, kiloWatts | 1,000 Watts |
| kW | Fixture Input kW, total rated power usage of lighting fixtures | kW |
| kWh | Kilowatt Hour | kWh |
| KWH | Annual Electric Energy Usage | kWh/yr |
| KWHSF | Annual kWh savings factor based on typical load profile for | K VV III y I |
| KWIISI | application | |
| lbs | Pounds (Weight) | lbs |
| L | Ballast Location Factor | 108 |
| LBS | Pounds of food cooked per day | I be/day |
| LKWH | Lifetime kWh Savings | Lbs/day kWh |
| LI | Limited Income sector | W AA II |
| LN | Natural Log | |
| | | |
| LO | Lost Opportunity Park Hasting lead on the gas heiler or furness | Btu/hr |
| Load | Peak Heating load on the gas boiler or furnace | Watts/ ft ² |
| LPD | Lighting Power Density | watts/ It |
| M&V MBH | Measurement and Verification | 1000 Btu/hr |
| | Thousands of Btus per hour | |
| MEF | Clothes Washer Modified Energy Factor | ft ³ /kWh/ cycle |
| MMBtu | One Million of British Thermal Units | 1,000,000 BTU % |
| MP | Machine Proportion of clothes washer energy | 1 % |
| MW | Megawatt a unit of electric demand equal 1000 Kilo-Watt | |
| N | Production Rate | |
| N | Number of | |
| n NA A OC | Fixture number | |
| NAAQS | National Ambient Air Quality Standards | |
| NLI N. | Non-Low Income sector | 1-337 |
| Nr | Nameplate Rating of baseboard electric resistance heat | kW |
| 0 | Quantity of fixtures that have occupancy sensors | 01 |
| OHLE | Oven Heavy Load Efficiency | % D: " |
| OIR | Oven Idle Energy Rate | Btu/h |
| OPC | Oven Production Capacity | Lbs/h |
| OPE | Oven Preheat Energy | Btu |
| O&M | Operation and Maintenance | CI CI |
| P | Heating Penalty and Recovery adjustment | % |
| P | Potato Production Capacity | Lbs/h |
| PAA | Percent of facilities' energy use effected by PRIME | |
| PD | Peak Day savings for Gas measures | CcF |
| PD | Annual electric energy usage dependent on production quantity | kWh/yr |
| PDF | Peak Day Factor (Gas) | |
| PDHW | Peak hour hot water load | Btu |
| PF | Peak Factor | kW/kWh |
| Pf | Power factor | |
| PkW | kW demand savings | kW |

| Symbol | Description (See Note [1]) | Units |
|------------------|--|-----------------------------|
| PSC | Permanent Split Capacitor | |
| PSD | Program Savings Documentation | |
| PTAC | Package Terminal Air Conditioner | |
| PTHP | Package Terminal Heat Pump | |
| r | Climate Adjustment Ratio | |
| R | R value is a measure of thermal resistance | $ft^2 x h x {}^0F / BTU$ |
| Ratio | Ratio of heating capacity to cooling capacity | |
| REM | Residential Energy Modeling software or results | |
| RNC | Residential New Construction sector | |
| RP | Retail Products sector | |
| RTU | Roof Top Unit | |
| RUL | Remaining Useful Life | Years |
| S | Savings | varies |
| S | C&I Lighting annual kWh savings | kWh |
| SA | Seasonal efficiency adjustment | % |
| Savings Fraction | Fraction of base-case consumption saved with low-intensity radiant | 70 |
| Savings Fraction | heaters. | |
| SAWC | Steamer Average Water Consumption Rate | Gal/h |
| SEER | Seasonal Energy Efficiency Ratio | Guirii |
| SF | Area | Square Feet |
| SF | Savings Factor | Square 1 cet |
| SHLE | Steamer Heavy Load Efficiency | % |
| SIR | Steamer Idle Energy Rate | Btu/h |
| size | Capacity (Volume) | ft ³ , pints/day |
| SKF | Summer Factor | kW/ft ² |
| SKW | | kW |
| Sleeve | Seasonal Summer Peak Summer Demand Savings Unit without louvered sides | K VV |
| SLR | Standby Loss Rate | Btu/hr |
| SMB | Small Business | Dtu/III |
| SO | | |
| SPC | Spill-over | Lbs/h |
| SPCS | Steamer Production Capacity Steamer Percent of time in Constant Steam mode | % |
| SPE SPE | | , <u>-</u> |
| T | Steamer Preheat Energy | Btu °F |
| | Temperature | _ |
| TON | Capacity of the Equipment, Tons | 12,000 BTU/h |
| TRACE | Computer Energy Simulation Tool | |
| UDRH | User defined reference home | |
| UI | United Illuminating | Valta |
| V | Volume | Volts ft ³ |
| V | Volume | 1t |
| VAV | Variable Air Volume | |
| VFD | Variable Frequency Drives | C. |
| W | Width | ft |
| Watt, W | Wattage Dale Watta | Watt |
| $Watt_{\Delta}$ | Delta Watts | 1 3371 |
| WCS | Electric Cooling energy savings from Wisconsin study | kWh |
| WF | Water Factor | Gal/ft ³ |
| WH | Water Heater, Water Heating | |
| WHS | Electric Heating energy savings from Wisconsin study | |
| WICDD | Cooling Degree Days for WI | |
| WIHDD | Heating Degree Days for WI | |
| Window | Unit with louvered sides | 1 777 |
| WKW | Seasonal Winter Peak Demand Savings | kW |

Version Date: 10/30/2012 Subscripts

| Symbol | Description (See Note [1]) | Units |
|-------------|---|-------|
| WP | Water Heating Proportion of clothes washer energy | % |
| WPF | Winter Peak Factor | W/kWh |
| WSHP | Water Source Heat Pump | |
| YR | Year | |
| ΔkW | Reduction in power for each light | kW |
| ΔT | Delta (or Differential) Temperature | °F |
| ηb | base case efficiency | |
| ηρ | proposed case efficiency | |

Subscripts

| Symbol | Description (See Note [1]) | Units |
|----------------|--|--------------------------|
| ···A | Actual/installed Unit | |
| ···a | After PRIME | |
| •••ь | Baseline Unit | |
| ···BD | Blower Door flow rate reading performed at 50 Pa | Cubic Feet per Minute |
| ···Bin | Temperature BIN hours | |
| с | Cooling | |
| CAC | Central Air Conditioning | |
| ···CDH | From CDH HVAC study | |
| ···d | number of hours that piece of equipment is expected to operate per | h |
| | Day | |
| ···∆ | Delta | |
| ···dp | Double pane window | |
| · · · door kit | Door kit, Door sweep | |
| ···DS | Duct Sealing flow rate reading performed at 25 Pa | Cubic Feet per Minute |
| •••Е | Electric energy | |
| •••e | Existing (unit, production rate, etc) | |
| ···es | ENERGY STAR | |
| · · · ES 09 | ENERGY STAR 2009 unit | |
| · · · fed std | Federal Standard unit | |
| ···G | Natural Gas | |
| · · · gasket | Air sealing gasket | |
| h | Based on billing history | |
| н | Heating | |
| ···HP | Heat Pump | |
| ···HVAC | HVAC motor | |
| ···hw | Hard Wired light fixtures | |
| i | incoming | |
| _i | Installed Unit | |
| ···ic | Interactive Cooling | |
| L | Lighting | |
| ···LI | Low Income sector | |
| ···LO | Lost Opportunity measure | |
| ···lpd | Lighting Power Density | |
| ···lt | Life Time | |
| ···M | Motors | |
| ···N | Non-HVAC applications | |
| ···NLI | Non-Low Income sector | |

Version Date: 10/30/2012 Subscripts

| Symbol | Description (See Note [1]) | Units |
|----------------|--|-------|
| 0 | Oil | |
| 0 | Others | |
| ···os | Occupancy Sensors | |
| •••Р | Process | |
| •••Р | Propane | |
| · · · post | Final Reading | |
| ···pre | Initial Reading | |
| ···R | Electric Resistance | |
| ···R | Refrigeration | |
| · · · ratio | Ratio between low efficiency value and high efficiency value | |
| · · · retire | Retirement portion | |
| ···retro | Retrofit portion | |
| · · · retrofit | Retrofit portion | |
| ···s | Summer | |
| ···sealing | Caulking, sealing, polyethylene tape | foot |
| ···total | Total, Sum | |
| ···w | Water Heating | |
| ···wop | Without PRIME | |
| ···wp | With PRIME | |
| ···wt | Winter | |
| ···wx | Weatherstrip, repair | |
| •••у | number of hours that piece of equipment is expected to operate per | h |
| • | Year | |

<u>Notes</u>

[1] Many of these terms have more complete definitions in the Glossary section.